IMPROVING THE ACCURACY OF ALIGO CALIBRATION: CALIBRATION ERROR MODELS FOR PRECISION TESTS OF GENERAL RELATIVITY

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ABSTRACT

In 2015, the first direct detection of gravitational waves (GWs) was realized with the advanced Laser Interferometer Gravitational Wave Observatory (aLIGO). With the detection emerged the ability to test General Relativity (GR) in large velocity, highly dynamical and strong-field gravity regimes. If GWs were to reveal deviations from GR, the deviations would be extremely small; characterizing and reducing uncertainties in aLIGO data would allow as much physical information to be recovered in the GW signal as possible. The intent of this project is twofold: to describe the calibration methods and uncertainties used for aLIGO and to also begin the discussion on the impact of calibration errors on precision tests of GR. We first describe the current calibration methods for aLIGO and the most important calibration error sources. Then, in a model, we generate GW signals with a non-GR deviation in the merger-ringdown regime. We recover the deviation through Bayesian parameter estimation to determine the precision with which such deviations can be detected. We conclude with discussing how new calibration error models could increase that precision, and include a more sophisticated model setup in the Appendix.

I. INTRODUCTION

In 1915, Einstein published his General Theory of Relativity (GR). This theory and his following papers predicted the existence of gravitational waves (GWs), or oscillations in the curvature of spacetime caused by the acceleration of massive bodies. In 1993, a Nobel Prize went to Hulse and Taylor [8] who discovered a pulsar system losing energy at the same rate as predicted by GW emission and thus providing strong observational evidence for the existence of GWs. Then in 2015, a direct detection of a GW occurred. GW150914, identified as a result of a binary black hole merger, was observed with the Advanced Laser Interferometer Gravitational Wave Observatory (aLIGO) detector network [2]. With this detection, the field of direct GW observations emerged.

GWs allow us to observe strong-field dynamics of space-time and astrophysical phenomena inaccessible by electromagnetic radiation. With the direct detection of GWs, experiments to test GR in large velocity, highly dynamical, and strong-field gravity regimes can be conducted. Because GWs cause extremely small deviations in spacetime (on the order of 10^{-23} [2]) the aLIGO sensors and signal analyses need to be precise. Characterizing and reducing uncertainties in aLIGO data allows us to extract as much physical information from the GW signal as possible.

The goals of this work are to (1) describe both the calibration methods used for aLIGO and their uncertainties and (2) begin the discussion on the effects of this calibration uncertainty on precision tests of GR. It is unknown how large non-GR deviations in GW signals may be if

they exist, and consequently whether the calibration errors (CEs) in aLIGO are large enough to disguise any of these non-GR deviations, which that may otherwise be revealed by stacking many GW signals (a technique discussed in Section V). If they are great enough, it is unknown if implementing a calibration error model would reduce the CE impact enough to see these non-GR deviations. So we begin the discussion of the effects of calibration uncertainty on precision tests of GR by developing a model in which we introduce a parametrized deviation from the GR-predicted GW waveform in the mergerringdown regime. Then we attempt to recover the deviation through Bayesian parameter estimation. We suggest next steps in this investigation, including implementing a frequency dependent calibration error model to see its impact.

The layout of this paper is as follows. First, we specify our focus on CEs in Section II. Next, we summarize how aLIGO detects GW and how these CEs impact the instrument in III. In IV, we describe the differential arm length (DARM) closed feedback loop transfer function, which contains the GW wave signals and CEs for aLIGO. We then describe our model in VI. We discuss next steps in VII and a more sophisticated modeling in X.

II. CALIBRATION ERRORS

Two sources of uncertainty in any instrument are statistical and systematic uncertainty. Statistical uncertainty— a zero-mean Gaussian distribution measurement variation— is unavoidable, but it can be reduced by taking additional measurements. Systematic uncertainty stems from an incorrect characterization of

a detector, resulting in, for example, calibration errors (the dominant source of systematic error in aLIGO). For aLIGO, careful calibration has to be maintained to accurately associate the frequency response of the detector with the motion of aLIGO's optics to reduce systematic error. These systematic/calibration errors are the focus of this project.

