

Interferometer Techniques for Gravitational-Wave Detection

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Abstract

Several km-scale gravitational-wave detectors have been constructed world wide. These instruments combine a number of advanced technologies to push the limits of precision length measurement. The core devices are laser interferometers of a new kind; developed from the classical Michelson topology these interferometers integrate additional optical elements, which significantly change the properties of the optical system. Much of the design and analysis of these laser interferometers can be performed using well-known classical optical techniques; however, the complex optical layouts provide a new challenge. In this review we give a textbook-style introduction to the optical science required for the understanding of modern gravitational wave detectors, as well as other high-precision laser interferometers. In addition, we provide a number of examples for a freely available interferometer simulation software and encourage the reader to use these examples to gain hands-on experience with the discussed optical methods.

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1 Introduction

1.1 The scope and style of the review

The historical development of laser interferometers for application as gravitational-wave detectors [138] has involved the combination of relatively simple optical subsystems into more and more complex assemblies. The individual elements that compose the interferometers, including mirrors, beam splitters, lasers, modulators, various polarising optics, photo detectors and so forth, are individually well described by relatively simple, mostly-classical physics. Complexity arises from the combination of multiple mirrors, beam splitters etc. into optical cavity systems that have narrow resonant features, and the consequent requirement to stabilise relative separations of the various components to sub-wavelength accuracy, and indeed in many cases to very small fractions of a wavelength.

Thus, classical physics describes the interferometer techniques and the operation of current gravitational-wave detectors. However, we note that at signal frequencies above a couple of hundreds of Hertz, the sensitivity of current detectors is limited by the photon counting noise at the interferometer readout, also called shot-noise. The next generation systems such as Advanced LIGO [74, 92], Advanced Virgo [6] and KAGRA [150] are expected to operate in a regime where the quantum physics of both light and mirror motion couple to each other. Then, a rigorous quantum-mechanical description is certainly required. Sensitivity improvements beyond these ‘Advanced’ detectors necessitate the development of *non-classical* techniques; a comprehensive discussion of such techniques is provided in [55]. This review provides a brief introduction to quantum noise in Section 6 but otherwise focusses on the non-quantum aspects of interferometry that play an important role in overcoming other limits to current detectors, due to, for example, thermal effects and feedback control systems. At the same time these classical techniques will provide the means for implementing new, non-classical schemes and just remain as important as ever.

The optical components employed tend to behave in a linear fashion with respect to the optical field, i.e. nonlinear optical effects need hardly be considered. Indeed, almost all aspects of the design of laser interferometers are dealt with in the linear regime. Therefore the underlying mathematics is relatively simple and many standard techniques are available, including those that naturally allow numerical solution by computer models. Such computer models are in fact necessary as the exact solutions can become quite complicated even for systems of a few components. In practice, workers in the field rarely calculate the behaviour of the optical systems from first principles, but instead rely on various well-established numerical modelling techniques. An example of software that enables modelling of interferometers and their component systems is FINESSE [72, 70]. This was developed by some of us (AF, DB), has been validated in a wide range of situations, and was used to prepare the examples included in the present review.

The target readership we have in mind is the student or researcher who desires to get to grips with practical issues in the design of interferometers or component parts thereof. For that reason, this review consists of sections covering the basic physics and approaches to simulation, intermixed with some practical examples. To make this as useful as possible, the examples are intended to be realistic with sensible parameters reflecting typical application in gravitational wave detectors. The examples, prepared using FINESSE, are designed to illustrate the methods typically applied in designing gravitational wave detectors. We encourage the reader to obtain FINESSE and to follow the examples (see Appendix A).

1.2 Overview of the goals of interferometer design

Gravitational-wave detectors strive to pick out signals carried by passing gravitational waves from a background of self-generated noise. The principles of operation are set out at various points in the review, but in essence, the goal has been to prepare many photons, stored for as long as

practical in the ‘arms’ of a laser interferometer (traditionally the two arms are at right angles), so that tiny phase shifts induced by the gravitational waves form as large as possible a signal, when the light leaving the appropriate ‘port’ of the interferometer is detected and the resulting signal analysed.

The evolution of gravitational-wave detectors can be seen by following their development from prototypes and early observing systems towards the Advanced detectors, which are currently under construction, with the first scientific data taking of Advanced LIGO planned for this year. Starting from the simplest Michelson interferometer [67], then by the application of techniques to increase the number of photons stored in the arms: delay lines [89], Fabry-Perot arm cavities [65, 66] and power recycling [25, 60]. The final step in the development of classical interferometry was the inclusion of signal recycling [115, 88], which, among other effects, allows the signal from a gravitational-wave signal of approximately-known spectrum to be enhanced above the noise.

Reading out a signal from even the most basic interferometer requires minimising the coupling of local environmental effects to the detected output. Thus, the relative positions of all the components must be stabilised. This is commonly achieved by suspending the mirrors etc. as pendulums, often multi-stage pendulums in series, and then applying closed-loop control to maintain the desired operating condition. The careful engineering required to provide low-noise suspensions with the correct vibration isolation, and also low-noise actuation, is described in many works, for example, [35, 133, 22, 18]. As the interferometer optics become more complicated, the resonance conditions, i.e. the allowed combinations of inter-component path lengths required to allow the photon number in the interferometer arms to reach maximum, become more narrowly defined. It is likewise necessary to maintain angular alignment of all components, such that beams required to interfere are correctly co-aligned. Typically the beams need to be aligned within a small fraction (and sometimes a very small fraction) of the far-field diffraction angle, and the requirement can be in the low nano-radian range for km-scale detectors [125, 71]. Therefore, for each optical component there is typically one longitudinal (i.e. along the direction of light propagation), plus two angular degrees of freedom (pitch and yaw about the longitudinal axis). A complex interferometer can consist of up to around seven highly sensitive components and so there can be of order 20 degrees of freedom to be measured and controlled [5, 169].

Although the light fields are linear, the coupling between the position of a mirror and the complex amplitude of the detected light field typically shows strongly nonlinear dependence on mirror positions due to the sharp resonance features exhibited by cavity systems. However, the fields do vary linearly or at least smoothly close to the desired operating point. So, while well-understood linear control theory suffices to design the control system needed to maintain the optical configuration at its operating point, bringing the system to that operating condition is often a separate and more challenging nonlinear problem. In the current version of this work we consider only the linear aspects of sensing and control.

Control systems require actuators, and those employed are typically electrical-force transducers that act on the suspended optical components, either directly or – to provide enhanced noise rejection – at upper stages of multi-stage suspensions. The transducers are normally coil-magnet actuators, with the magnets on the moving part, or, less frequently, electrostatic actuators of varying design. The actuators are frequently regarded as part of the mirror suspension subsystem and are not discussed in the current work.

To give order to our review we consider the main physics describing the operation of the basic optical components (mirrors, beam splitters, modulators, etc.) required to construct interferometers. Although all of the relevant physics is generally well known and not new, we take it as a starting point that permits the introduction of notation and conventions. It is also true that the interferometry employed for gravitational-wave detection has a different emphasis than other interferometer applications. As a consequence, descriptions or examples of a number of crucial optical properties for gravitational wave detectors cannot be found in the literature.

The purpose of this review is especially to provide a coherent theoretical framework for describing such effects. With the basics established, it can be seen that the interferometer configurations that have been employed in gravitational-wave detection may be built up and simulated in a relatively straightforward manner.

1.3 Plane-wave analysis

The main optical systems of interferometric gravitational-wave detectors are designed such that all system parameters are well known and stable over time. The stability is achieved through a mixture of passive isolation systems and active feedback control. In particular, the light sources are some of the most stable, low-noise continuous-wave laser systems so that electromagnetic fields can be assumed to be essentially monochromatic. Additional frequency components can be modelled as small modulations (in amplitude or phase). The laser beams are well collimated, propagate along a well-defined optical axis and remain always very much smaller than the optical elements they interact with. Therefore, these beams can be described as *paraxial* and the well-known paraxial approximations can be applied.

It is useful to first derive a mathematical model based on monochromatic, scalar, plane waves. As it turns out, a more detailed model including the polarisation and the shape of the laser beam as well as multiple frequency components, can be derived as an extension to the plane-wave model. A plane electromagnetic wave is typically described by its electric field component:

The diagram shows the equation $\vec{E}(x, y, z, t) = E_0 \vec{e}_p \cos(\omega t - \vec{k}\vec{r} + \varphi)$ with several callouts in rounded rectangles:

- A callout above \vec{k} states: " \vec{k} gives the direction of the wave with $k = \omega/c$ ".
- A callout above \vec{e}_p states: "direction of polarisation".
- A callout above φ states: "phase offset".
- A callout below E_0 states: "field amplitude".
- A callout below ω states: " $\omega = 2\pi f$ is the angular frequency".

Figure 1.1

with E_0 as the (constant) field amplitude in V/m, \vec{e}_p the unit vector in the direction of polarisation, such as, for example, \vec{e}_y for \mathcal{S} -polarised light, ω the angular oscillation frequency of the wave, and $\vec{k} = \vec{e}_k \omega/c$ the wave vector pointing in the direction of propagation. The absolute phase φ only becomes meaningful when the field is superposed with other light fields.

In this document we will consider waves propagating along the optical axis given by the z -axis, so that $\vec{k}\vec{r} = kz$. For the moment we will ignore the polarisation and use scalar waves, which can be written as

$$E(z, t) = E_0 \cos(\omega t - kz + \varphi). \quad (1.1)$$

Further, in this document we use complex notation, i.e.

$$E = \Re \{E'\} \quad \text{with} \quad E' = E'_0 \exp(i(\omega t - kz)). \quad (1.2)$$

This has the advantage that the scalar amplitude and the phase φ can be given by one, now complex, amplitude $E'_0 = E_0 \exp(i\varphi)$. We will use this notation with complex numbers throughout. For clarity we will simply use the unprimed letters for the auxiliary field. In particular, we will use the letter E and also a and b to denote complex electric-field amplitudes. But remember that, for example, in $E = E_0 \exp(-ikz)$ neither E nor E_0 are physical quantities. Only the real part of E exists and deserves the name field amplitude.

1.4 Frequency domain analysis

In most cases we are either interested in the fields *at one particular location*, for example, on the surface of an optical element, or we want to know the fields at all places in the interferometer but *at one particular point in time*. The latter is usually true for the *steady state* approach: assuming that the interferometer is in a steady state, all solutions must be independent of time so that we can perform all computations at $t = 0$ without loss of generality. In that case, the scalar plane wave can be written as

$$E = E_0 \exp(-i k z). \tag{1.3}$$

The frequency domain is of special interest as numerical models of gravitational-wave detectors tend to be much faster to compute in the frequency domain than in the time domain.

2 Optical Components: Coupling of Field Amplitudes

When an electromagnetic wave interacts with an optical system, all of its parameters can be changed as a result. Typically optical components are designed such that, ideally, they only affect one of the parameters, i.e. either the amplitude *or* the polarisation *or* the shape. Therefore, it is convenient to derive separate descriptions concerning each parameter. This section introduces the coupling of the complex field amplitude at optical components. Typically, the optical components are described in the simplest possible way, as illustrated by the use of abstract schematics such as those shown in Figure 2.1.

