



Active Wavefront Control for Megawatt Arm Power

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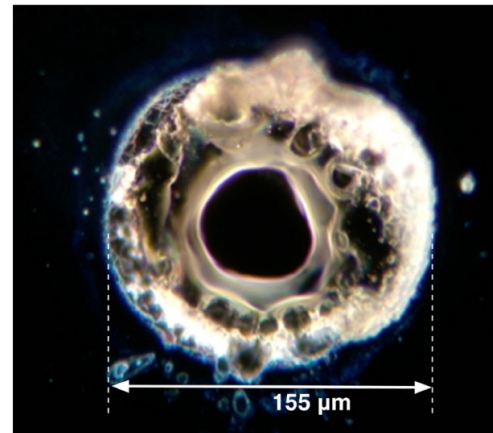
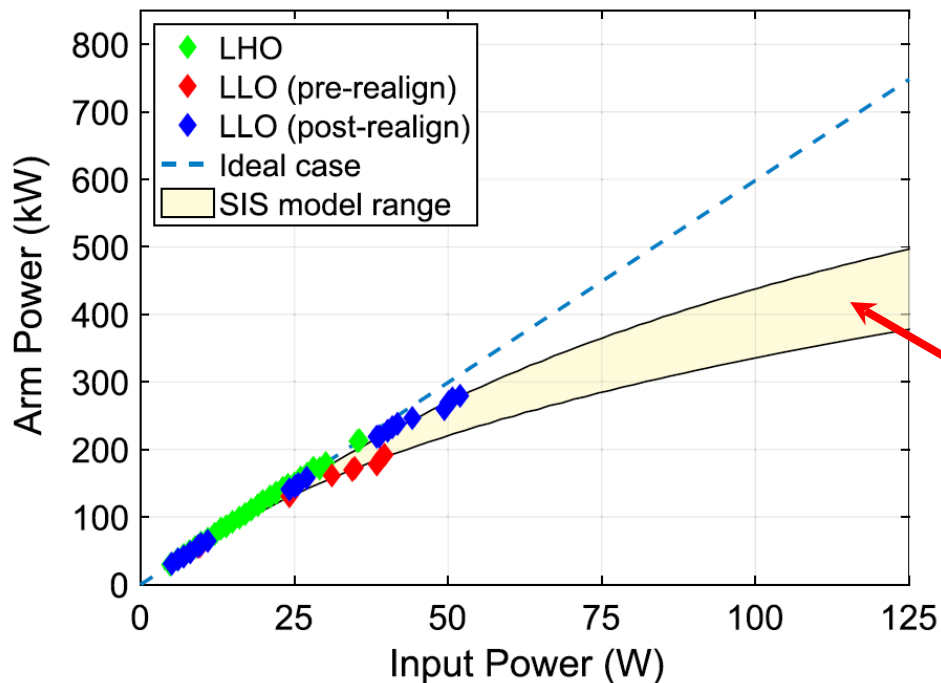
LIGO-G2200399

Introduction

- In the push towards higher interferometer power, **coating absorption** is a limiting problem
 - Serious challenges both from nonuniform *and* uniform absorption
- At megawatt power, even uniform absorption will require higher-order (above ROC) wavefront corrections
 - Beyond the capabilities of the current Thermal Compensation System (TCS)
- Here we present a design for a new wavefront actuator targeting these emerging challenges

Challenge #1: Point Absorber Scattering

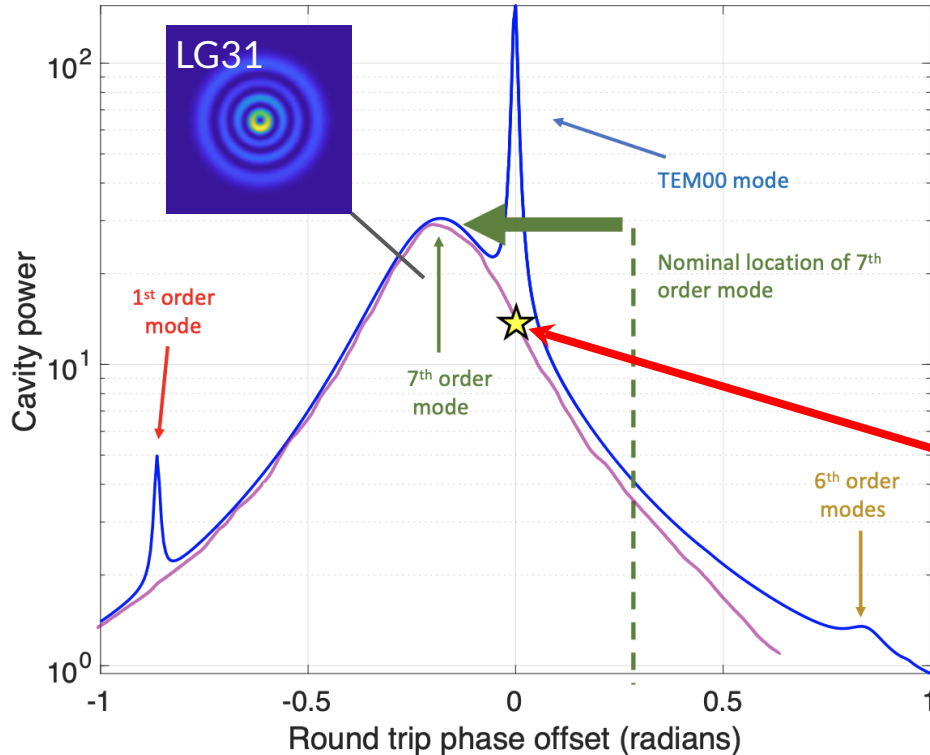
The aLIGO picture circa O3 (Brooks *et al.*, [P1900287](#))



Dependence on point absorber position

Modal Degeneracies Exacerbate Scatter Losses

Simulated arm cavity scan (A. Brooks, [G2101232](#))



- Loss of power from mode HG00 to HGmn:

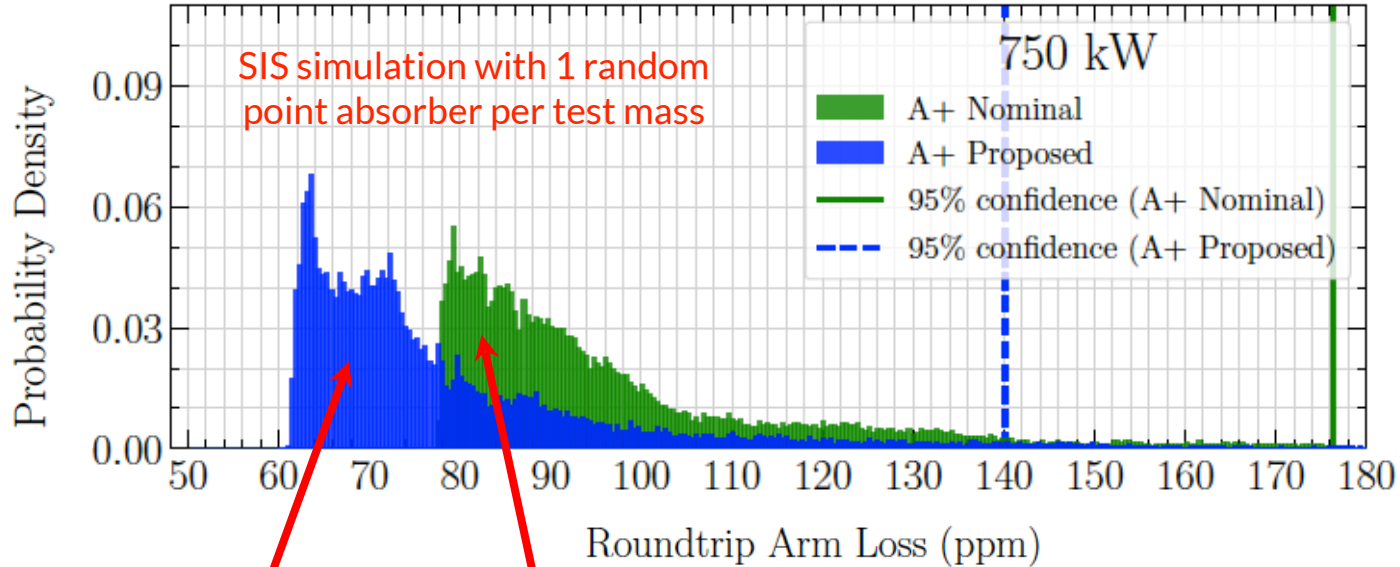
$$\mathcal{L}_{mn} = a_{00|mn}^2 g_{mn}$$

Single-bounce scattering coefficient

Resonant enhancement/suppression factor

Modal Degeneracies Exacerbate Scatter Losses

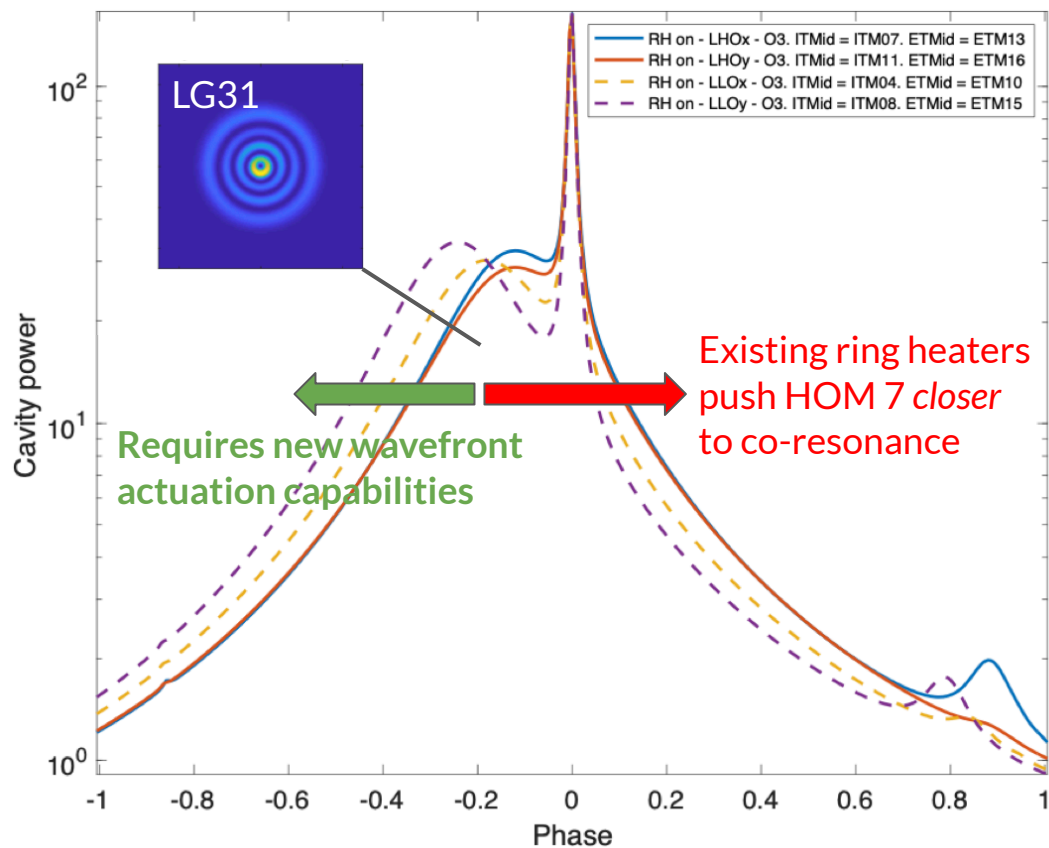
Simulated arm loss distributions (J. Richardson *et al.*, [P2100184](#))