For aLIGO, calibration errors (CEs) are errors that pertain to the conversion of instrumental readout to GW strain data and are contained in a differential arm length (DARM) control loop. CEs can affect detection rates and parameter estimations; here we are concerned with parameter estimation. Current CEs for aLIGO are estimated as a correction to the amplitude and phase response of the detector, as an (assumed smooth) function of frequency. The detector response is, to a very good approximation, linear: GWs at a particular frequency appear in the detector response only at that frequency. A new, functional frequency dependent estimation method [15, 19] is discussed in Section X.

This work uses a Bayesian approach to quantify potential CE effects on signal injections which mimic both GR and non-GR conforming GWs. It is possible that the CEs will blur our ability to distinguish between the two; we also investigate if our frequency dependent method of characterizing CEs will allow us to distinguish the GR and non-GR conforming signal injections. Though the few individual GW signals detected so far have had no statistically significant disagreement with GR and their statistical error exceeds their systematic error, the aLIGO detectors are not yet at their design sensitivities, louder GW sources may yet be detected, and the potential to combine or "stack" GW observations as in [16] to increase sensitivity all encourage this work [4].

III. HOW LIGO DETECTS GWS

aLIGO is a complex and cutting edge instrument; it consists of a modified Michelson interferometer with Fabry-Perot arms, power-recycling mirrors, and resonant sideband extraction which all allow it to measure minuscule phase propagation differences via the Pound-Drever-Hall technique [7, 10, 12]. However, we follow [19] in this analysis and reduce the entire instrument to a sensor with a single degree of freedom: differential arm length (DARM) deviations. When a GW passes through aLIGO, the space in one direction stretches while the space in the other direction contracts; this arm length change/deviation interrupts the constructive interference of laser light maintained in the arm cavities and some light escapes the arms to a photodetector (see Figure 1). This escaped light generates the signal we analyze to recover the GW parameters.

Figure 2 illustrates a waveform that aLIGO might detect. From the amplitude and phase of this waveform, we can extract astrophysical parameters such as those listed in Table 1.

In this work, we focus on a single-parameter analysis in the merger-ringdown regime to test GR using multiple events, rather than characterizing a particular GW event. Consequently, we marginalize over the parameters listed in Table 1.

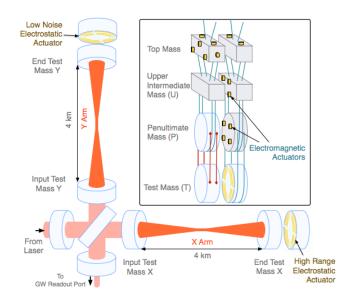


FIG. 1.— This diagram of aLIGO is from [15]. The arm cavities are contained between the reflective test masses. These test masses are suspended from a quadruple pendulum system and are adjusted spatially by an actuating system displayed in the upper right panel. These adjustments allow resonance to be maintained in the arm cavities. When resonance is disrupted by a passing GW stretching one arm cavity and shrinking the other, some light escapes to the GW Readout Port at the bottom of the figure.

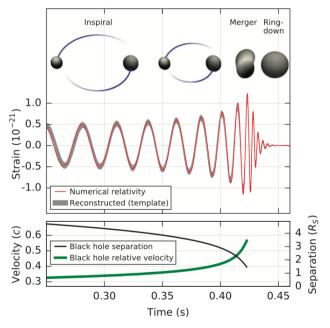


FIG. 2.— A figure illustrating an inspiral-merger-ringdown (IMR) of a compact binary system from [2]. According to GR, two objects in orbit will slowly spiral inwards due to a loss of energy and angular momentum via GWs. The frequency and amplitude of the emitted GWs increases as the orbital distance between the objects shrinks. When the objects finally merge they can radiate GWs as a superposition of quasinormal ringdown modes. One mode will eventually dominate with a exponentially damped, constant frequency wave [4]. We observe this as a lower frequency inspiral phase, a post-merger peak at some fixed frequency, and then a higher frequency ringdown. In this work we investigate the differences due to non-GR conformity as described in a parameter pertaining to the merger and ringdown of the GW.