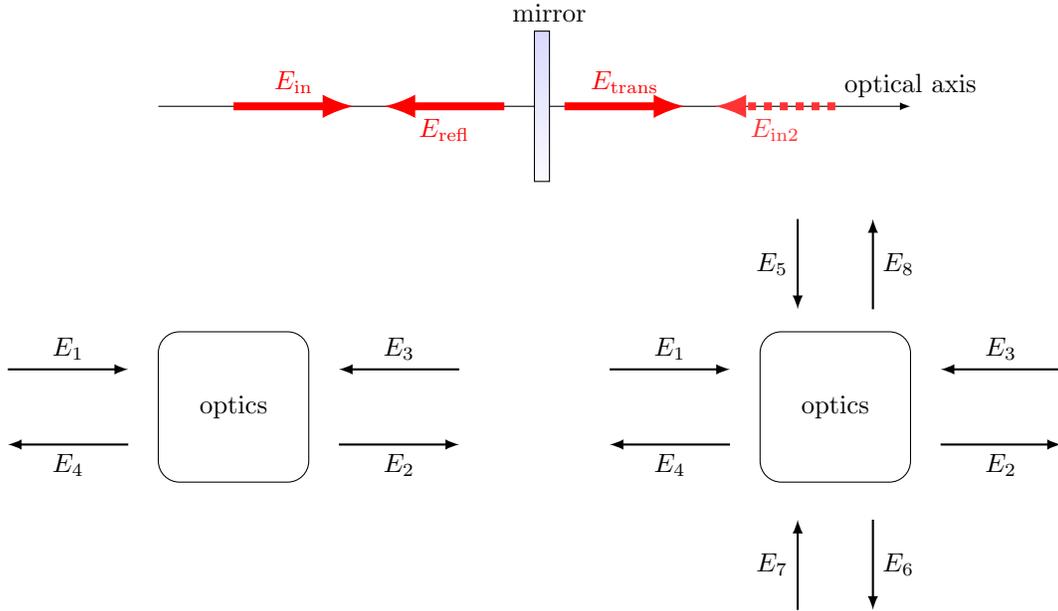


Figure 2.1: This set of figures introduces an abstract form of illustration, which will be used in this document. The top figure shows a typical example taken from the analysis of an optical system: an incident field E_{in} is reflected and transmitted by a semi-transparent mirror; there might be the possibility of second incident field $E_{\text{in}2}$. The lower left figure shows the abstract form we choose to represent the same system. The lower right figure depicts how this can be extended to include a beam splitter object, which connects two optical axes.

2.1 Mirrors and spaces: reflection, transmission and propagation

The core optical systems of current interferometric gravitational interferometers are composed of two building blocks: a) resonant optical cavities, such as Fabry-Perot resonators, and b) beam splitters, as in a Michelson interferometer. In other words, the laser beam is either propagated through a vacuum system or interacts with a partially-reflecting optical surface.

The term *optical surface* generally refers to a boundary between two media with possibly different indices of refraction n , for example, the boundary between air and glass or between two types of glass. A real fused silica mirror in an interferometer features two surfaces, which interact with a reflected or transmitted laser beam. However, in some cases, one of these surfaces has been treated with an anti-reflection (AR) coating to minimise the effect on the transmitted beam.

The terms *mirror* and *beam splitter* are sometimes used to describe a (theoretical) optical

surface in a model. We define real *amplitude coefficients* for reflection and transmission r and t , with $0 \leq r, t \leq 1$, so that the field amplitudes can be written as

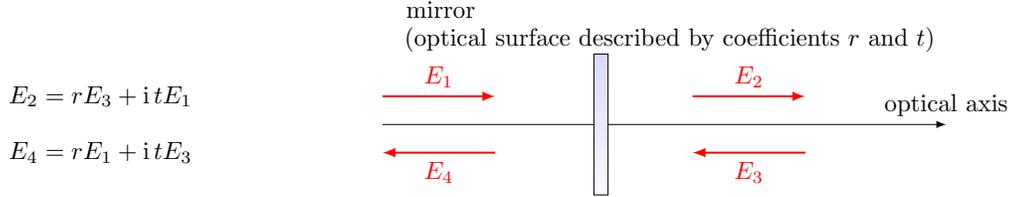


Figure 2.2

The $\pi/2$ phase shift upon transmission (here given by the factor i) refers to a phase convention explained in Section 2.4.

The free propagation of a distance D through a medium with index of refraction n can be described with the following set of equations:

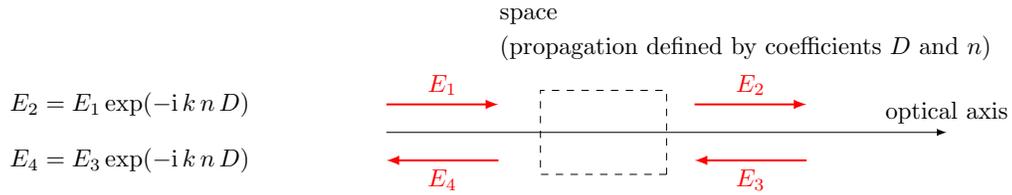


Figure 2.3

In the following we use $n = 1$ for simplicity.

Note that we use above relations to demonstrate various mathematical methods for the analysis of optical systems. However, refined versions of the coupling equations for optical components, including those for spaces and mirrors, are also required, see, for example, Section 2.6.

2.2 The two-mirror resonator

The linear optical resonator, also called a *cavity* is formed by two partially-transparent mirrors, arranged in parallel as shown in Figure 2.4. This simple setup makes a very good example with which to illustrate how a mathematical model of an interferometer can be derived, using the equations introduced in Section 2.1. A more detailed description of the two-mirror cavity is provided in Section 5.1.

The cavity is defined by a propagation length D (in vacuum), the amplitude reflectivities r_1 , r_2 and the amplitude transmittances t_1 , t_2 . The amplitude at each point in the cavity can be computed simply as the superposition of fields. The entire set of equations can be written as

$$\begin{aligned}
 a_1 &= it_1 a_0 + r_1 a'_3 \\
 a'_1 &= \exp(-ikD) a_1 \\
 a_2 &= it_2 a'_1 \\
 a_3 &= r_2 a'_1 \\
 a'_3 &= \exp(-ikD) a_3 \\
 a_4 &= r_1 a_0 + it_1 a'_3
 \end{aligned} \tag{2.1}$$

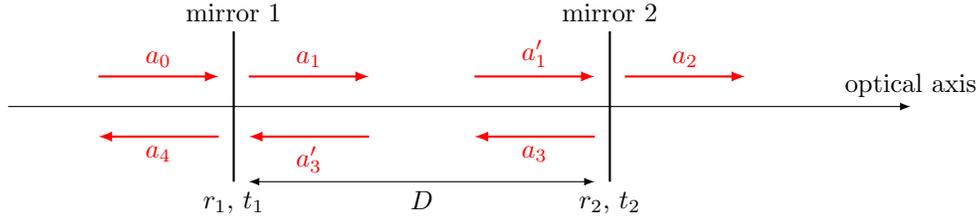


Figure 2.4: Simplified schematic of a two mirror cavity. The two mirrors are defined by the amplitude coefficients for reflection and transmission. Further, the resulting cavity is characterised by its length D . Light field amplitudes are shown and identified by a variable name, where necessary to permit their mutual coupling to be computed.

The circulating field impinging on the first mirror (surface) a'_3 can now be computed as

$$\begin{aligned} a'_3 &= \exp(-ikD) a_3 = \exp(-ikD) r_2 a'_1 = \exp(-i2kD) r_2 a_1 \\ &= \exp(-i2kD) r_2 (it_1 a_0 + r_1 a'_3). \end{aligned} \quad (2.2)$$

This then yields

$$a'_3 = a_0 \frac{ir_2 t_1 \exp(-i2kD)}{1 - r_1 r_2 \exp(-i2kD)}. \quad (2.3)$$

We can directly compute the reflected field to be

$$a_4 = a_0 \left(r_1 - \frac{r_2 t_1^2 \exp(-i2kD)}{1 - r_1 r_2 \exp(-i2kD)} \right) = a_0 \left(\frac{r_1 - r_2 (r_1^2 + t_1^2) \exp(-i2kD)}{1 - r_1 r_2 \exp(-i2kD)} \right), \quad (2.4)$$

while the transmitted field becomes

$$a_2 = a_0 \frac{-t_1 t_2 \exp(-ikD)}{1 - r_1 r_2 \exp(-i2kD)}. \quad (2.5)$$

The properties of two mirror cavities will be discussed in more detail in Section 5.1.

2.3 Coupling matrices

Computations that involve sets of linear equations as shown in Section 2.2 can often be done or written efficiently with matrices. Two methods of applying matrices to coupling field amplitudes are demonstrated below, using again the example of a two mirror cavity. First of all, we can rewrite the coupling equations in matrix form. The mirror coupling as given in Figure 2.2 becomes

$$\begin{pmatrix} a_2 \\ a_4 \end{pmatrix} = \begin{pmatrix} it & r \\ r & it \end{pmatrix} \begin{pmatrix} a_1 \\ a_3 \end{pmatrix}$$

Figure 2.5

and the amplitude coupling at a ‘space’, as given in Figure 2.3, can be written as

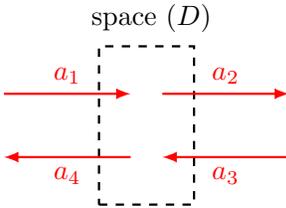
$$\begin{pmatrix} a_2 \\ a_4 \end{pmatrix} = \begin{pmatrix} \exp(-ikD) & 0 \\ 0 & \exp(-ikD) \end{pmatrix} \begin{pmatrix} a_1 \\ a_3 \end{pmatrix}$$


Figure 2.6

In these examples the matrix simply transforms the ‘known’ impinging amplitudes into the ‘unknown’ outgoing amplitudes.

Coupling matrices for numerical computations

An obvious application of the matrices introduced above would be to construct a large matrix for an extended optical system appropriate for computerisation. A very flexible method is to setup one equation for each field amplitude. The set of linear equations for a mirror would expand to

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ -it & 1 & -r & 0 \\ 0 & 0 & 1 & 0 \\ -r & 0 & -it & 1 \end{pmatrix} \begin{pmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \end{pmatrix} = \begin{pmatrix} a_1 \\ 0 \\ a_3 \\ 0 \end{pmatrix} = M_{\text{system}} \vec{a}_{\text{sol}} = \vec{a}_{\text{input}}, \quad (2.6)$$

where the input vector¹ \vec{a}_{input} has non-zero values for the impinging fields and \vec{a}_{sol} is the ‘solution’ vector, i.e. after solving the system of equations the amplitudes of the impinging as well as those of the outgoing fields are stored in that vector.

As an example we apply this method to the two mirror cavity. The system matrix for the optical setup shown in Figure 2.4 becomes

$$\begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ -it_1 & 1 & 0 & -r_1 & 0 & 0 & 0 \\ -r_1 & 0 & 1 & -it_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & -e^{-ikD} \\ 0 & -e^{-ikD} & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & -it_2 & 1 & 0 \\ 0 & 0 & 0 & 0 & -r_2 & 0 & 1 \end{pmatrix} \begin{pmatrix} a_0 \\ a_1 \\ a_4 \\ a'_3 \\ a'_1 \\ a_2 \\ a_3 \end{pmatrix} = \begin{pmatrix} a_0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad (2.7)$$

This is a *sparse* matrix. Sparse matrices are an important subclass of linear algebra problems and many efficient numerical algorithms for solving sparse matrices are freely available (see, for example, [58]). The advantage of this method of constructing a single matrix for an entire optical system is the direct access to all field amplitudes. It also stores each coupling coefficient in one or more dedicated matrix elements, so that numerical values for each parameter can be read out or changed after the matrix has been constructed and, for example, stored in computer memory. The obvious disadvantage is that the size of the matrix quickly grows with the number of optical elements (and with the degrees of freedom of the system, see, for example, Section 9).

¹ In many implementations of numerical matrix solvers the input vector is also called the *right-hand side* vector.