After elimination of
HOM 7 co-resonances

Nominal
arm cavity

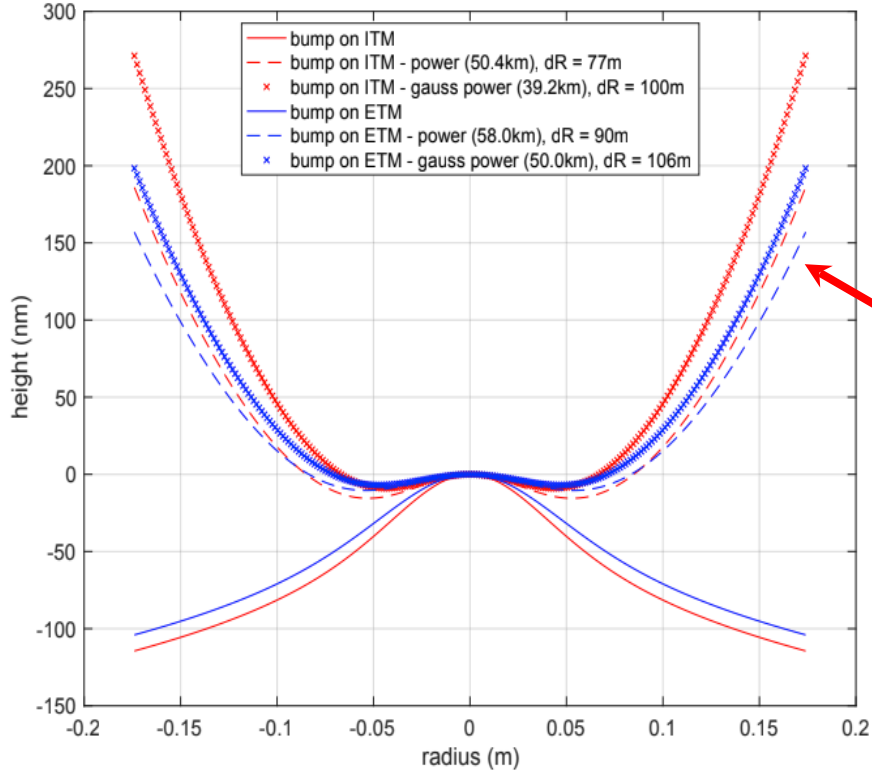
Active Mitigation of HOM 7 Co-Resonances



(A. Brooks, [G2101232](#))

Challenge #2: Uniform Coating Absorption

Deformation by 1W absorption (H. Yamamoto)

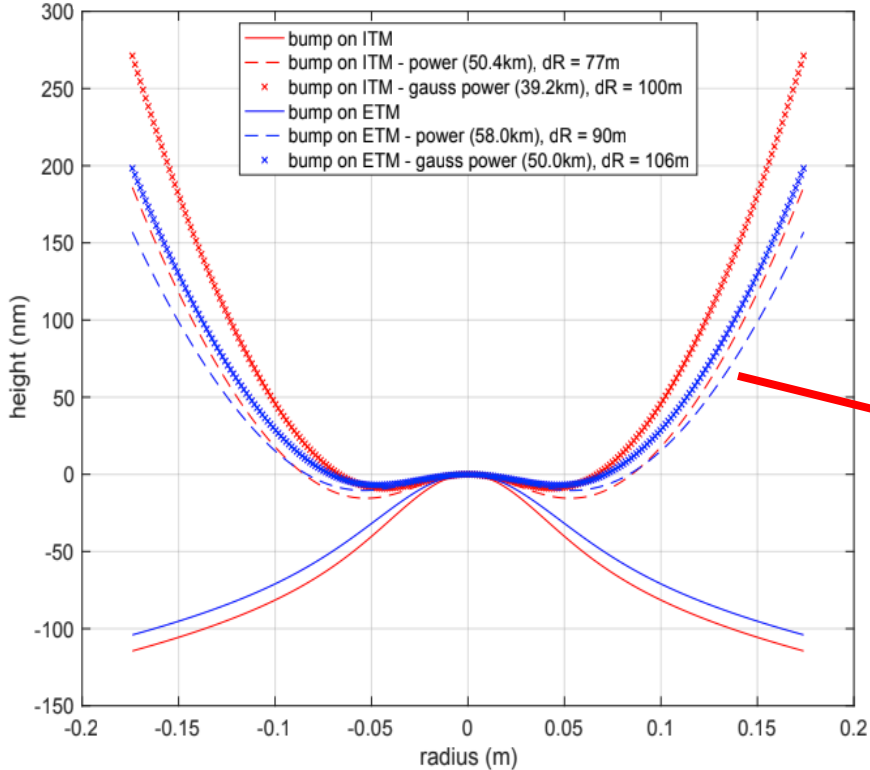


1W coating absorption = (2 MW arm power) x (0.5 ppm)

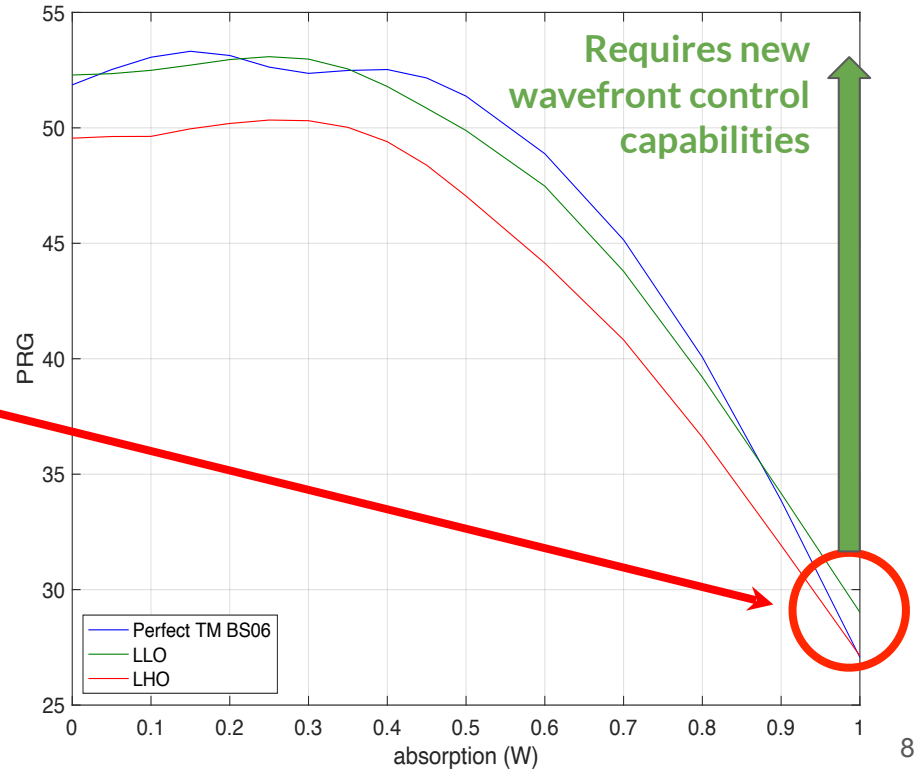
Residual ETM/ITM surface deformation
after optimal ring heater correction