TABLE 1 PARAMETERS USED TO CHARACTERIZE A GW DETECTION.

| m_1, m_2 | Masses | | |
|------------------------------|-----------------------------------|--|--|
| q | Mass ratio | | |
| \mathcal{M}_c | Chirp Mass | | |
| $\mathbf{S}_1, \mathbf{S}_2$ | Spins | | |
| χ_{eff} | Effective inspiral spin parameter | | |
| D_L | Luminosity Distance | | |
| t_c | Coalescence time | | |
| ϕ_i | Phase of coalescence | | |
| α, δ | Sky location | | |
| $\cos \iota$ | Orbital orientation | | |
| ψ | Polarization angle | | |

The external differential arm length change, ΔL_{free} , is related to the GW amplitude, called the "strain:" $h(f;t) = \frac{\Delta L_{free}}{\langle L \rangle} \tag{1}$

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where $\langle L \rangle \approx 4000m$ is the arm cavity length of aLIGO. aLIGO's photodetector does not directly measure ΔL_{free} but rather the current generated from the carrier laser power fluctuations, d_{err} (the DARM error signal), in arbitrary units. ΔL_{free} must be reconstructed from $d_{err}(f)$.

 $d_{err}(f)$ is measured continuously in a closed feedback loop. The purpose of this feedback loop (see the reduced block schematic in Figure 3) is to recenter the mirrors used in aLIGO after the arms have been perturbed by a GW or noise so that the constructive interference/resonance of the laser is maintained. This allows the instrument to remain in the constant linear response regime, and measure the next arm length differential as quickly as possible.

We can reconstruct h(f;t) from the DARM control loop (see Figure 3):

$$\langle L \rangle h(f;t) - \Delta L_{ctrl} = \Delta L_{res}$$

$$h(f;t) = \frac{1}{\langle L \rangle} \left(\frac{1}{C(f;t)} D(f) d_{err} + A(f;t) d_{ctrl} \right)$$
(3)

$$h(f;t) = \frac{1}{\langle L \rangle} \left(\frac{1 + G(f;t)}{C(f;t)} d_{err} \right)$$
 (4)

$$h(f;t) = \frac{1}{\langle L \rangle} R_e(f;t) d_{err}$$
 (5)

where
$$R_e(f;t) = \frac{1 + A(f;t)D(f)C(f;t)}{C(f;t)}$$
 (6)

$$=\frac{1+G(f;t)}{C(f;t)}\tag{7}$$

Here, C(f;t) is the transfer function of the arm cavity or the sensing function, D(f) is a digital filter, and A(f;t) is the actuation function that corrects mirror position. d_{ctrl} is the signal sent to the actuators describing how to move the test masses to recover resonance, ΔL_{ctrl} is the length deviation the actuation function applies to the test masses, and ΔL_{res} is any residual length change the actuation function happens to not correct. The product of these transfer functions is G(f;t) = C(f;t)D(f)A(f;t), the DARM open loop gain. We further rearrange this equation into a response func-

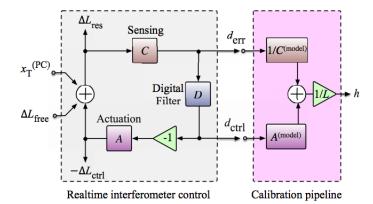


Fig. 3.— A block diagram of the DARM feedback control servo from [15]. This schematic shows that aLIGO's output is dependent on the performance of the feedback loop. Each component of the feedback loop is described by a transfer function and the uncertainty on the overall loop transfer function yields the CEs on the GW strain detection. The transfer functions of all of the components in the feedback loop are necessary to reconstruct the GW signal. The subsystems are described more thoroughly in [15, 19].

tion, $R_e(f;t)$, which lets us estimate uncertainty more easily. D(f) is known precisely, so the uncertainty in our GW strain, $\sigma_h(f;t)$, is dominated by the uncertainty in $R_e(f;t)$: $\sigma_R(f;t)$. Equation 7 is derived and its components described more thoroughly in [19, 15]. More complex calibration loop treatments are given in [1, 13].

In equation 5, $R_e(f;t)$ gives the theoretical or exact response function, but the measured length function $R_m(f;t)$ includes CEs from the sensing C(f;t) and actuation A(f;t) functions as well as the slow, timedependent drift in these functions. Because detectors are noisy, drift with time, and can glitch, $R_e(f;t)$ and $R_m(f;t)$ can differ. This leads to systematic errors in GW strain reconstruction.

The frequency dependent and time dependent parameters of R(f;t) are what impact the response function uncertainty, $\sigma_R(f;t)$. We examine these parameters for C(f;t) and A(f;t).