Coupling matrices for a compact system descriptions

The following method is probably most useful for analytic computations, or for optimisation aspects of a numerical computation. The idea behind the scheme, which is used for computing the characteristics of dielectric coatings [86, 112] and has been demonstrated for analysing gravitational wave detectors [124], is to rearrange equations as in Figure 2.5 and Figure 2.6 such that the overall matrix describing a series of components can be obtained by multiplication of the component matrices. In order to achieve this, the coupling equations have to be re-ordered so that the input vector consists of two field amplitudes *at one side of the component*. For the mirror, this gives a coupling matrix of

$$\begin{pmatrix} a_1 \\ a_4 \end{pmatrix} = \frac{i}{t} \begin{pmatrix} -1 & r \\ -r & r^2 + t^2 \end{pmatrix} \begin{pmatrix} a_2 \\ a_3 \end{pmatrix}. \quad (2.8)$$

In the special case of the lossless mirror this matrix simplifies as we have $r^2 + t^2 = R + T = 1$. The space component would be described by the following matrix:

$$\begin{pmatrix} a_1 \\ a_4 \end{pmatrix} = \begin{pmatrix} \exp(ikD) & 0 \\ 0 & \exp(-ikD) \end{pmatrix} \begin{pmatrix} a_2 \\ a_3 \end{pmatrix}. \quad (2.9)$$

With these matrices we can very easily compute a matrix for the cavity with two lossless mirrors as

$$M_{\text{cav}} = M_{\text{mirror1}} \times M_{\text{space}} \times M_{\text{mirror2}} \quad (2.10)$$

$$= \frac{-1}{t_1 t_2} \begin{pmatrix} e^+ - r_1 r_2 e^- & -r_2 e^+ + r_1 e^- \\ -r_2 e^- + r_1 e^+ & e^- - r_1 r_2 e^+ \end{pmatrix}, \quad (2.11)$$

with $e^+ = \exp(ikD)$ and $e^- = \exp(-ikD)$. The system of equation describing a cavity shown in Equation (2.1) can now be written more compactly as

$$\begin{pmatrix} a_0 \\ a_4 \end{pmatrix} = \frac{-1}{t_1 t_2} \begin{pmatrix} e^+ - r_1 r_2 e^- & -r_2 e^+ + r_1 e^- \\ -r_2 e^- + r_1 e^+ & e^- - r_1 r_2 e^+ \end{pmatrix} \begin{pmatrix} a_2 \\ 0 \end{pmatrix}. \quad (2.12)$$

This allows direct computation of the amplitude of the transmitted field resulting in

$$a_2 = a_0 \frac{-t_1 t_2 \exp(-ikD)}{1 - r_1 r_2 \exp(-i2kD)}, \quad (2.13)$$

which is the same as Equation (2.5).

The advantage of this matrix method is that it allows compact storage of any series of mirrors and propagations, and potentially other optical elements, in a single 2×2 matrix. The disadvantage inherent in this scheme is the lack of information about the field amplitudes inside the group of optical elements.

2.4 Phase relation at a mirror or beam splitter

The magnitude and phase of reflection at a single optical surface can be derived from Maxwell's equations and the electromagnetic boundary conditions at the surface, and in particular the condition that the field amplitudes tangential to the optical surface must be continuous. The results are called *Fresnel's equations* [96]. Thus, for a field impinging on an optical surface under normal incidence we can give the reflection coefficient as

$$r = \frac{n_1 - n_2}{n_1 + n_2}, \quad (2.14)$$

with n_1 and n_2 the indices of refraction of the first and second medium, respectively. The transmission coefficient for a lossless surface can be computed as $t^2 = 1 - r^2$. We note that the phase change upon reflection is either 0 or 180° , depending on whether the second medium is optically thinner or thicker than the first. It is not shown here but Fresnel's equations can also be used to show that the phase change for the transmitted light at a lossless surface is zero. This contrasts with the definitions given in Section 2.1 (see Figure (2.2)ff.), where the phase shift upon any reflection is defined as zero and the transmitted light experiences a phase shift of $\pi/2$. The following section explains the motivation for the latter definition having been adopted as the common notation for the analysis of modern optical systems.

Composite optical surfaces

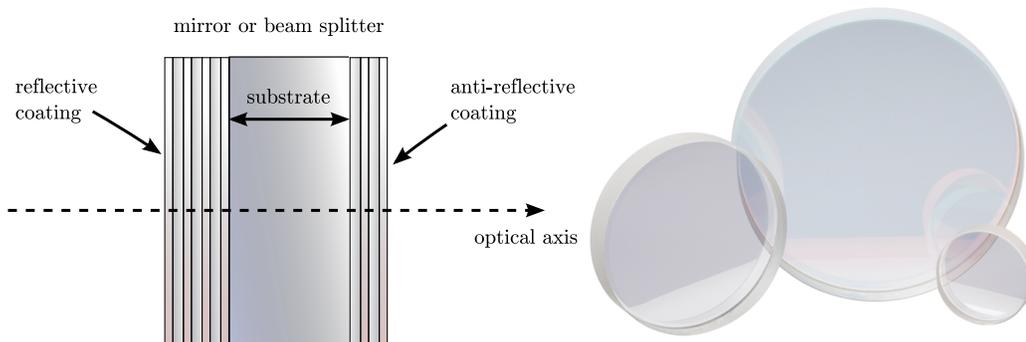


Figure 2.7: This sketch shows a mirror or beam splitter component with dielectric coatings and the photograph shows some typical commercially available examples [128]. Most mirrors and beam splitters used in optical experiments are of this type: a substrate made from glass, quartz or fused silica is coated on both sides. The *reflective coating* defines the overall reflectivity of the component (anything between $R \approx 1$ and $R \approx 0$, while the *anti-reflective coating* is used to reduce the reflection at the second optical surface as much as possible so that this surface does not influence the light. Please note that the drawing is not to scale, the coatings are typically only a few microns thick on a several millimetre to centimetre thick substrate.

Modern mirrors and beam splitters that make use of dielectric coatings are complex optical systems, see Figure 2.7 whose reflectivity and transmission depend on the multiple interference inside the coating layers and thus on microscopic parameters. The phase change upon transmission or reflection depends on the details of the applied coating and is typically not known. In any case, the knowledge of an absolute value of a phase change is typically not of interest in laser interferometers because the absolute positions of the optical components are not known to sub-wavelength precision. Instead the *relative* phase between the incoming and outgoing beams is of importance. In the following we demonstrate how constraints on these relative phases, i.e. the phase relation between the beams, can be derived from the fundamental principle of power conservation. To do this we consider a Michelson interferometer, as shown in Figure 2.8, with perfectly-reflecting mirrors. The beam splitter of the Michelson interferometer is the object under test. We assume that the magnitude of the reflection r and transmission t are known. The phase changes upon transmission and reflection are unknown. Due to symmetry we can say that the phase change upon transmission φ_t should be the same in both directions. However, the phase change on reflection might be different for either direction, thus, we write φ_{r1} for the reflection at the front and φ_{r2} for the reflection at the back of the beam splitter.

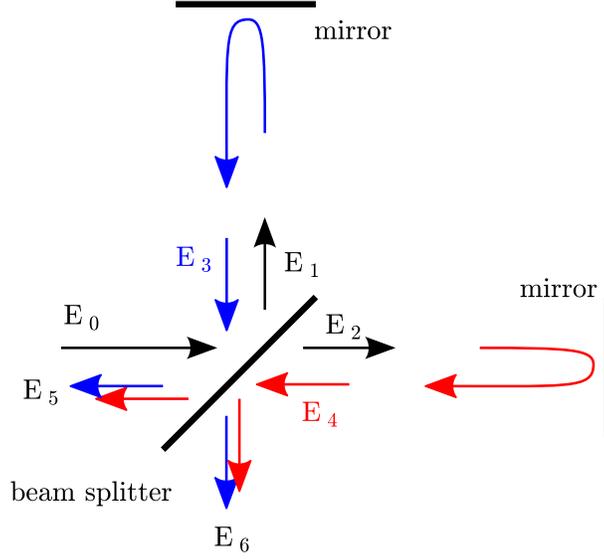


Figure 2.8: The relation between the phase of the light field amplitudes at a beam splitter can be computed assuming a Michelson interferometer, with arbitrary arm length but perfectly-reflecting mirrors. The incoming field E_0 is split into two fields E_1 and E_2 which are reflected at the end mirrors and return to the beam splitter, as E_3 and E_4 , to be recombined into two outgoing fields. These outgoing fields E_5 and E_6 are depicted by two arrows to highlight that these are the sum of the transmitted and reflected components of the returning fields. We can derive constraints for the phase of E_1 and E_2 with respect to the input field E_0 from the conservation of energy: $|E_0|^2 = |E_5|^2 + |E_6|^2$.

Then the electric fields can be computed as

$$E_1 = r E_0 e^{i\varphi_{r1}} ; \quad E_2 = t E_0 e^{i\varphi_t}. \quad (2.15)$$

We do not know the length of the interferometer arms. Thus, we introduce two further unknown phases: Φ_1 for the total phase accumulated by the field in the vertical arm and Φ_2 for the total phase accumulated in the horizontal arm. The fields impinging on the beam splitter compute as

$$E_3 = r E_0 e^{i(\varphi_{r1} + \Phi_1)} ; \quad E_4 = t E_0 e^{i(\varphi_t + \Phi_2)}. \quad (2.16)$$

The outgoing fields are computed as the sums of the reflected and transmitted components:

$$\begin{aligned} E_5 &= E_0 (R e^{i(2\varphi_{r1} + \Phi_1)} + T e^{i(2\varphi_t + \Phi_2)}) \\ E_6 &= E_0 r t (e^{i(\varphi_t + \varphi_{r1} + \Phi_1)} + e^{i(\varphi_t + \varphi_{r2} + \Phi_2)}), \end{aligned} \quad (2.17)$$

with $R = r^2$ and $T = t^2$.

It will be convenient to separate the phase factors into common and differential ones. We can write

$$E_5 = E_0 e^{i\alpha_+} (R e^{i\alpha_-} + T e^{-i\alpha_-}), \quad (2.18)$$

with

$$\alpha_+ = \varphi_{r1} + \varphi_t + \frac{1}{2}(\Phi_1 + \Phi_2) ; \quad \alpha_- = \varphi_{r1} - \varphi_t + \frac{1}{2}(\Phi_1 - \Phi_2), \quad (2.19)$$

and similarly

$$E_6 = E_0 r t e^{i\beta_+} 2 \cos(\beta_-), \quad (2.20)$$

with

$$\beta_+ = \varphi_t + \frac{1}{2} (\varphi_{r1} + \varphi_{r2} + \Phi_1 + \Phi_2) ; \quad \beta_- = \frac{1}{2} (\varphi_{r1} - \varphi_{r2} + \Phi_1 - \Phi_2). \quad (2.21)$$

For simplicity we now limit the discussion to a 50:50 beam splitter with $r = t = 1/\sqrt{2}$, for which we can simplify the field expressions even further:

$$E_5 = E_0 e^{i\alpha_+} \cos(\alpha_-) ; \quad E_6 = E_0 e^{i\beta_+} \cos(\beta_-). \quad (2.22)$$

Conservation of energy requires that $|E_0|^2 = |E_5|^2 + |E_6|^2$, which in turn requires

$$\cos^2(\alpha_-) + \cos^2(\beta_-) = 1, \quad (2.23)$$

which is only true if

$$\alpha_- - \beta_- = (2N + 1) \frac{\pi}{2}, \quad (2.24)$$

with N as in integer (positive, negative or zero). This gives the following constraint on the phase factors

$$\frac{1}{2} (\varphi_{r1} + \varphi_{r2}) - \varphi_t = (2N + 1) \frac{\pi}{2}. \quad (2.25)$$

One can show that exactly the same condition results in the case of arbitrary (lossless) reflectivity of the beam splitter [139].

We can test whether two known examples fulfil this condition. If the beam-splitting surface is the front of a glass plate we know that $\varphi_t = 0$, $\varphi_{r1} = \pi$, $\varphi_{r2} = 0$, which conforms with Equation (2.25). A second example is the two-mirror resonator, see Section 2.2. If we consider the cavity as an optical ‘black box’, it also splits any incoming beam into a reflected and transmitted component, like a mirror or beam splitter. Further we know that a symmetric resonator must give the same results for fields injected from the left or from the right. Thus, the phase factors upon reflection must be equal $\varphi_r = \varphi_{r1} = \varphi_{r2}$. The reflection and transmission coefficients are given by Equations (2.4) and (2.5) as

$$r_{\text{cav}} = \left(r_1 - \frac{r_2 t_1^2 \exp(-i 2kD)}{1 - r_1 r_2 \exp(-i 2kD)} \right), \quad (2.26)$$

and

$$t_{\text{cav}} = \frac{-t_1 t_2 \exp(-i kD)}{1 - r_1 r_2 \exp(-i 2kD)}. \quad (2.27)$$

We demonstrate a simple case by putting the cavity on resonance ($kD = N\pi$). This yields

$$r_{\text{cav}} = \left(r_1 - \frac{r_2 t_1^2}{1 - r_1 r_2} \right) ; \quad t_{\text{cav}} = \frac{i t_1 t_2}{1 - r_1 r_2}, \quad (2.28)$$

with r_{cav} being purely real and t_{cav} imaginary and thus $\varphi_t = \pi/2$ and $\varphi_r = 0$ which also agrees with Equation (2.25).