Challenge #2: Uniform Coating Absorption

Deformation by 1W absorption (H. Yamamoto)

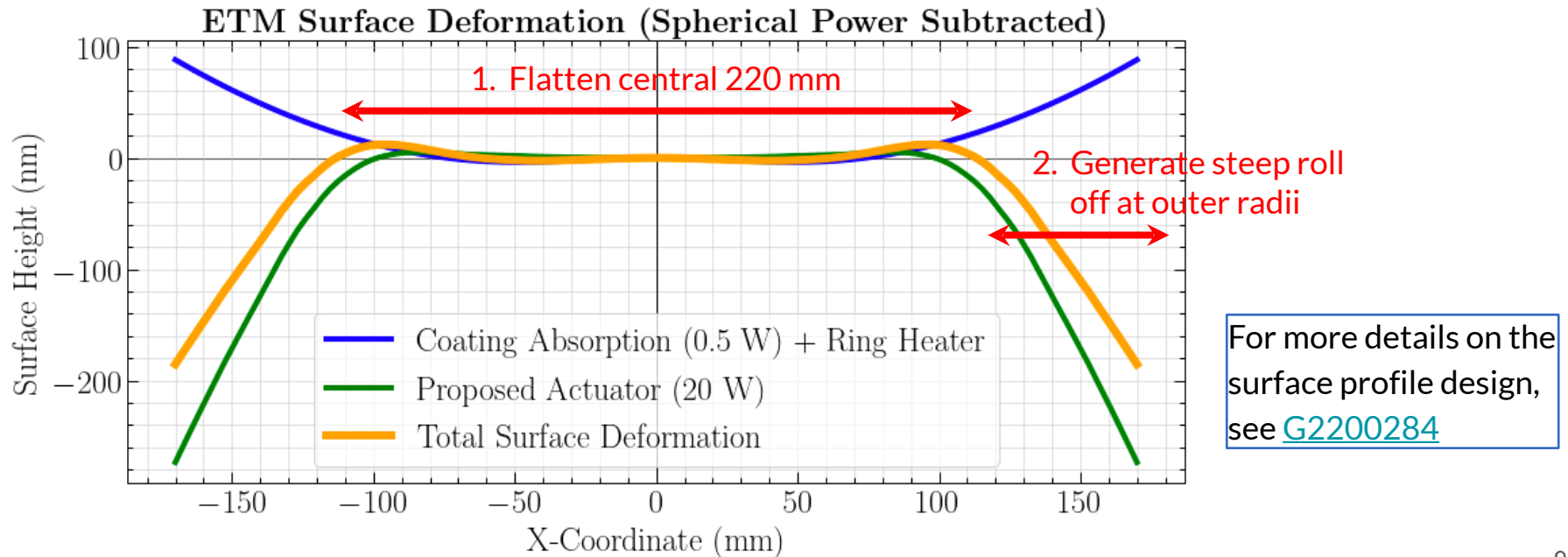


Power recycling gain vs. absorption (H. Yamamoto)

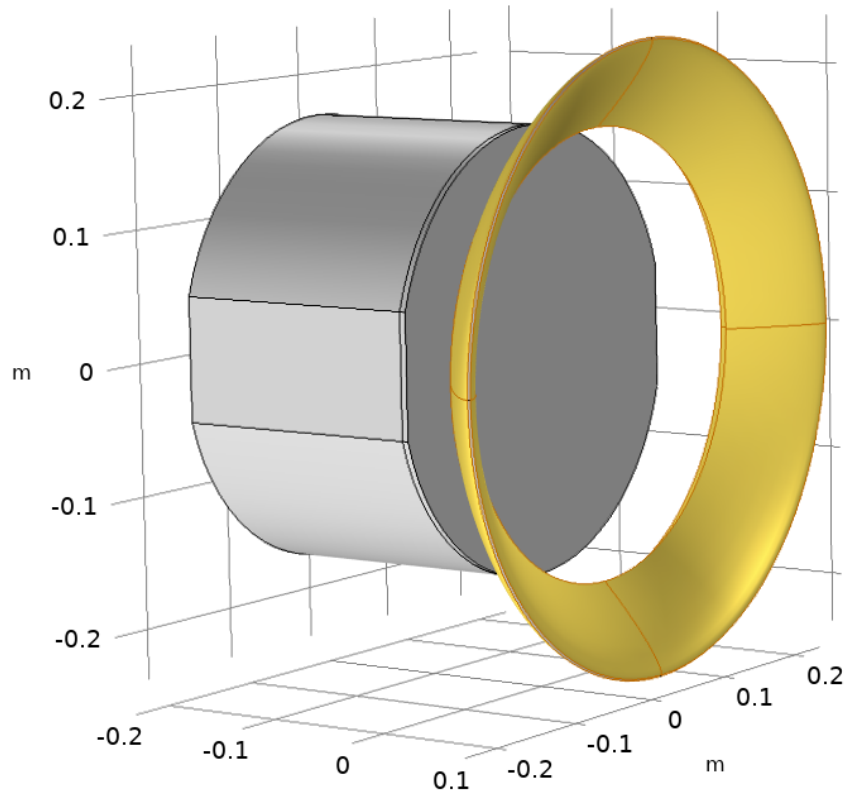


The Higher-Order Mode (HOM) Ring Heater

- We have designed a new wavefront actuator aimed at both of these problems:

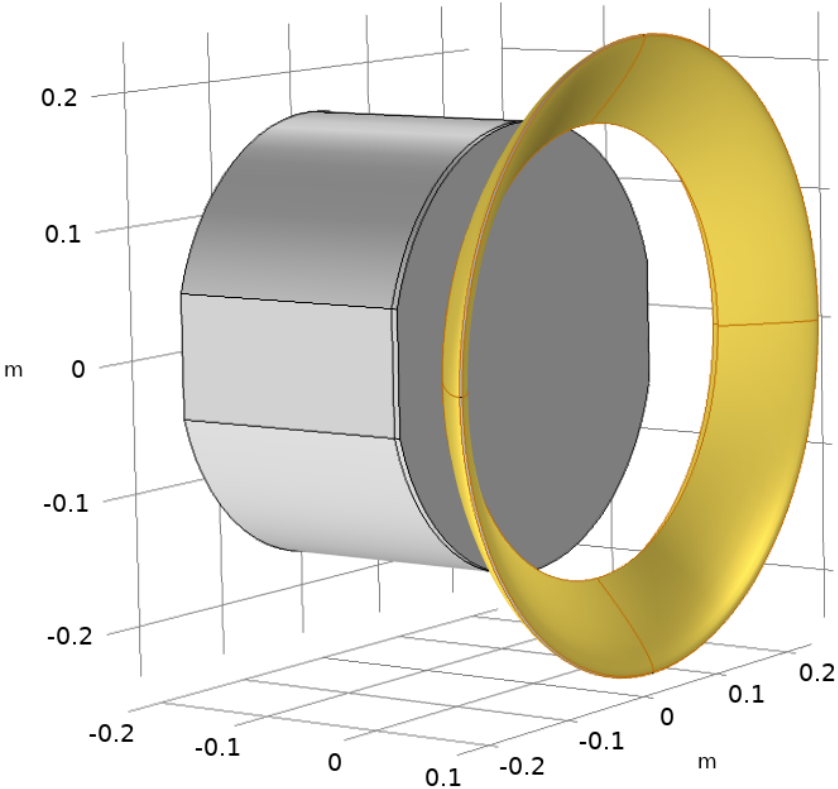


HOM Ring Heater Design

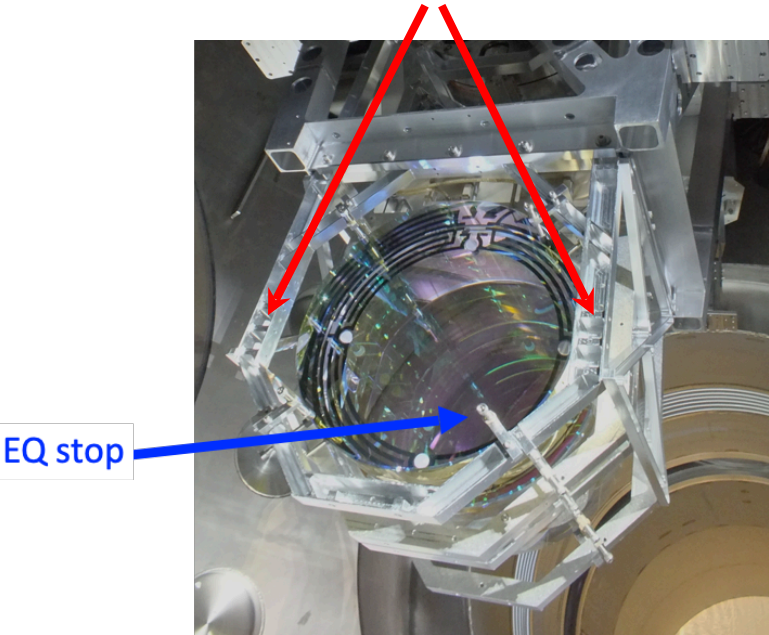


- Annular heating pattern projected onto front surface of test mass
- **Simple design:** Consists of ring heater element and 8.25 cm-long reflector
- Reflector interior:
 - Superpolished to < 10 nm RMS
 - Metallic thin film broadband reflective coating (e.g., gold)
- Reflector exterior:
 - Sandblasted for minimal specular reflection of 1064 nm light
 - 1064 nm absorptive coating (possibly)

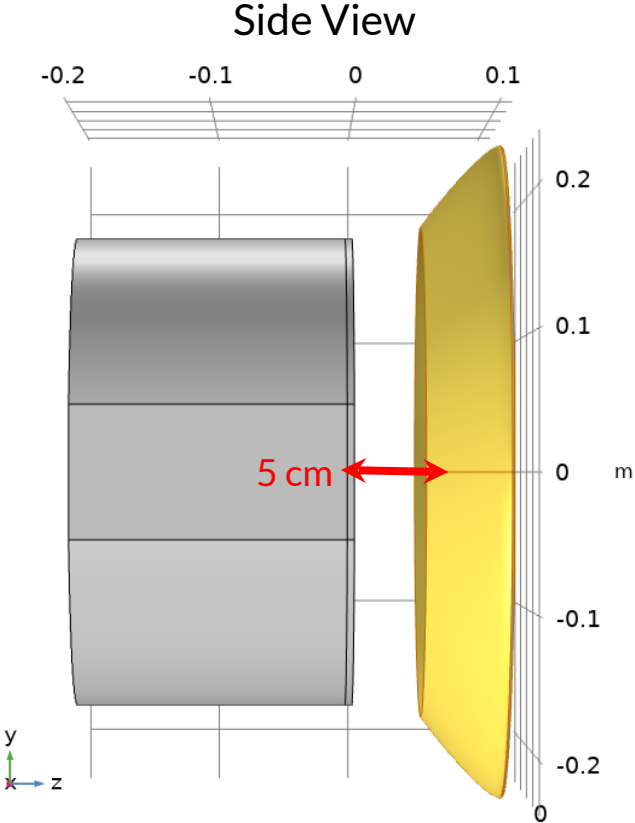
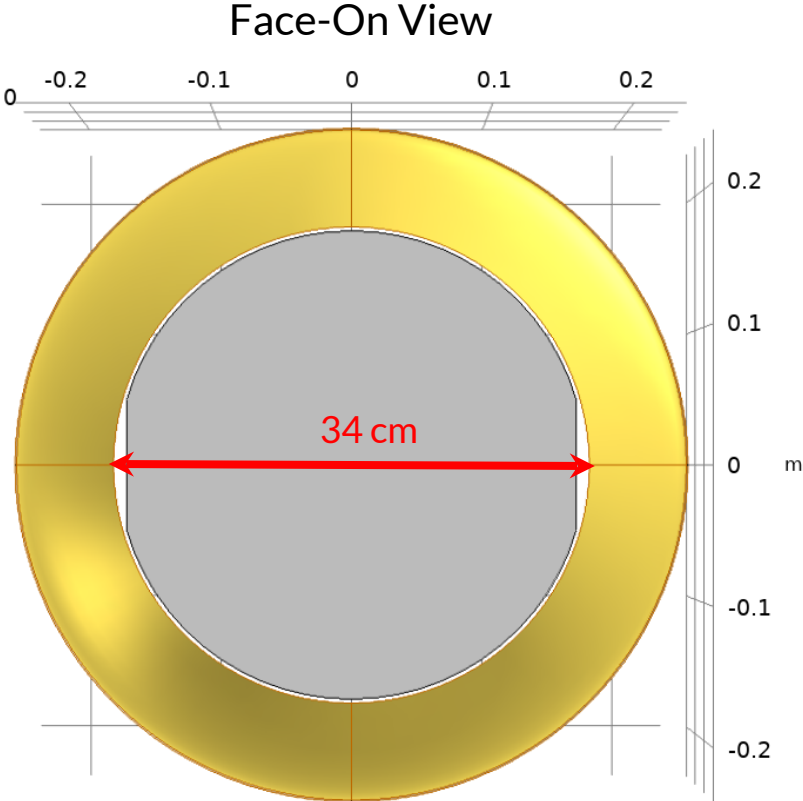
HOM Ring Heater Design