IV.I. Sensing Function, C(f;t)

The sensing function (see Figure 4) "senses" GW strain. It represents the interferometer optical plant and is approximated by a coupled-cavity single pole function [9]:

$$C(f;t) = \frac{\kappa_C(t)C_R(f)}{1 + if/f_{CC}(t)}e^{-2\pi i f \tau_C}$$
(8)

optical gain $\kappa_c(t)$:

fcc(t): coupled cavity pole frequency "sensing residual" after cavity $C_R(f)$: pole is divided out

sensing function time delay τ_C :

The optical gain $\kappa_c(t)$ depends on the laser power in the optical arm cavities and has a time dependent scalar gain factor. Equation 7 indicates $R_e(f;t) \approx 1/C(f;t)$ when $|G(f;t)| \ll 1$. Changes in the optical gain produce the largest systematic errors at frequencies above

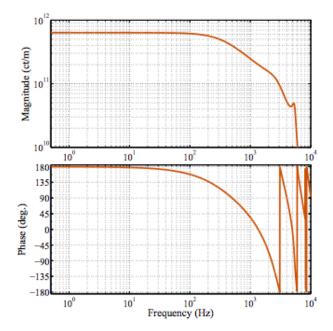


Fig. 4.— Figure from [15]. The sensing function model is shown in magnitude (top) and phase (bottom). The frequency dependence of C(f;t) is determined by f_{cc} up until 1 kHz; afterwards, analog-to-digital conversion factors (in $C_R(f)$) dominate. The features at higher frequencies are due to photodiode electronics and processing filters [15].

the unity gain frequency (40 Hz and 56 Hz for H1 and L1, respectively [15]). The coupled cavity pole frequency $f_{cc}(t)$ depends on the reflectivities of the interferometer optics and has a time dependency due to cavity length and alignment changes [14]. This changes the shape of the sensing function at frequencies close to the nominal coupled cavity pole frequencies. At high frequencies, $C_R(f)$ contributes systematic errors in the magnitude of ΔL_{free} [17].

IV.II. Actuation Function A(f;t)

The actuation function (see Figure 5) describes the physical actuators that spatially adjust the test masses hung in the quadruple pendulum (see Figure 1). The pendulum stages are labeled as follows: Top, Upper Intermediate, Penultimate, and Test. All except for the top stage are actuated upon and so contribute a term to the actuation function. The Upper-Intermediate and Penultimate masses have Optical Sensor and Electromagnetic (OSEM) actuators while the test mass, the mass that the laser light hits, has a ElectroStatic Drive (ESD) actuator. The ESD allows for finer spatial adjustments but can build up charge. Consequently, its strength changes with time.

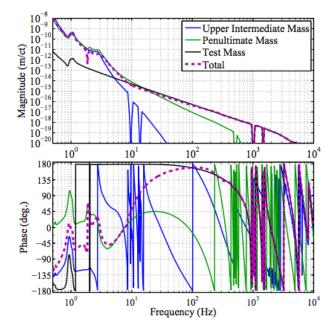


Fig. 5.— Figure from [15]. The actuation function A(f;t) shown in magnitude (top) and phase (bottom), includes the actuation functions for each pendulum stage. As frequency increases, the dominating pendulum stage progresses to the lower pendulum stages. Digital notch filters are apparent at select frequencies with the purpose of avoiding mechanical instabilities [15].

$$A(f;t) = \left[\kappa_T(t)A_T(f) + \kappa_P(t)A_P(f) + \kappa_P(t)A_U(f)\right]e^{-2\pi i f \tau_A}$$
(9)

 $\kappa_T(t):$ ESD actuation strength $\kappa_P(t):$ OSEM actuation strength $A_T(f):$ Test mass actuation function

 $A_P(f)$: Penultimate mass actuation function

 $A_U(f)$: Upper-Intermediate mass actuation function

 au_A : computational time delay in digital-to-analog conversion

Equation 7 indicates $R_e(f;t) \approx A(f;t)D(f)$ when |G(f;t)| >> 1. $A_T(f)$ is the dominant term in A(f;t) for frequencies greater than 20 Hz; the largest systematic errors contained in A(f;t) ($\pm 15\%$) are due to variations in the actuation strength of the ESD from 20-50 Hz and are contained in $\kappa_T(t)$ [17].