In most cases we neither know nor care about the exact phase factors. Instead we can pick any set which fulfils Equation (2.25). For this document we have chosen to use phase factors equal to those of the cavity, i.e. $\varphi_t = \pi/2$ and $\varphi_r = 0$, which is why we write the reflection and transmission at a mirror or beam splitter as

$$E_{\text{refl}} = r E_0 \quad \text{and} \quad E_{\text{trans}} = i t E_0. \quad (2.29)$$

In this definition r and t are positive real numbers satisfying $r^2 + t^2 = 1$ for the lossless case.

Please note that we only have the freedom to chose convenient phase factors when we do not know or do not care about the details of the optical system, which performs the beam splitting. If instead the details are important, for example, when computing the properties of a thin coating layer, such as anti-reflex coatings, the proper phase factors for the respective interfaces must be computed and used.

2.5 Lengths and tunings: numerical accuracy of distances

The resonance condition inside an optical cavity and the operating point of an interferometer depends on the optical path lengths modulo the laser wavelength, i.e. for light from an Nd:YAG laser length differences of less than $1 \mu\text{m}$ are of interest, not the full magnitude of the distances between optics. On the other hand, several parameters describing the general properties of an optical system, like the finesse or free spectral range of a cavity (see Section 5.1) depend on the macroscopic distance and do not change significantly when the distance is changed on the order of a wavelength. This illustrates that the distance between optical components might not be the best parameter to use for the analysis of optical systems. Furthermore, it turns out that in numerical algorithms the distance may suffer from rounding errors. Let us use the Virgo [163] arm cavities as an example to illustrate this. The cavity length is approximately 3 km, the wavelength is on the order of $1 \mu\text{m}$, the mirror positions are actively controlled with a precision of 1 pm and the detector sensitivity can be as good as 10^{-18} m, measured on ~ 10 ms timescales (i.e. many samples of the data acquisition rate). The floating point accuracy of common, fast numerical algorithms is typically not better than 10^{-15} . If we were to store the distance between the cavity mirrors as such a floating point number, the accuracy would be limited to 3 pm, which does not even cover the accuracy of the control systems, let alone the sensitivity.

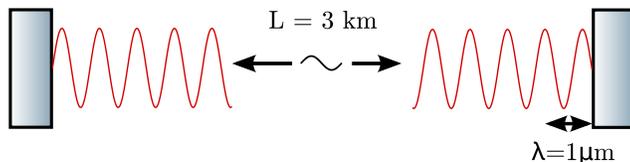


Figure 2.9: Illustration of an arm cavity of the Virgo gravitational-wave detector [163]: the macroscopic length L of the cavity is approximately 3 km, while the wavelength of the Nd:YAG laser is $\lambda \approx 1 \mu\text{m}$. The resonance condition is only affected by the microscopic position of the wave nodes with respect to the mirror surfaces and not by the macroscopic length, i.e. displacement of one mirror by $\Delta x = \lambda/2$ re-creates exactly the same condition. However, other parameters of the cavity, such as the finesse, only depend on the macroscopic length L and not on the microscopic tuning.

A simple and elegant solution to this problem is to split a distance D between two optical components into two parameters [87]: one is the macroscopic ‘length’ L , defined as the multiple of a constant wavelength λ_0 yielding the smallest difference to D . The second parameter is the microscopic *tuning* T that is defined as the remaining difference between L and D , i.e. $D = L + T$. Typically, λ_0 can be understood as the wavelength of the laser in vacuum, however, if the laser frequency changes during the experiment or multiple light fields with different frequencies are used simultaneously, a default constant wavelength must be chosen arbitrarily. Please note that usually the term λ in any equation refers to the actual wavelength at the respective location as $\lambda = \lambda_0/n$ with n the index of refraction at the local medium.

We have seen in Section 2.1 that distances appear in the expressions for electromagnetic waves

in connection with the wavenumber, for example,

$$E_2 = E_1 \exp(-i k z). \quad (2.30)$$

Thus, the difference in phase between the field at $z = z_1$ and $z = z_1 + D$ is given as

$$\varphi = -kD. \quad (2.31)$$

We recall that $k = 2\pi/\lambda = \omega/c$. We can define $\omega_0 = 2\pi c/\lambda_0$ and $k_0 = \omega_0/c$. For any given wavelength λ we can write the corresponding frequency as a sum of the default frequency and a difference frequency $\omega = \omega_0 + \Delta\omega$. Using these definitions, we can rewrite Equation (2.31) with length and tuning as

$$-\varphi = kD = \frac{\omega_0 L}{c} + \frac{\Delta\omega L}{c} + \frac{\omega_0 T}{c} + \frac{\Delta\omega T}{c}. \quad (2.32)$$

The first term of the sum is always a multiple of 2π , which is equivalent to zero. The last term of the sum is the smallest, approximately of the order $\Delta\omega \cdot 10^{-14}$. For typical values of $L \approx 1$ m, $T < 1$ μm and $\Delta\omega < 2\pi \cdot 100$ MHz we find that

$$\frac{\omega_0 L}{c} = 0, \quad \frac{\Delta\omega L}{c} \lesssim 2, \quad \frac{\omega_0 T}{c} \lesssim 6, \quad \frac{\Delta\omega T}{c} \lesssim 2 \cdot 10^{-6}, \quad (2.33)$$

which shows that the last term can often be ignored.

We can also write the tuning directly as a phase. We define as the dimensionless tuning

$$\phi = \omega_0 T / c. \quad (2.34)$$

This yields

$$\exp\left(i \frac{\omega}{c} T\right) = \exp\left(i \frac{\omega_0}{c} T \frac{\omega}{\omega_0}\right) = \exp\left(i \frac{\omega}{\omega_0} \phi\right). \quad (2.35)$$

The tuning ϕ is given in radian with 2π referring to a microscopic distance of one wavelength² λ_0 .

Finally, we can write the following expression for the phase difference between the light field taken at the end points of a distance D :

$$\varphi = -kD = -\left(\frac{\Delta\omega L}{c} + \phi \frac{\omega}{\omega_0}\right), \quad (2.36)$$

or if we neglect the last term from Equation (2.33) we can approximate ($\omega/\omega_0 \approx 1$) to obtain

$$\varphi \approx -\left(\frac{\Delta\omega L}{c} + \phi\right). \quad (2.37)$$

This convention provides two parameters L and ϕ , that can describe distances with a markedly improved numerical accuracy. In addition, this definition often allows simplification of the algebraic notation of interferometer signals. By convention we associate a length L with the propagation through free space, whereas the tuning will be treated as a parameter of the optical components. Effectively the tuning then represents a microscopic *displacement* of the respective component. If, for example, a cavity is to be resonant to the laser light, the tunings of the mirrors have to be the same whereas the length of the space in between can be arbitrary.

² Note that in other publications the tuning or equivalent microscopic displacements are sometimes defined via an optical path-length difference. In that case, a tuning of 2π is used to refer to the change of the optical path length of one wavelength, which, for example, if the reflection at a mirror is described, corresponds to a change of the mirror's position of $\lambda_0/2$.

2.6 Revised coupling matrices for space and mirrors

Using the definitions for length and tunings we can rewrite the coupling equations for mirrors and spaces introduced in Section 2.1 as follows. The mirror coupling becomes

$$\begin{pmatrix} a_2 \\ a_4 \end{pmatrix} = \begin{pmatrix} it & r \exp(i2\phi \frac{\omega}{\omega_0}) \\ r \exp(-i2\phi \frac{\omega}{\omega_0}) & it \end{pmatrix} \begin{pmatrix} a_1 \\ a_3 \end{pmatrix}$$

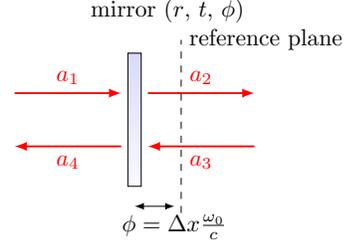


Figure 2.10

(compare this to Figure 2.5), and the amplitude coupling for a ‘space’, formally written as in Figure 2.6, is now written as

$$\begin{pmatrix} a_2 \\ a_4 \end{pmatrix} = \begin{pmatrix} \exp(-i\Delta knL) & 0 \\ 0 & \exp(-i\Delta knL) \end{pmatrix} \begin{pmatrix} a_1 \\ a_3 \end{pmatrix}$$

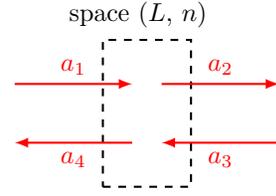


Figure 2.11

2.7 Finesse examples

2.7.1 Mirror reflectivity and transmittance

We use FINESSE to plot the amplitudes of the light fields transmitted and reflected by a mirror (given by a single surface). Initially, the mirror has a power reflectance and transmittance of $R = T = 0.5$ and is, thus, lossless. For the plot in Figure 2.12 we tune the transmittance from 0.5 to 0. Since we do not explicitly change the reflectivity, R remains at 0.5 and the mirror loss increases instead, which is shown by the trace labelled ‘total’ corresponding to the sum of the reflected and transmitted light power. The plot also shows the phase convention of a 90° phase shift for the transmitted light.

Finesse input file for ‘Mirror reflectivity and transmittance’

```
laser l1 1 0 n1 % laser with P=1W at the default frequency
space s1 1 n1 n2 % space of 1m length
mirror m1 0.5 0.5 0 n2 n3 % mirror with T=R=0.5 at zero tuning
ad ad_t 0 n3 % an ‘amplitude’ detector for transmitted light
ad ad_r 0 n2 % an ‘amplitude’ detector for reflected light
set t ad_t abs
set r ad_r abs
func total = $r^2 + $t^2 % computing the sum of the reflected and transmitted power
```

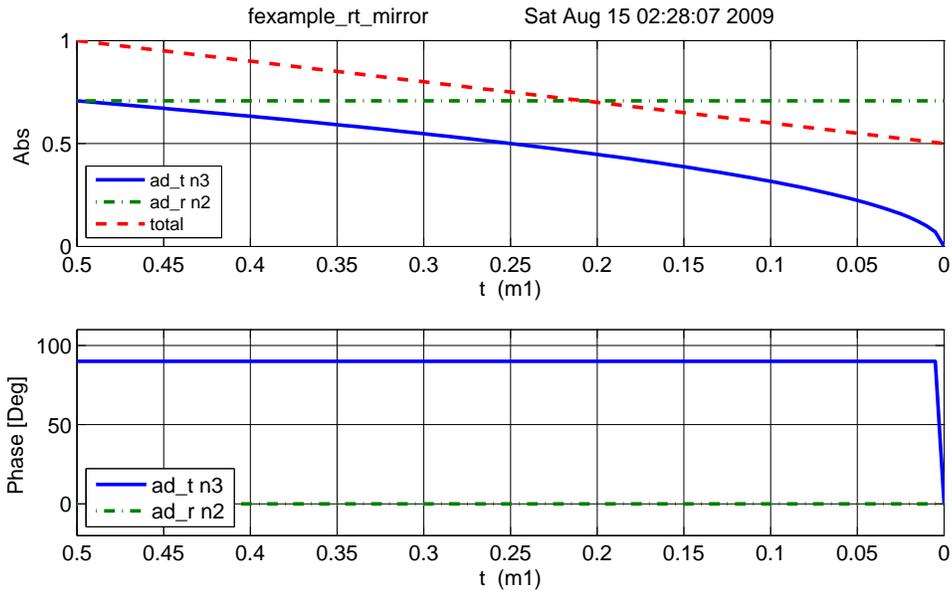


Figure 2.12: FINESSE example: Mirror reflectivity and transmittance.

```

xaxis m1 t lin 0.5 0 100 % changing the transmittance of the mirror 'm1'
yaxis abs:deg % plotting amplitude and phase of the results

```

2.7.2 Length and tunings

These FINESSE files demonstrate the conventions for lengths and microscopic positions introduced in Section 2.5. The top trace in Figure 2.13 depicts the phase change of a beam reflected by a beam splitter as the function of the beam splitter tuning. By changing the tuning from 0 to 180° the beam splitter is moved forward and shortens the path length by one wavelength, which by convention increases the light phase by 360° . On the other hand, if a length of a space is changed, the phase of the transmitted light is unchanged (for the default wavelength $\Delta k = 0$), as shown in the lower trace.