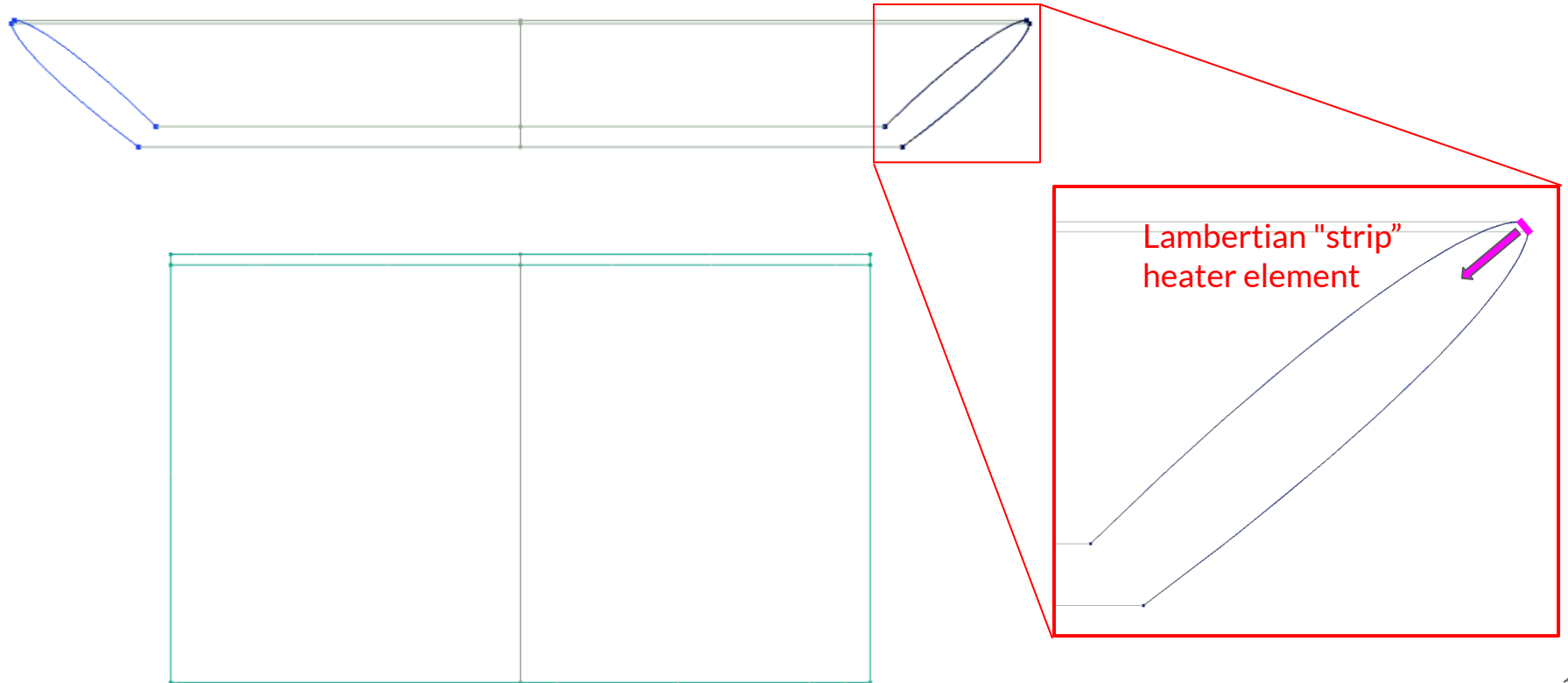
Mounted to lowest section of suspension cage