IV.III. Full Parametrization of the Response Function and Real-Time Calibration Measures

With our parameters from C(f;t) and A(f;t), we can rewrite our actuation function beginning with equation 7 and compensating for known time delays:

$$R_e(f;t) = \frac{1 + A(f;t)D(f)C(f;t)}{C(f;t)}$$
(10)

$$R_e(f;t) = \frac{1}{C(f;t)} + D(f)A(f;t)$$
 (11)

$$R_e(f;t) = \left(\frac{1 + if/f_{CC}(t)}{\kappa_C(t)C_R(f)}\right) + D(f)\left(\kappa_T(t)A_T(f) + \kappa_P(t)A_P(f)\kappa_P(t)A_U(f)\right)$$
(1)

The time dependent parameters $(\kappa_T(t), \kappa_P(t), \kappa_C(t), f_{CC}(t))$ are monitored for variation using intentional injections at four frequencies (called calibration lines) into the DARM spectrum throughout an observation run (see Table 2). The calibration lines reveal any short-term gain fluctuations in optical plant or actuation strengths.

TABLE 2 CALIBRATION LINE TABLE RECREATED FROM [17]. LINES 1-3 ARE USED TO ESTIMATE κ_T AND κ_P AND LINE 4 FOR κ_C AND f_c FOR THE LIGO HANFORD (H1) AND LIGO LIVINGSTON (L1) DETECTORS.

| # | Signal | Freq. | (Hz) | Line Purpose |
|---|-------------------|-------|-------|----------------------------------|
| | | H1. | L1 | - |
| 1 | x_T | 35.9 | 35.3 | ESD actuation strength |
| 2 | ΔL_{pcal} | 36.7 | 34.7 | DARM actuation |
| 3 | x_{ctrl} | 37.3 | 33.7 | Penultimate & Upper- |
| | | | | Intermediate actuation strengths |
| 4 | ΔL_{pcal} | 331.9 | 331.3 | Optical gain and coupled cavity |
| | | | | pole frequency |

The frequency dependent parameters in our response function $(A_U(f), A_P(f), A_T(f), C_R(f))$ are measured between observation runs using swept sine calibration; a sine wave displacement signal is applied to a test mass while the interferometer is locked. Then, the frequency is slowly swept over the GW detection band and the error signal is measured as a function of the displacement. This yields the closed loop transfer function.

The interpreted GW strain will be different from the true GW strain in both phase and amplitude. As discussed in Section III, this affects not only the precision measurement of astrophysical parameters like masses, sky location, distance, and etc, but also the precision measurement of universal parameters like those that describe variations from GR. To decrease the difference between the measured length function and the exact length function, we seek to better characterize aLIGO's CEs through Bayesian parameter estimation.

V. BAYESIAN PARAMETER ESTIMATION

We can compare a parametrized GW waveform model to the detected strain signal, using a matched filtering technique with template banks, further described in [6]. It is an accurate and time sensitive method to identify potential GWs from compact binary coalescence (CBC). Figure 2 shows the GW waveform model used for GW150914.

With the matched filtering results, we can construct probability density functions (PDFs) for each of the parameters in the GW detection. To be explicit, we begin with Bayes' theorem; the probability that a parameter, θ , is the correct value given some data, x, is equal to the probability of getting the data given the parameter times the prior probability that the parameter is the correct value, and divided by the evidence of the data:

$$P(\theta|x) = \frac{P(x|\theta) \times P(\theta)}{P(x)} \tag{13}$$

Here, $P(\theta|x)$ is the posterior probability, $P(x|\theta)$ is the likelihood, $P(\theta)$ the prior, and $P(x) = \int P(x|\theta)P(\theta)d\theta$ the evidence.

We can then express the probability that the strain data x(f) came from an astrophysical system with parameter θ with the log-likelihood, $\ln P(x|\theta)$:

$$\ln P(x|\theta) = -1/2 \int_0^\infty \frac{|h(f,\theta) - x(f)|^2}{S_{nn}(f)}$$
 (14)

where x(f) is the strain data from the detector, $h(f, \theta)$ is the GR prediction for the strain with parameter θ , and $S_{nn}(f)$ is the power spectral density of the detector's strain noise.