Finesse input files for ‘Length and tunings’

File for top trace:

```

laser l1 1 0 n1 % laser with P=1W at the default frequency
space s1 1 1 n1 n2 % space of 1m length
bs b1 1 0 0 n2 n3 dump dump % beam splitter as 'turning mirror', normal incidence
space s2 1 1 n3 n4 % another space of 1m length
ad ad1 0 n4 % amplitude detector
% 1) first trace: change microscopic position of beamsplitter
xaxis b1 phi lin 0 180 100
yaxis deg % plotting the phase of the results

```

File for bottom trace:

```

laser l1 1 0 n1 % laser with P=1W at the default frequency
space s1 1 1 n1 n2 % space of 1m length

```

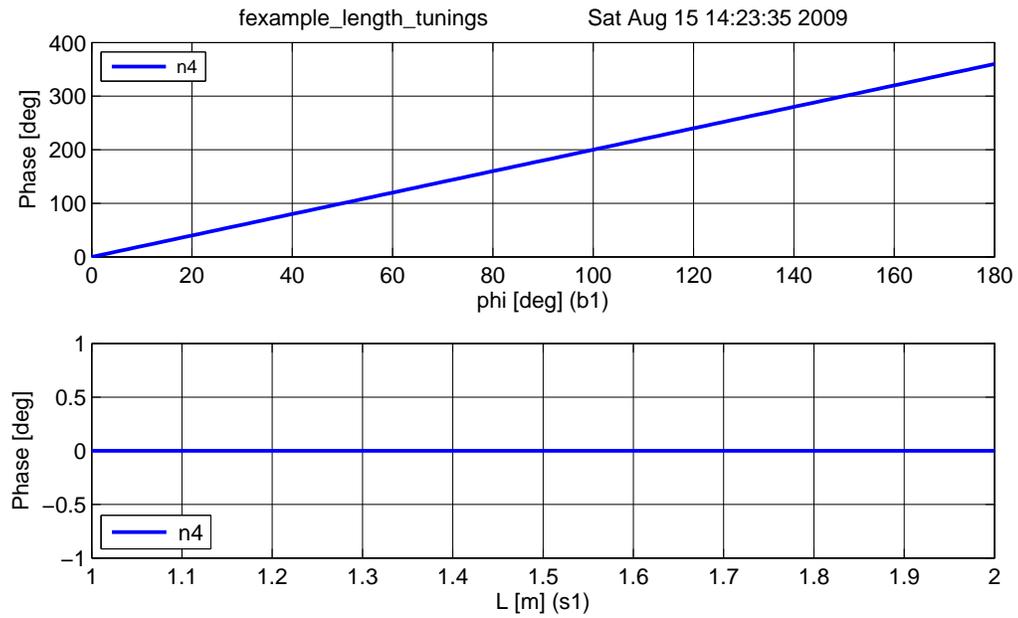


Figure 2.13: FINESSE example: Length and tunings.

```

bs      b1 1 0 0 0 n2 n3 dump dump % beam splitter as 'turning mirror', normal incidence
space   s2 1 1 n3 n4 % another space of 1m length
ad      ad1 0 n4      % amplitude detector
% second trace: change length of space s1
xaxis   s1 L lin 1 2 100
yaxis   deg      % plotting the phase of the results

```

3 Light with Multiple Frequency Components

So far we have considered the electromagnetic field to be monochromatic. This has allowed us to compute light-field amplitudes in a quasi-static optical setup. In this section, we introduce the frequency of the light as a new degree of freedom. In fact, we consider a field consisting of a finite and discrete number of frequency components. We write this as

$$E(t, z) = \sum_j a_j \exp(i(\omega_j t - k_j z)), \quad (3.1)$$

with complex amplitude factors a_j , ω_j as the angular frequency of the light field and $k_j = \omega_j/c$. In many cases the analysis compares different fields at one specific location only, in which case we can set $z = 0$ and write

$$E(t) = \sum_j a_j \exp(i\omega_j t). \quad (3.2)$$

In the following sections the concept of light modulation is introduced. As this inherently involves light fields with multiple frequency components, it makes use of this type of field description. Again we start with the two-mirror cavity to illustrate how the concept of modulation can be used to model the effect of mirror motion.

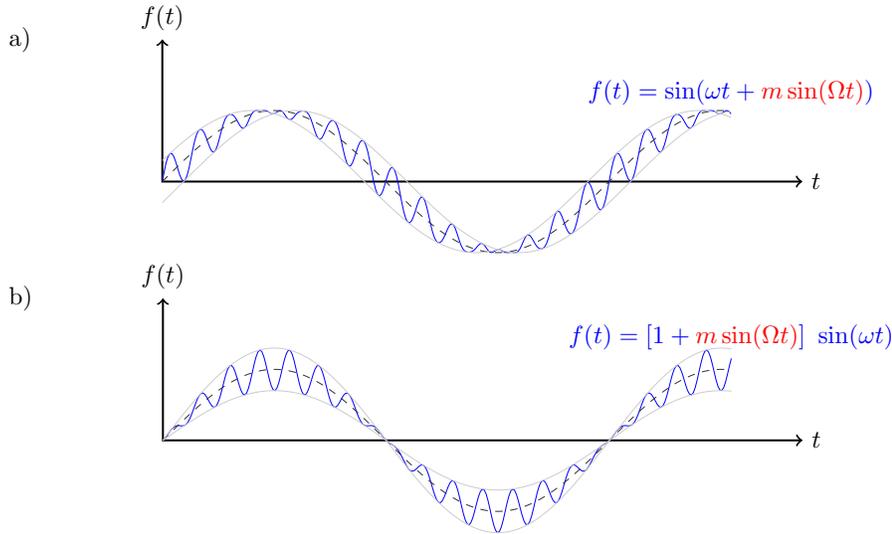


Figure 3.1: Example traces for phase and amplitude modulation: the upper plot a) shows a phase-modulated sine wave and the lower plot b) depicts an amplitude-modulated sine wave. Phase modulation is characterised by the fact that it mostly affects the zero crossings of the sine wave. Amplitude modulation affects mostly the maximum amplitude of the wave. The equations show the modulation terms in red with m the modulation index and Ω the modulation frequency.

3.1 Modulation of light fields

Laser interferometers typically use three different types of light fields: the laser with a frequency of, for example, $f \approx 2.8 \cdot 10^{14}$ Hz, *radio frequency* (RF) sidebands used for interferometer control with frequencies (offset to the laser frequency) of $f \approx 1 \cdot 10^6$ to $150 \cdot 10^6$ Hz, and the *signal* sidebands at frequencies of 1 to 10,000 Hz³. As these modulations usually have as their origin a change in

³ The signal sidebands are sometimes also called *audio sidebands* because of their frequency range.

optical path length, they are often phase modulations of the laser frequency, the RF sidebands are utilised for optical readout purposes, while the signal sidebands carry the signal to be measured (the gravitational-wave signal plus noise created in the interferometer).

Figure 3.1 shows a *time domain* representation of an electromagnetic wave of frequency ω_0 , whose amplitude or phase is modulated at a frequency Ω . One can easily see some characteristics of these two types of modulation, for example, that amplitude modulation leaves the zero crossing of the wave unchanged whereas with phase modulation the maximum and minimum amplitude of the wave remains the same. In the *frequency domain* in which a modulated field is expanded into several unmodulated field components, the interpretation of modulation becomes even easier: any sinusoidal modulation of amplitude or phase generates new field components, which are shifted in frequency with respect to the initial field. Basically, light power is shifted from one frequency component, the *carrier*, to several others, the *sidebands*. The relative amplitudes and phases of these sidebands differ for different types of modulation and different modulation strengths. This section demonstrates how to compute the sideband components for amplitude, phase and frequency modulation.

3.2 Phase modulation

Phase modulation can create a large number of sidebands. The number of sidebands with noticeable power depends on the modulation strength (or depth) given by the *modulation index* m . Assuming an input field

$$E_{\text{in}} = E_0 \exp(i\omega_0 t), \quad (3.3)$$

a sinusoidal phase modulation of the field can be described as

$$E = E_0 \exp\left(i(\omega_0 t + m \cos(\Omega t))\right). \quad (3.4)$$

This equation can be expanded using the identity [80]

$$\exp(iz \cos \varphi) = \sum_{k=-\infty}^{\infty} i^k J_k(z) \exp(ik\varphi), \quad (3.5)$$

with *Bessel functions of the first kind* $J_k(m)$. We can write

$$E = E_0 \exp(i\omega_0 t) \sum_{k=-\infty}^{\infty} i^k J_k(m) \exp(ik\Omega t). \quad (3.6)$$

The field for $k = 0$, oscillating with the frequency of the input field ω_0 , represents the carrier. The sidebands can be divided into *upper* ($k > 0$) and *lower* ($k < 0$) sidebands. These sidebands are light fields that have been shifted in frequency by $k\Omega$. The upper and lower sidebands with the same absolute value of k are called a pair of sidebands of order k . Equation (3.6) shows that the carrier is surrounded by an infinite number of sidebands. However, for small modulation indices ($m < 1$) the Bessel functions rapidly decrease with increasing k (the lowest orders of the Bessel functions are shown in Figure 3.2). For small modulation indices we can use the approximation [3]

$$J_k(m) = \left(\frac{m}{2}\right)^k \sum_{n=0}^{\infty} \frac{\left(-\frac{m^2}{4}\right)^n}{n!(k+n)!} = \frac{1}{k!} \left(\frac{m}{2}\right)^k + O(m^{k+2}). \quad (3.7)$$

In which case, only a few sidebands have to be taken into account. For $m \ll 1$ we can write

$$E = E_0 \exp(i\omega_0 t) \times \left(J_0(m) - i J_{-1}(m) \exp(-i\Omega t) + i J_1(m) \exp(i\Omega t) \right), \quad (3.8)$$

and with

$$J_{-k}(m) = (-1)^k J_k(m), \quad (3.9)$$

we obtain

$$E = E_0 \exp(i\omega_0 t) \left(1 + i \frac{m}{2} \left(\exp(-i\Omega t) + \exp(i\Omega t) \right) \right), \quad (3.10)$$

as the first-order approximation in m . In the above equation the carrier field remains unchanged by the modulation, therefore this approximation is not the most intuitive. It is clearer if the approximation up to the second order in m is given:

$$E = E_0 \exp(i\omega_0 t) \left(1 - \frac{m^2}{4} + i \frac{m}{2} \left(\exp(-i\Omega t) + \exp(i\Omega t) \right) \right), \quad (3.11)$$

which shows that power is transferred from the carrier to the sideband fields.