HOM Ring Heater Design

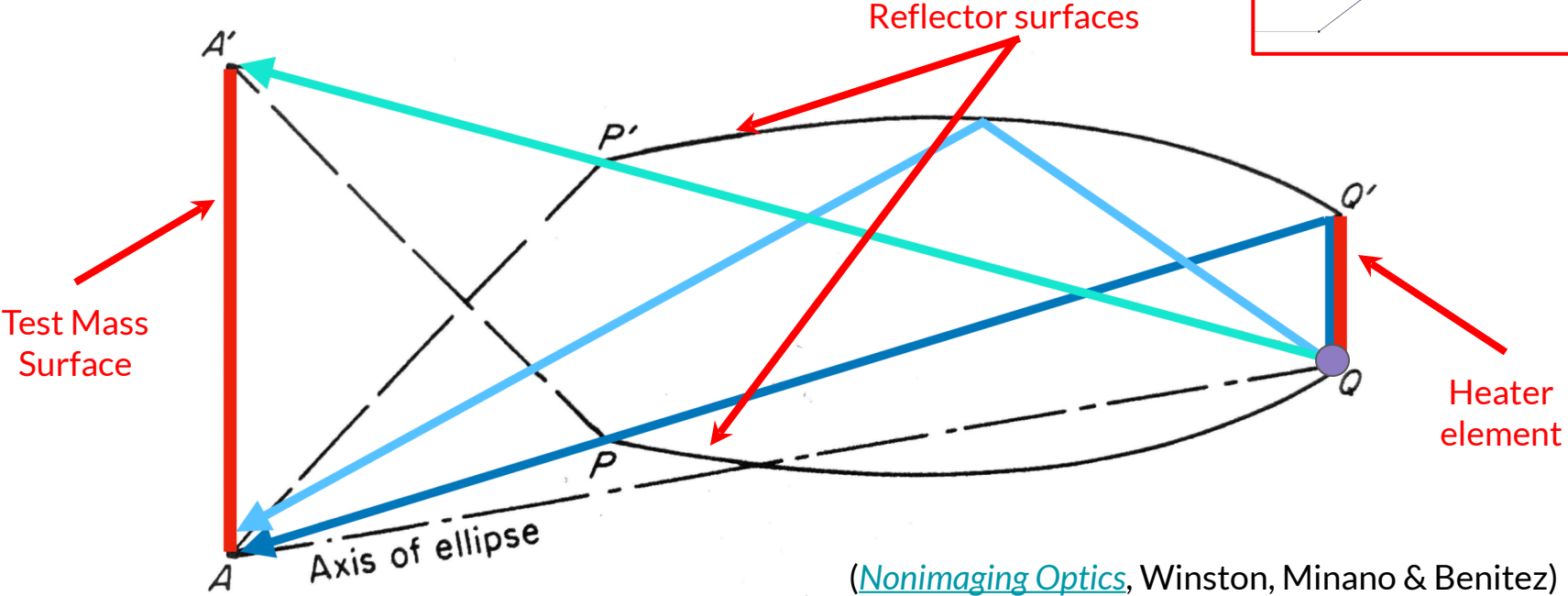


Two-Dimensional Cross-Section



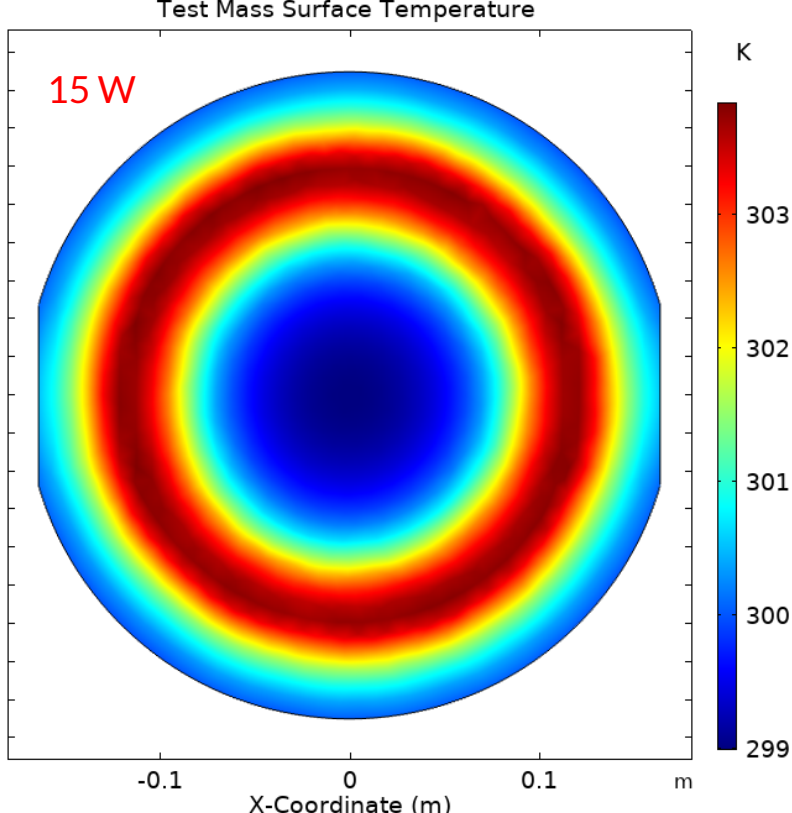
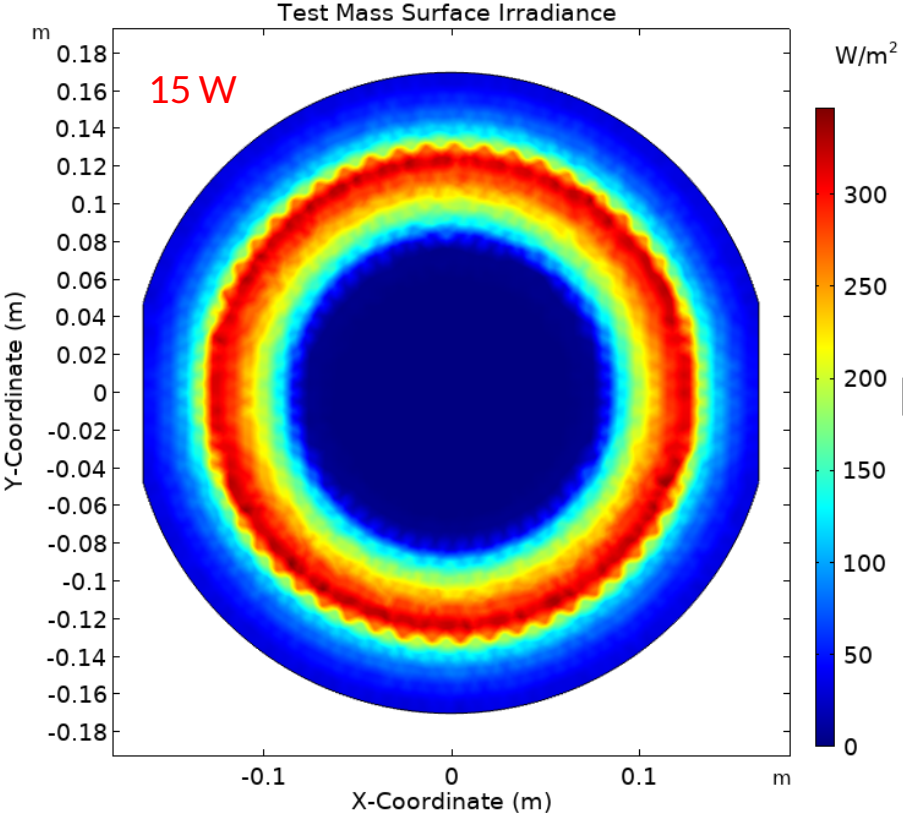
Optical Design Principle