We can update this probability as more data becomes available. We can "stack" GW observations like so:

$$P(\theta|x,y) = \frac{P(x,y|\theta) \times P(\theta)}{P(x,y)}$$

$$= \frac{P(y|\theta,x) \times P(\theta|x)}{P(x,y)} \quad \text{Substitute in Eqn. 13}$$

$$= \frac{P(y|\theta) \times P(x|\theta) \times P(\theta)}{P(x)P(y)} \tag{15}$$

Assuming GWs are uncorrelated the probability of y does not depend on x

where $P(\theta|x,y)$ is the posterior probability that θ is the correct value given that x, our data or a GW detection, and y, new data or another GW detection, exist. The normalization constants of these models are typically ignored in favor of simply comparing two competing models. This model selection (rather than parameter estimation) involves taking the ratio (called the odds ratio) of posterior probabilities to the evidence/potential GW signal:

$$O_{i,j} = \frac{P(\mathcal{H}_i|x)}{P(\mathcal{H}_j|x)} B_{ij}$$
 (16)

where \mathcal{H}_i is some hypothesis and is compared to another hypothesis, \mathcal{H}_j . The Bayes factor or evidence ratio, B_{ij} , is the ratio of likelihoods between the models. It is often used as a statistic to describe confidence in the correctness of a model or to rank competing hypotheses given the observed data. From equation 15 we see that as we amass new GW detections we update the probability by multiplying the posterior probability distributions for θ for each event together. For an arbitrary number of detections, the probability of the parameter is then given by:

$$P(\theta|x_i) \propto \left[\prod_i P(x_i|\theta)\right] \times P(\theta)$$
 (17)

Stacking GW strain signals in this way can constrain parameter estimation better than a single detection can. For computational simplicity, we limit our model to one parameter.

VI. THE MODEL

Though up to 100's of observations per year are expected by the time LIGO operates at design sensitivity [3], only two GW detections have been published as of the time of this paper. For now, we use simulated GW

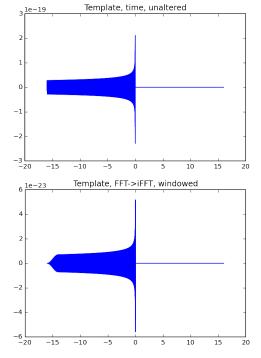


FIG. 6.— The unaltered GW151226 template (above), available from https://losc.ligo.org/s/events/GW151226/LOSC_Event_tutorial_GW151226.html, and the windowed template (below).

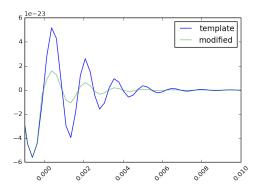
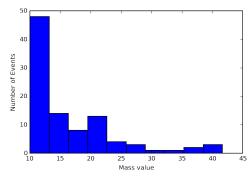


Fig. 7.— A smoothly damped ringdown

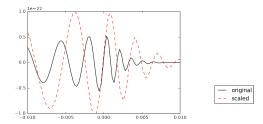
signals instead of real GW signals. GW waveform models are based on an analytical inspiral-merger-ringdown (IMR) model (see Figure 2)

Our model begins with the GW151226 template windowed with a Tukey/tapered cosine window to remove effects at the beginning and end of the template (See Figure 6). We modified a copy of the template to create the base for our mock data by smoothly decreasing the amplitude of the ringdown (see Figure 7) by 50% with a logistic function. This represents a possible non-GR deviation in our GW template. We then created 550 templates of these smoothly damped in ringdown templates in order to populate a template bank for match filtering. We additionally scaled these templates by mass, following a m⁻¹ power law from 5 to $45M_{\odot}$ (See Figures 8 and 9).

Returning to our original ringdown damped template, we added colored (frequency-dependent) noise to achieve a mock signal (see Figure 10). The mock signal strength



 ${\it Fig.}$ 8.— The mass distribution sampled from to scale the templates and generate mock data.



 ${\rm Fig.~9.--}$ A resulting scaled ringdown. Note that a higher total mass results in both a larger amplitude and oscillations with longer periods.

was chosen via sampling from an SNR^{-4} distribution (see Figure 11).