Higher-order expansions in m can be performed simply by specifying the highest order of Bessel function, which is to be used in the sum in Equation (3.6), i.e.

$$E = E_0 \exp(i\omega_0 t) \sum_{k=-order}^{order} i^k J_k(m) \exp(ik\Omega t). \quad (3.12)$$

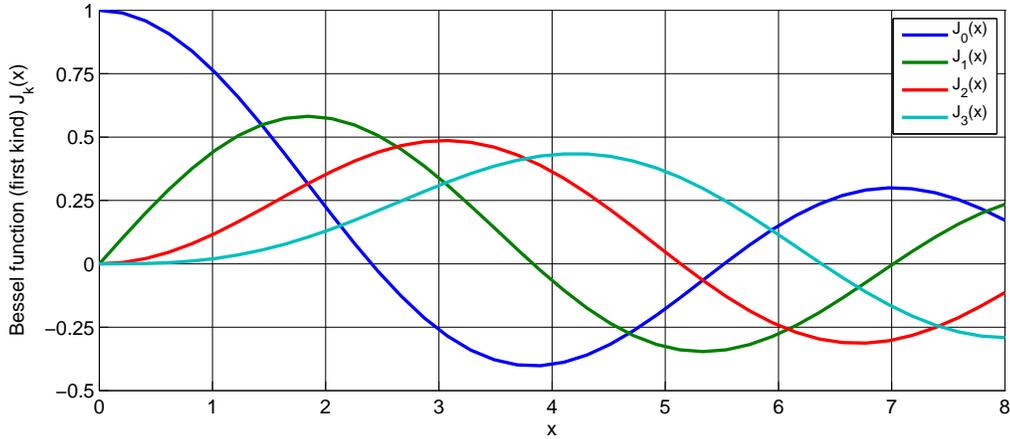


Figure 3.2: Some of the lowest-order Bessel functions $J_k(x)$ of the first kind. For small x the expansion shows a simple x^k dependency and higher-order functions can often be neglected.

3.3 Frequency modulation

For small modulation, indices, phase modulation and frequency modulation can be understood as different descriptions of the same effect [87]. Following the same spirit as above we would assume a modulated frequency to be given by

$$\omega = \omega_0 + m' \cos(\Omega t), \quad (3.13)$$

and then we might be tempted to write

$$E = E_0 \exp\left(i(\omega_0 + m' \cos(\Omega t))t\right), \quad (3.14)$$

which would be wrong. The frequency of a wave is actually defined as $\omega/(2\pi) = f = d\varphi/dt$. Thus, to obtain the frequency given in Equation (3.13), we need to have a phase of

$$\omega_0 t + \frac{m'}{\Omega} \sin(\Omega t). \quad (3.15)$$

For consistency with the notation for phase modulation, we define the modulation index to be

$$m = \frac{m'}{\Omega} = \frac{\Delta\omega}{\Omega}, \quad (3.16)$$

with $\Delta\omega$ as the frequency swing – how *far* the frequency is shifted by the modulation – and Ω the modulation frequency – how *fast* the frequency is shifted. Thus, a sinusoidal frequency modulation can be written as

$$E = E_0 \exp(i\varphi) = E_0 \exp\left(i\left(\omega_0 t + \frac{\Delta\omega}{\Omega} \cos(\Omega t)\right)\right), \quad (3.17)$$

which is exactly the same expression as Equation (3.4) for phase modulation. The practical difference is the typical size of the modulation index, with phase modulation having a modulation index of $m < 10$, while for frequency modulation, typical numbers might be $m > 10^4$. Thus, in the case of frequency modulation, the approximations for small m are not valid. The series expansion using Bessel functions, as in Equation (3.6), can still be performed; however, very many terms of the resulting sum need to be taken into account.

3.4 Amplitude modulation

In contrast to phase modulation, (sinusoidal) amplitude modulation always generates exactly two sidebands. Furthermore, a natural maximum modulation index exists: the modulation index is defined to be one ($m = 1$) when the amplitude is modulated between zero and the amplitude of the unmodulated field.

If the amplitude modulation is performed by an active element, for example by modulating the current of a laser diode, the following equation can be used to describe the output field:

$$\begin{aligned} E &= E_0 \exp(i\omega_0 t) \left(1 + m \cos(\Omega t)\right) \\ &= E_0 \exp(i\omega_0 t) \left(1 + \frac{m}{2} \exp(i\Omega t) + \frac{m}{2} \exp(-i\Omega t)\right). \end{aligned} \quad (3.18)$$

However, passive amplitude modulators (like acousto-optic modulators or electro-optic modulators with polarisers) can only reduce the amplitude. In these cases, the following equation is more useful:

$$\begin{aligned} E &= E_0 \exp(i\omega_0 t) \left(1 - \frac{m}{2} (1 - \cos(\Omega t))\right) \\ &= E_0 \exp(i\omega_0 t) \left(1 - \frac{m}{2} + \frac{m}{4} \exp(i\Omega t) + \frac{m}{4} \exp(-i\Omega t)\right). \end{aligned} \quad (3.19)$$

3.5 Sidebands as phasors in a rotating frame

A common method of visualising the behaviour of sideband fields in interferometers is to use *phase diagrams* in which each field amplitude is represented by an arrow in the complex plane.

We can think of the electric field amplitude $E_0 \exp(i\omega_0 t)$ as a vector in the complex plane, rotating around the origin with angular velocity ω_0 . To illustrate or to help visualise the addition of several light fields it can be useful to look at this problem using a *rotating reference frame*,

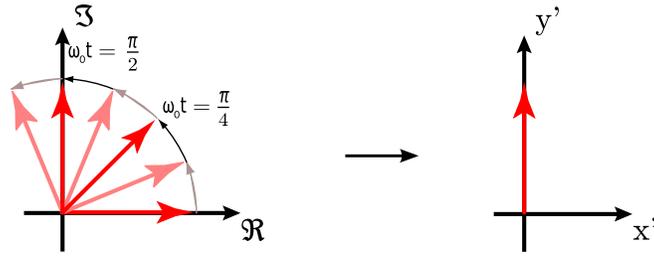


Figure 3.3: Electric field vector $E_0 \exp(i\omega_0 t)$ depicted in the complex plane and in a rotating frame (x', y') rotating at ω_0 so that the field vector appears stationary.

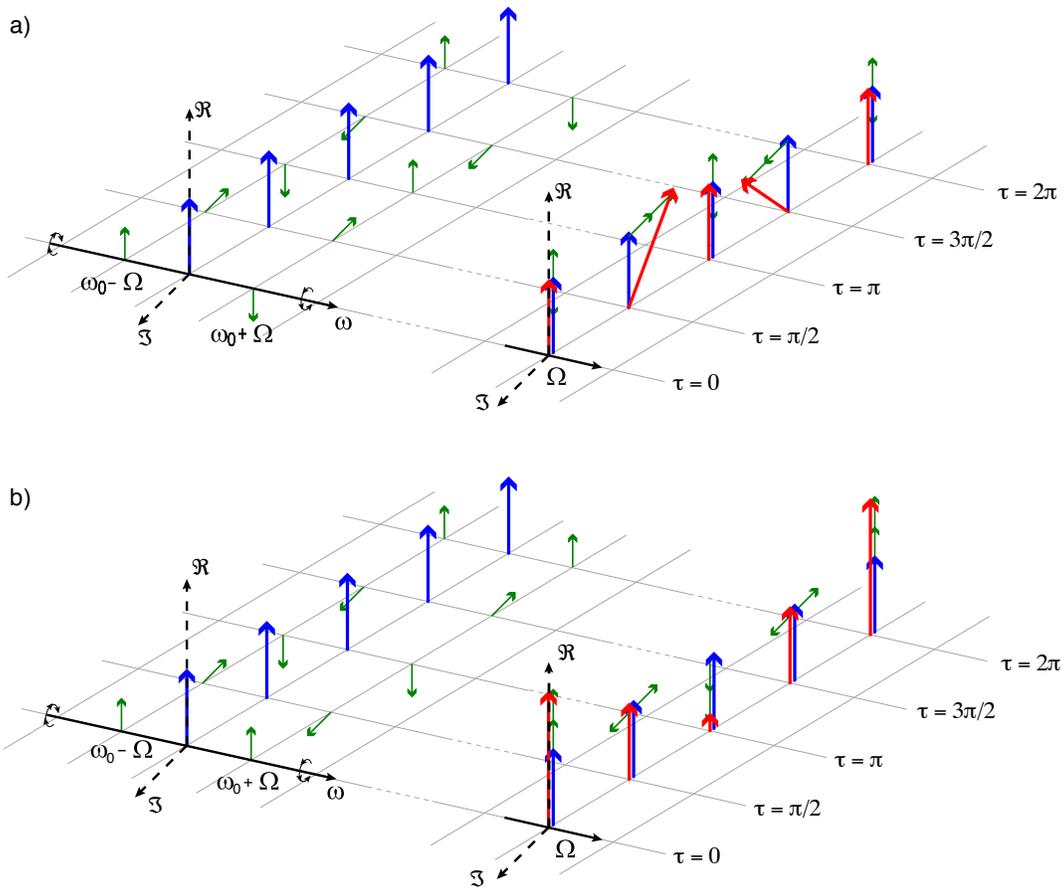


Figure 3.4: Amplitude and phase modulation in the ‘phasor’ picture. The upper plots a) illustrate how a phasor diagram can be used to describe phase modulation, while the lower plots b) do the same for amplitude modulation. In both cases the left hand plot shows the carrier in blue and the modulation sidebands in green as snapshots at certain time intervals. One can see clearly that the upper sideband ($\omega_0 + \Omega$) rotates faster than the carrier, while the lower sideband rotates slower. The right plot in both cases shows how the total field vector at any given time can be constructed by adding the three field vectors of the carrier and sidebands. [Drawing courtesy of Simon Chelkowski]

defined as follows. A complex number shall be defined as $z = x + iy$ so that the real part is plotted along the x -axis, while the y -axis is used for the imaginary part. We want to construct a new coordinate system (x', y') in which the field vector is at a constant position. This can be achieved by defining

$$\begin{aligned} x &= x' \cos \omega_0 t - y' \sin \omega_0 t \\ y &= x' \sin \omega_0 t + y' \cos \omega_0 t, \end{aligned} \quad (3.20)$$

or

$$\begin{aligned} x' &= x \cos(-\omega_0 t) - y \sin(-\omega_0 t) \\ y' &= x \sin(-\omega_0 t) + y \cos(-\omega_0 t). \end{aligned} \quad (3.21)$$

Figure 3.3 illustrates how the transition into the rotating frame makes the field vector to appear stationary. The angle of the field vector in a rotating frame depicts the phase offset of the field. Therefore these vectors are also called *phasors* and the illustrations using phasors are called *phasor diagrams*. Two more complex examples of how phasor diagrams can be employed is shown in Figure 3.4 [48].

Phasor diagrams can be especially useful to see how frequency coupling of light field amplitudes can change the type of modulation, for example, to turn phase modulation into amplitude modulation. An extensive introduction to this type of phasor diagram can be found in [109].

3.6 Phase modulation through a moving mirror

Several optical components can modulate transmitted or reflected light fields. In this section we discuss in detail the example of phase modulation by a moving mirror. Mirror motion does not change the transmitted light; however, the phase of the reflected light will be changed as shown in Equation (2.10).

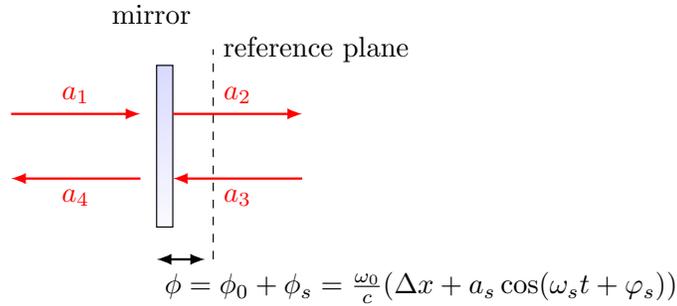


Figure 3.5: A sinusoidal signal with amplitude a_s frequency ω_s and phase offset φ_s is applied to a mirror position, or to be precise, to the mirror tuning. The equation given for the tuning ϕ assumes that $\omega_s/\omega_0 \ll 1$, see Section 2.5.