Based on the *nonimaging elliptical concentrator* from solar energy

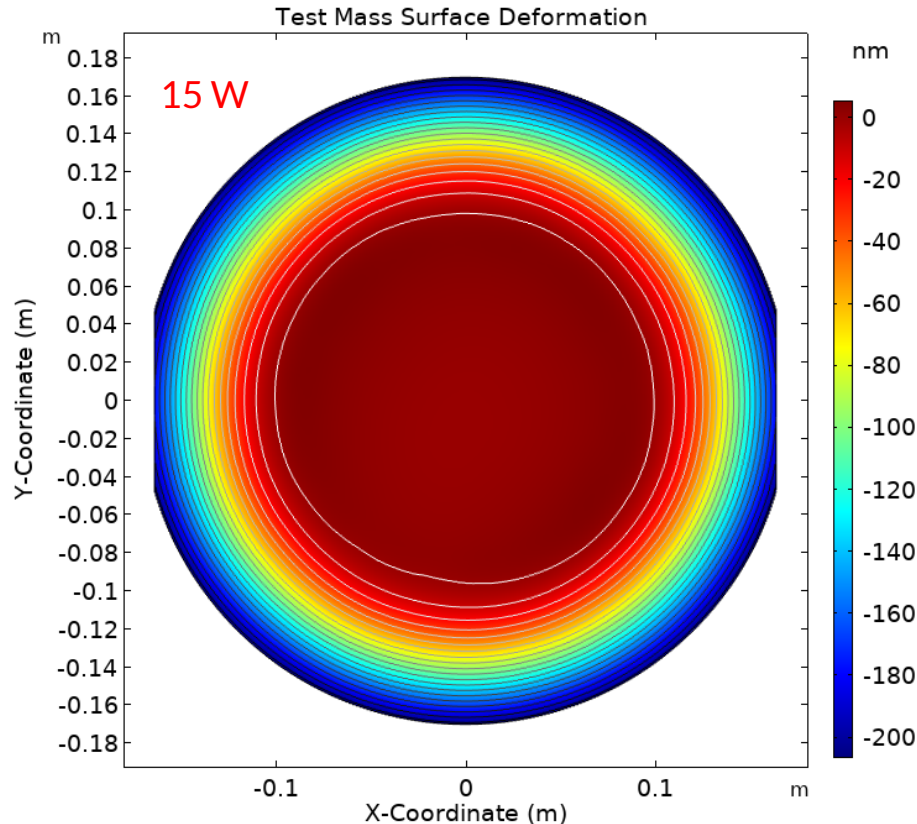


([Nonimaging Optics](#), Winston, Minano & Benitez)

COMSOL Ray-Tracing Analysis

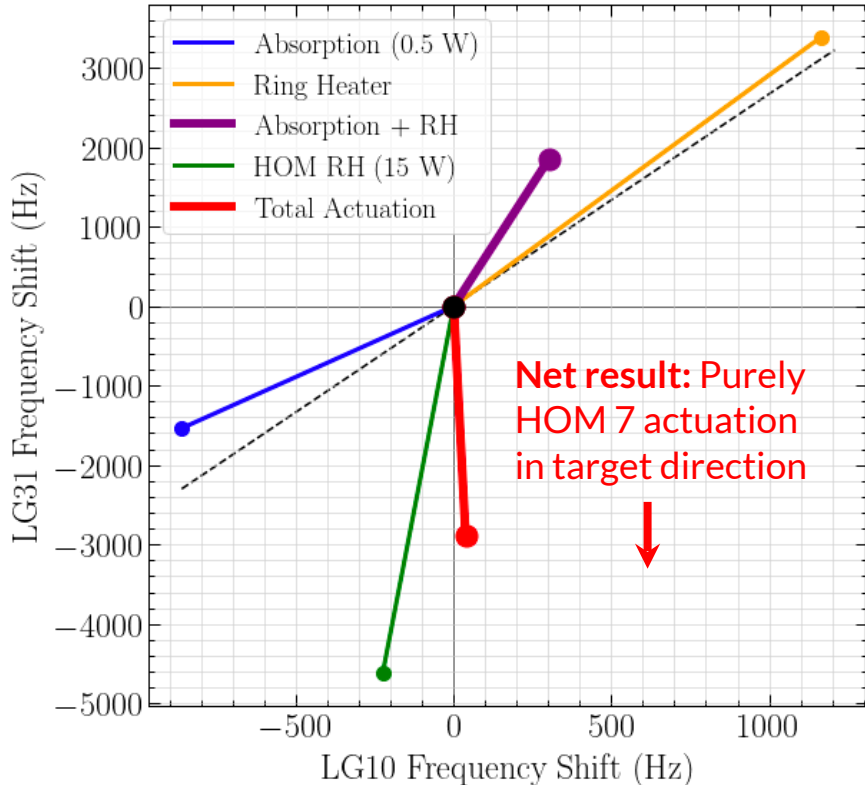


COMSOL Thermal Stress Analysis



- **70.0%** power transfer efficiency
- Nominal operation:
 - $P = 15\text{ W}$
 - $T = 560\text{ K}$ (287 C)
- Max-power operation:
 - $P = 40\text{ W}$
 - $T = 716\text{ K}$ (443 C)

Performance Metric



- Compare the shift in resonance frequencies of LG31 vs. LG10 modes
- Design objective:
 - Maximize overall LG31 shift (dynamic range)
 - Minimize overall LG10 shift (impact on low-order modes)

Project Status & Next Steps

- NSF-supported joint development effort between UC Riverside (Richardson group) and LIGO Lab (ADTR led by A. Brooks, [M2200050](#))
- Targeted as an O4 Detector Improvement
- Next steps:
 - Mechanical design (mounting structure)
 - Electrical design (in-vacuum cabling, feedthroughs)
 - Materials selection (coatings, etc. may require UHV qualification)
 - Prototype fabrication