We then run our mock data through match filtering against our template bank to generate PDFs for the non-GR parameter for different SNRs, noting which templates were returned as the best fits (see Figure 12). Next, we stacked our observations by multiplying the posteriors (assuming a flat prior). After renormalizing the PDFs, we measured their variance to represent our uncertainty of the parameter measurement and plotted that uncertainty against the number of events stacked (see Figure 13)

VII. NEXT STEPS

The most immediate next step in this project is correcting the tapering of the waveform; we used a Tukey window to remove effects at the beginning and end of the template, though the end of the template already smoothly goes to zero. This may improve our results for lower SNR regimes.

The next priority is to run the model with more than 50 events and calculate the errors on the uncertainty measurements to see if the uncertainty reaches a constant value above 50 stacked events, as hinted by Figure 13.

Afterwards, adding a CE to the mock data representing optical gain uncertainty error along with a CE model would allow us to see if the non-GR deviation is recoverable. Repeating this for very low SNR (~ 10) would give us a more realistic representation of our ability to recover non-GR deviations in the face of CE errors. Once this is implemented, we can test ideas such as: What calibration accuracy do we need before statistical error dominates for one event? For hundreds of events? With a calibration error included, how well can we constrain that parameter? How well should we measure the parameter for N events?

The answers to such questions will inform us in

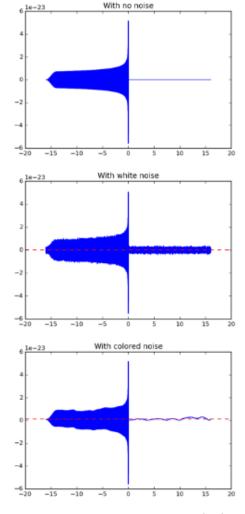
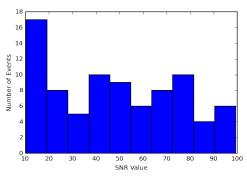


Fig. 10.— The original modified template (top) followed by the template with white/Gaussian noise (middle) and finally colored/frequency dependent noise (bottom).



 $\,$ Fig. 11.— The SNR distribution from which the SNR for our mock data was generated.

our estimation of the impact of aLIGO calibration uncertainty on precision tests of GR using observations of GWs from BBH mergers. Additionally, they will direct us to the most important questions to ask of more sophisticated models of calibration, such as that described in Section X.

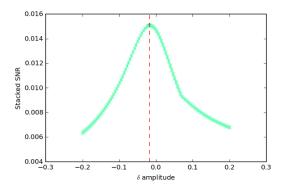


Fig. 12.— The SNR returned by the matched filtering function versus the deviation of the amplitude of the merger and ringdown with respect to the prediction from GR. The predicted amplitude is marked by the red dashed line.

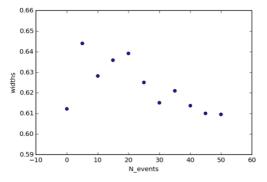


Fig. 13.— The uncertainty in the non-GR parameter measurement versus the number of events. It looks as if the uncertainty reaches a constant value above around 50 stacked events, but more runs would clarify the result. Next steps with this model include runs with more than 50 events and the calculation of errors on these uncertainty measurements.

We provided an overview of the calibration methods used for aLIGO and their uncertainties, describe how aLIGO detects GWs, and how CEs in the DARM closed feedback loop transfer function impact our detections. We presented a model that generates mock data, match filters, stacks observations, and uses Bayesian parameter estimation to begin to explore the effects of calibration uncertainty on precision tests of GR. We suggested next steps in the investigation, including the implementation of a frequency-dependent calibration error model and a more sophisticated model set up in Section X.

The first GW has only recently been detected; the universe as illustrated by GWs is an emerging perspective in astronomy. Observing things in the universe for the first time is exciting and impactful, but verification that the detection data are accurate is vital. Publishing uncertain/inaccurate detections can confuse and delay our understanding of the universe. Consequently, good calibrations of instrumentation is essential if we are to be confident about collected data and use it to understand how our universe works. Though only two GW detections have been observed, many more expect to be seen in the future. Analyzing our calibration uncertainties and their impact on important questions like the existence non-GR deviation now will help us prepare our instrumentation for the next leg of direct GW detection astronomy.

IX. ACKNOWLEDGMENTS

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X. APPENDIX

A more sophisticated investigation into the impact of CEs on precision tests of GR could use the the parameter estimation pipeline LALInference [18] and TIGER [5], a data analysis pipeline for testing the strong-field dynamics of GR with GW signals.