We assume sinusoidal change of the mirror's tuning as shown in Figure 3.5. The position modulation is given as $x_m = a_s \cos(\omega_s t + \varphi_s)$, and thus the reflected field at the mirror becomes (assuming $a_4 = 0$)

$$a_3 = r a_1 \exp(-i 2\phi_0) \exp(i 2k x_m) \approx r a_1 \exp(-i 2\phi_0) \exp\left(i 2k_0 a_s \cos(\omega_s t + \varphi_s)\right), \quad (3.22)$$

setting $m = 2k_0 a_s$. This can be expressed as

$$\begin{aligned}
a_3 &= r a_1 \exp(-i 2\phi_0) \left(1 + i \frac{m}{2} \exp\left(-i(\omega_s t + \varphi_s)\right) + i \frac{m}{2} \exp\left(i(\omega_s t + \varphi_s)\right) \right) \\
&= r a_1 \exp(-i 2\phi_0) \left(1 + \frac{m}{2} \exp\left(-i(\omega_s t + \varphi_s - \pi/2)\right) \right. \\
&\quad \left. + \frac{m}{2} \exp\left(i(\omega_s t + \varphi_s + \pi/2)\right) \right).
\end{aligned} \tag{3.23}$$

3.7 Coupling matrices for beams with multiple frequency components

The coupling between electromagnetic fields at optical components introduced in Section 2 referred only to the amplitude and phase of a simplified monochromatic field, ignoring all the other parameters of the electric field of the beam given in Equation (1.1). However, this mathematical concept can be extended to include other parameters provided that we can find a way to describe the total electric field as a sum of components, each of which is characterised by a discrete value of the related parameters. In the case of the frequency of the light field, this means we have to describe the field as a sum of monochromatic components. In the previous sections we have shown how this could be done in the special case of an initial monochromatic field that is subject to modulation: if the modulation index is small enough we can limit the amount of frequency components that we need to consider. In many cases it is actually sufficient to describe a modulation only by the interaction of the carrier at ω_0 (the unmodulated field) and two sidebands with a frequency offset of $\pm\omega_m$ to the carrier. A beam given by the sum of three such components can be described by a complex vector:

$$\vec{a} = \begin{pmatrix} a(\omega_0) \\ a(\omega_0 - \omega_m) \\ a(\omega_0 + \omega_m) \end{pmatrix} = \begin{pmatrix} a_{\omega 0} \\ a_{\omega 1} \\ a_{\omega 2} \end{pmatrix} \tag{3.24}$$

with $\omega_0 = \omega 0$, $\omega_0 - \omega_m = \omega 1$ and $\omega_0 + \omega_m = \omega 2$. In the case of a phase modulator that applies a modulation of small modulation index m to an incoming light field \vec{a}_1 , we can describe the coupling of the frequency component as follows:

$$\begin{aligned}
a_{2,\omega 0} &= J_0(m) a_{1,\omega 0} + J_1(m) a_{1,\omega 1} + J_{-1}(m) a_{1,\omega 2} \\
a_{2,\omega 1} &= J_0(m) a_{1,\omega 1} + J_{-1}(m) a_{1,\omega 0} \\
a_{2,\omega 2} &= J_0(m) a_{1,\omega 2} + J_1(m) a_{1,\omega 0},
\end{aligned} \tag{3.25}$$

which can be written in matrix form:

$$\vec{a}_2 = \begin{pmatrix} J_0(m) & J_1(m) & J_{-1}(m) \\ J_{-1}(m) & J_0(m) & 0 \\ J_1(m) & 0 & J_0(m) \end{pmatrix} \vec{a}_1. \tag{3.26}$$

And similarly, we can write the complete coupling matrix for the modulator component, for example, as

$$\begin{pmatrix} a_{2,\omega 0} \\ a_{2,\omega 1} \\ a_{2,\omega 2} \\ a_{4,\omega 0} \\ a_{4,\omega 1} \\ a_{4,\omega 2} \end{pmatrix} \begin{pmatrix} J_0(m) & J_1(m) & J_{-1}(m) & 0 & 0 & 0 \\ J_{-1}(m) & J_0(m) & 0 & 0 & 0 & 0 \\ J_1(m) & 0 & J_0(m) & 0 & 0 & 0 \\ 0 & 0 & 0 & J_0(m) & J_1(m) & J_{-1}(m) \\ 0 & 0 & 0 & J_{-1}(m) & J_0(m) & 0 \\ 0 & 0 & 0 & J_1(m) & 0 & J_0(m) \end{pmatrix} \begin{pmatrix} a_{1,\omega 0} \\ a_{1,\omega 1} \\ a_{1,\omega 2} \\ a_{3,\omega 0} \\ a_{3,\omega 1} \\ a_{3,\omega 2} \end{pmatrix} \tag{3.27}$$

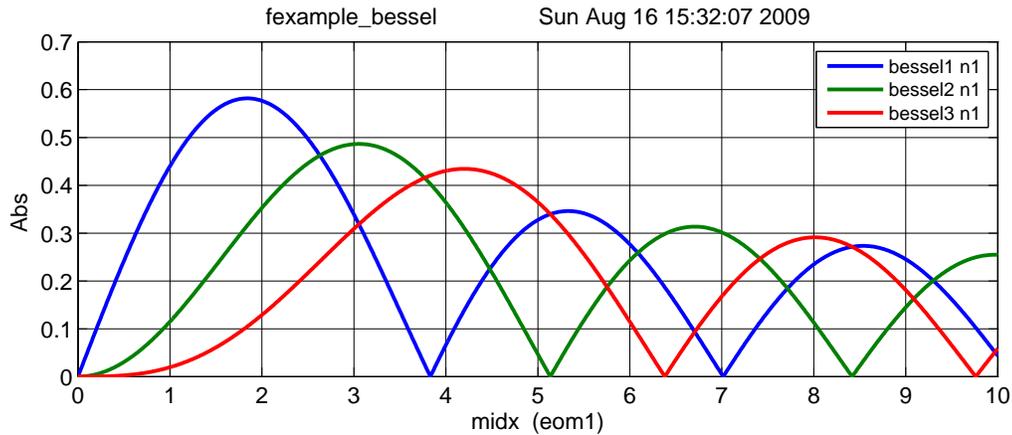


Figure 3.6: FINESSE example: Modulation index.

3.8 Finesse examples

3.8.1 Modulation index

This file demonstrates the use of a modulator. Phase modulation (with up to five higher harmonics) is applied to a laser beam and amplitude detectors are used to measure the field at the first three harmonics. Compare this to Figure 3.2 as well.

Finesse input file for ‘Modulation index’

```

laser i1 1 0 n0           % laser P=1W f_offset=0Hz
mod  eom1 40k .05 5 pm n0 n1 % phase modulator f_mod=40kHz, modulation index=0.05
ad   bessel1 40k n1       % amplitude detector f=40kHz
ad   bessel2 80k n1       % amplitude detector f=80kHz
ad   bessel3 120k n1      % amplitude detector f=120kHz
xaxis eom1 midx lin 0 10 1000 % x-axis: modulation index of eom1

yaxis abs                 % y-axis: plot ‘absolute’ amplitude

```

3.8.2 Mirror modulation

FINESSE offers two different types of modulators: the ‘modulator’ component shown in the example above, and the ‘fsig’ command, which can be used to apply a *signal modulation* to existing optical components. The main difference is that ‘fsig’ is meant to be used for transfer function computations. Consequently FINESSE discards all nonlinear terms, which means that the sideband amplitude is proportional to the signal amplitude and harmonics are not created.

Finesse input file for ‘Mirror modulation’

```

laser i1 1 0 n1           % laser P=1W f_offset=0Hz
space s1 1 1 n1 n2       % space of 1m length
bs    b1 1 0 0 n2 n3 dump dump % beam splitter as ‘turning mirror’, normal incidence
space s2 1 1 n3 n4       % another space of 1m length

```

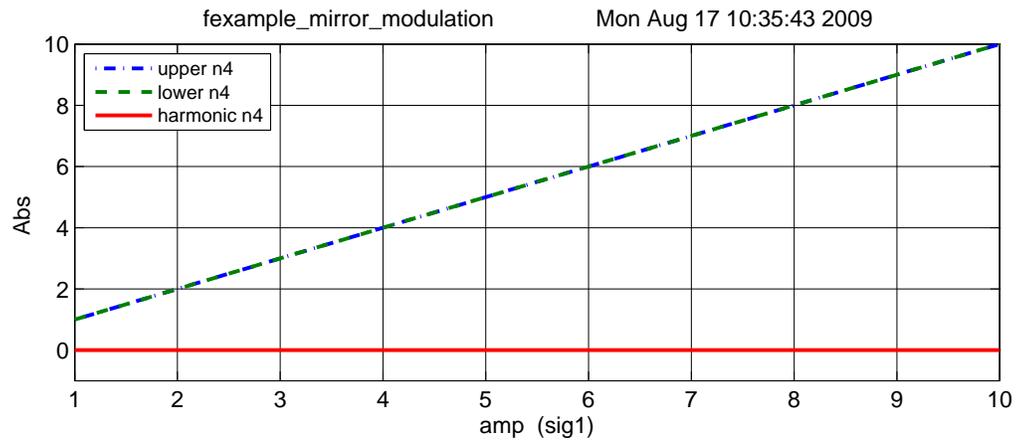


Figure 3.7: FINESSE example: Mirror modulation.

```

fsig sig1 b1 40k 1 0      % signal modulation applied to beam splitter b1
ad  upper  40k n4        % amplitude detector f=40kHz
ad  lower -40k n4       % amplitude detector f=-40kHz
ad  harmonic 80k n4     % amplitude detector f=80kHz
xaxis sig1 amp lin 1 10 100 % x-axis: amplitude of signal modulation
yaxis abs                % y-axis: plot 'absolute' amplitude

```

4 Optical Readout

In previous sections we have dealt with the amplitude of light fields directly and also used the *amplitude detector* in the FINESSE examples. This is the advantage of a mathematical analysis versus experimental tests, in which only light intensity or light power can be measured directly. This section gives the mathematical details for modelling photo detectors.

The intensity of a field impinging on a photo detector is given as the magnitude of the Poynting vector, with the Poynting vector given as [172]

$$\vec{S} = \vec{E} \times \vec{H} = \frac{1}{\mu_0} \vec{E} \times \vec{B}. \quad (4.1)$$

Inserting the electric and magnetic components of a plane wave, we obtain

$$|\vec{S}| = \frac{1}{\mu_0 c} E^2 = c\epsilon_0 E_0^2 \cos^2(\omega t) = \frac{c\epsilon_0}{2} E_0^2 (1 + \cos(2\omega t)), \quad (4.2)$$

with ϵ_0 the electric permeability of vacuum and c the speed of light.

The response of a photo detector is given by the total flux of effective radiation⁴ during the response time of the detector. For example, in a photo diode a photon will release a charge in the n-p junction. The response time is given by the time it takes for the charge to travel through the detector (and further time may be taken up in the electronic processing of the signal). The size of the photodiode and the applied bias voltage determine the travel time of the charges with typical values of approximately 10 ns. Thus, frequency components faster than perhaps 100 MHz are not resolved by a standard photodiode. For example, a laser beam with a wavelength of $\lambda = 1064$ nm has a frequency of $f = c/\lambda \approx 282 \cdot 10^{12}$ Hz = 282 THz. Thus, the 2ω component is much too fast for the photo detector; instead, it returns the average power

$$|\overline{\vec{S}}| = \frac{c\epsilon_0}{2} E_0^2. \quad (4.3)$$

In complex notation we can write

$$|\overline{\vec{S}}| = \frac{c\epsilon_0}{2} EE^*. \quad (4.4)$$

However, for more intuitive results the light fields can be given in converted units, so that the light power can be computed as the square of the light field amplitudes. Unless otherwise noted, throughout this work the unit of light field amplitudes is $\sqrt{\text{watt}}$. Thus, the notation used in this document to describe the computation of the light power of a laser beam is

$$P = EE^*. \quad (4.5)$$

4.1 Detection of optical beats

What is usually called an *optical beat* or simply a *beat* is the sinusoidal behaviour of the intensity of two overlapping and coherent fields. For example, if we superpose two fields of slightly different frequency, we obtain

$$\begin{aligned} E &= E_0 \cos(\omega_1 t) + E_0 \cos(\omega_2 t) \\ P &= E^2 = E_0^2 (\cos^2(\omega_1 t) + \cos^2(\omega_2 t) + 2 \cos(\omega_1 t) \cos(\omega_2 t)) \\ &= E_0^2 (\cos^2(\omega_1 t) + \cos^2(\omega_2 t) + \cos(\omega_+ t) + \cos(\omega_- t)), \end{aligned} \quad (4.6)$$

⁴ The term *effective* refers to that amount of incident light, which is converted into photo-electrons that are then usefully extracted from the junction (i.e. do not recombine within the device). This fraction is usually referred to as *quantum efficiency* η of the photodiode.