In this section, we outline astrophysical and calibration parameter estimation using LALInference and we describe the software signal injections used to mimic GR and non-GR conforming GW signals in TIGER.

LALInference compares a parametrized GW waveform model to the detected strain signal, using the matched filtering technique described in Section V. Section V. Using LALInference's results, we can construct PDFs for each of the parameters in the GW detection, and stack them to increase our SNR, as also described in described in V, but for all parameters instead of one.

However, Bayesian inference tends to be computationally expensive, especially with a large number of parameters (15 for the most simple compact binary merger models, excluding instrumental and calibration parameters, see Table 1). It additionally has complex multi-modal likelihood functions, and the computationally costly process of generating the model waveforms [18]. As a result, stochastic sampling techniques, like Markov Chain Monte Carlo (MCMC), Nested Sampling, and MultiNest/BAMBI, have been explored and developed for Bayesian inference for GW data and have been packaged into LALInference to speed up the process. This work could use the Nested Sampling routine LALInference_nest, for example.

CEs, as discussed previously, will introduce bias in the posterior distributions of the measured parameters. LALInference currently uses a spline-fitted CE model, but a new frequency-dependent CE model is being developed— a comparison between the effectiveness in parameter retrieval of two CE models is one possible next step.

TIGER could be used for generating the common non-GR parameter. TIGER (Test Infrastructure for GEneral Relativity) is a data analysis pipeline for model-independent testing the strong-field dynamics of general relativity with GW signals [5]. It relies on Bayesian model selection to combine information from multiple observations. It then compares the stacked data evidence between two hypotheses: a GW waveform model consistent with GR, H_{GR} , and a model with parametrized deformations of the GW waveform model, H_{modGR} , as given by additional parameters. TIGER uses an odds ratio to compare these models:

$$O_{GR}^{modGR} \equiv \frac{P(H_{modGR}|d,I)}{P(H_{GR}|d,I)} \tag{18}$$

where d is the data and I is our prior.

This method is considered model independent because

any/all of the additional parameters are allowed to vary

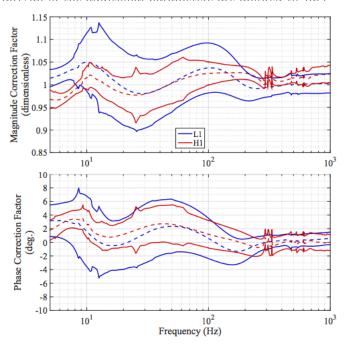


Fig. 14.— Figure from [15]. Differences in model and measured R(f;t) result in correction factors, $1+\delta R(f;t)/R(f;t)$, shown in magnitude (upper) and phase (lower). The dashed lines show the systematic errors, known from model parameters, and the solid lines the total statistical uncertainty [15]. This R(f;t) incorporates the frequency dependent calibration model that is being developed for LALInference. from zero (where they agree with GR) such that many

from zero (where they agree with GR) such that many different waveforms could be well fit. Each possible waveform is considered a sub-hypothesis and the Bayes factors for all of the sub-hypotheses can be merged into a single odds ratio with which to compare the GR consistent model.

Detector noise fluctuations can potentially mimic GR violations. To allay this, the odds ratio should be compared with a noisy background distribution; injecting many simulated GW signals with different astrophysical parameters into data surrounding the GW signal of interest can accomplish this [5]. The odds ratio can then be calculated for many GR consistent injections/noisy background sets. Then, a distribution of the odds ratio for GR consistent GWs can be calculated with an accompanying p-value. From this a threshold can be set for non-GR conforming GW model odds ratios to overcome.

For signal injections, LALInference_pipe, part of the LaLApps Suite [11], could be used. On such method could be to select a section of aLIGO data free of signals, undue noise, or other injections, and then add $\sim 50~\mathrm{GW}$ injections from systems with total masses of $10-50M_\odot$ and spins 0-0.99. A second set of these injections could be constructed to share a common non-GR parameter. This would allow us to estimate how many injections/detections are required to constrain a non-GR parameter if one exists.

This more sophisticated analysis would be a great follow-up to our introductory model, and would provide better insight to how limited aLIGO is in detecting small, non-GR deviations. Such a detection would indeed be a very important development in physics.

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