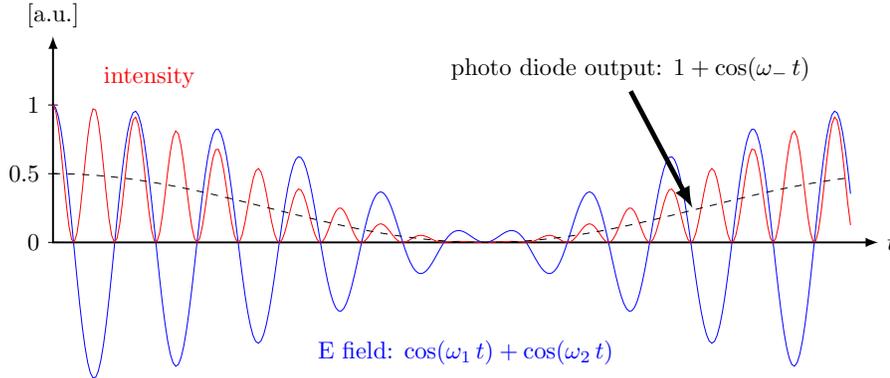


Figure 4.1: A beam with two frequency components hits the photo diode. Shown in this plot are the field amplitude, the corresponding intensity and the electrical output of the photodiode.

with $\omega_+ = \omega_1 + \omega_2$ and $\omega_- = \omega_1 - \omega_2$. In this equation the frequency ω_- can be very small and can then be detected with the photodiode as illustrated in Figure 4.1.

$$P_{\text{diode}} = E_0^2 (1 + \cos(\omega_- t)) \quad (4.7)$$

Using the same example photodiode as before: in order to be able to detect an optical beat ω_- would need to be smaller than 100 MHz. If we take two, slightly detuned Nd:YAG lasers with $f = 282$ THz, this means that the relative detuning of these lasers must be smaller than 10^{-7} .

In general, for a field with several frequency components, the photodiode signal can be written as

$$|E|^2 = E \cdot E^* = \sum_{i=0}^N \sum_{j=0}^N a_i a_j^* e^{i(\omega_i - \omega_j) t}. \quad (4.8)$$

For example, if the photodiode signal is filtered with a low-pass filter, such that only the DC part remains, we can compute the resulting signal by looking for all components without frequency dependence. The frequency dependence vanishes when the frequency becomes zero, i.e. in all parts of Equation (4.8) with $\omega_i = \omega_j$. The output is a real number, calculated like this:

$$x = \sum_i \sum_j a_i a_j^* \quad \text{with} \quad \{i, j \mid i, j \in \{0, \dots, N\} \wedge \omega_i = \omega_j\}. \quad (4.9)$$

4.2 Signal demodulation

A typical application of light modulation, is its use in a modulation-demodulation scheme, which applies an electronic demodulation to a photodiode signal. A ‘demodulation’ of a photodiode signal at a user-defined frequency ω_x , performed by an electronic mixer and a low-pass filter, produces a signal, which is proportional to the amplitude of the photo current at DC and at the frequency $\omega_0 \pm \omega_x$. Interestingly, by using two mixers with different phase offsets one can also reconstruct the phase of the signal, or to be precise the phase difference of the light at $\omega_0 \pm \omega_x$ with respect to the carrier light. This feature can be very powerful for generating interferometer control signals.

Mathematically, the demodulation process can be described by a multiplication of the output with a cosine: $\cos(\omega_x + \varphi_x)$ (φ_x is the *demodulation phase*), which is also called the ‘local oscillator’. After the multiplication was performed only the **DC** part of the result is taken into account. The signal is

$$S_0 = |E|^2 = E \cdot E^* = \sum_{i=0}^N \sum_{j=0}^N a_i a_j^* e^{i(\omega_i - \omega_j) t}. \quad (4.10)$$

Multiplied with the local oscillator it becomes

$$\begin{aligned} S_1 &= S_0 \cdot \cos(\omega_x t + \varphi_x) = S_0 \frac{1}{2} (e^{i(\omega_x t + \varphi_x)} + e^{-i(\omega_x t + \varphi_x)}) \\ &= \frac{1}{2} \sum_{i=0}^N \sum_{j=0}^N a_i a_j^* e^{i(\omega_i - \omega_j) t} \cdot (e^{i(\omega_x t + \varphi_x)} + e^{-i(\omega_x t + \varphi_x)}). \end{aligned} \quad (4.11)$$

With $A_{ij} = a_i a_j^*$ and $e^{i\omega_{ij} t} = e^{i(\omega_i - \omega_j) t}$ we can write

$$S_1 = \frac{1}{2} \left(\sum_{i=0}^N A_{ii} + \sum_{i=0}^N \sum_{j=i+1}^N (A_{ij} e^{i\omega_{ij} t} + A_{ij}^* e^{-i\omega_{ij} t}) \right) \cdot (e^{i(\omega_x t + \varphi_x)} + e^{-i(\omega_x t + \varphi_x)}). \quad (4.12)$$

When looking for the DC components of S_1 we get the following [69]:

$$\begin{aligned} S_{1,\text{DC}} &= \sum_{ij} \frac{1}{2} (A_{ij} e^{-i\varphi_x} + A_{ij}^* e^{i\varphi_x}) \quad \text{with} \quad \{i, j \mid i, j \in \{0, \dots, N\} \wedge \omega_{ij} = \omega_x\} \\ &= \sum_{ij} \Re \{A_{ij} e^{-i\varphi_x}\}. \end{aligned} \quad (4.13)$$

This would be the output of a mixer and a subsequent low-pass filter. The results for $\varphi_x = 0$ and $\varphi_x = \pi/2$ are called *in-phase* and *in-quadrature*, respectively (or also *first* and *second quadrature*). They are given by

$$\begin{aligned} S_{1,\text{DC,phase}} &= \sum_{ij} \Re \{A_{ij}\}, \\ S_{1,\text{DC,quad}} &= \sum_{ij} \Im \{A_{ij}\}. \end{aligned} \quad (4.14)$$

If only one mixer is used, the output is always real and is determined by the demodulation phase. However, with two mixers generating the in-phase and in-quadrature signals, it is possible to construct a complex number representing the signal amplitude and phase:

$$z = \sum_{ij} a_i a_j^* \quad \text{with} \quad \{i, j \mid i, j \in \{0, \dots, N\} \wedge \omega_{ij} = \omega_x\}. \quad (4.15)$$

Often several sequential demodulations are applied in order to measure very specific phase information. For example, a double demodulation can be described as two sequential multiplications of the signal with two local oscillators and taking the DC component of the result. First looking at the whole signal, we can write:

$$S_2 = S_0 \cdot \cos(\omega_x t + \varphi_x) \cos(\omega_y t + \varphi_y). \quad (4.16)$$

This can be written as

$$\begin{aligned} S_2 &= S_0 \frac{1}{2} (\cos(\omega_y t + \omega_x t + \varphi_y + \varphi_x) + \cos(\omega_y t - \omega_x t + \varphi_y - \varphi_x)) \\ &= S_0 \frac{1}{2} (\cos(\omega_+ t + \varphi_+) + \cos(\omega_- t + \varphi_-)), \end{aligned} \quad (4.17)$$

and thus reduced to two single demodulations. Since we now only care for the DC component we can use the expression from above (Equation (4.15)). These two demodulations give two complex numbers:

$$\begin{aligned} z_1 &= \sum_{ij} A_{ij} \quad \text{with} \quad \{i, j \mid i, j \in \{0, \dots, N\} \wedge \omega_i - \omega_j = \omega_+\}, \\ z_2 &= \sum_{ij} A_{kl} \quad \text{with} \quad \{k, l \mid k, l \in \{0, \dots, N\} \wedge \omega_k - \omega_l = \omega_-\}. \end{aligned} \quad (4.18)$$

The demodulation phases are applied as follows to get a real output (two sequential mixers)

$$x = \Re \{ (z_1 e^{-i\varphi_x} + z_2 e^{i\varphi_x}) e^{-i\varphi_y} \}. \quad (4.19)$$

In a typical setup, a user-defined demodulation phase for the first frequency (here φ_x) is given. If two mixers are used for the second demodulation, we can reconstruct the complex number

$$z = z_1 e^{-i\varphi_x} + z_2 e^{i\varphi_x}. \quad (4.20)$$

More demodulations can also be reduced to single demodulations as above.

4.3 Finesse examples

4.3.1 Optical beat

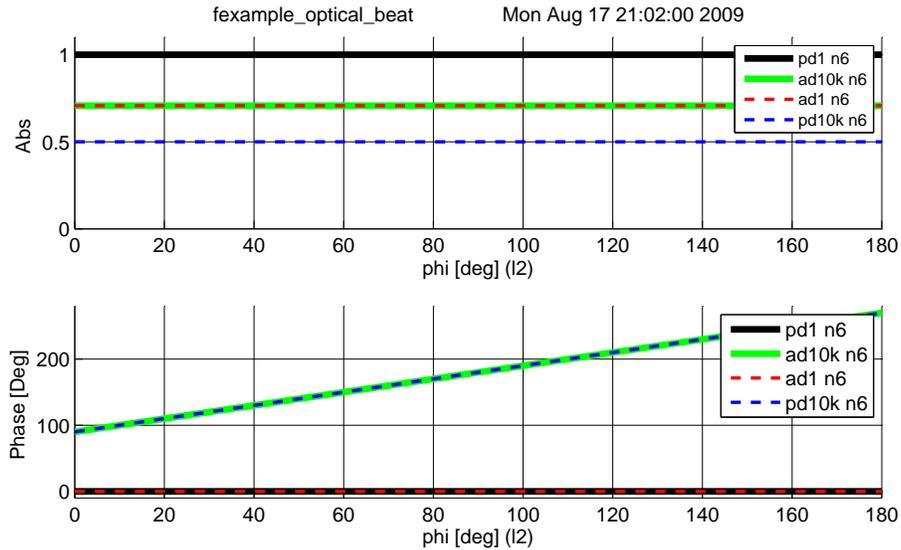


Figure 4.2: FINESSE example: Optical beat.

In this example two laser beams are superimposed at a 50:50 beam splitter. The beams have a slightly different frequency: the second beam has a 10 kHz offset with respect to the first (and to the default laser frequency). The plot illustrates the output of four different detectors in one of the beam splitter output ports, while the phase of the second beam is tuned from 0° to 180° . The photodiode ‘pd1’ shows the total power remaining constant at 1. The amplitude detectors ‘ad1’ and ‘ad10k’ detect the laser light at 0 Hz (default frequency) and 10 kHz respectively. Both show a constant absolute of $\sqrt{1/2}$ and the detector ‘ad10k’ tracks the tuning of the phase of the second laser beam. Finally, the detector ‘pd10k’ resembles a photodiode with demodulation at 10 kHz. In fact, this represents a photodiode and two mixers used to reconstruct a complex number as shown in Equation (4.15). One can see that the phase of the resulting electronic signal also directly follows the phase difference between the two laser beams.

Finesse input file for ‘Optical beat’

```

const freq 10k      % creating a constant for the frequency offset
laser  l1 1 0 n1    % laser with P=1W at the default frequency
space  s1 1n 1 n1 n2 % space of 1nm length
laser  l2 1 $freq n3 % a second laser with f=10kHz frequency offset
space  s2 1n 1 n3 n4 % another space of 1nm length

```

```
bs      b1 0.5 0.5 0 0 n2 n5 dump n4 % 50:50 beam splitter
space  s3 1n 1 n5 n6 % another space of 1nm length
ad      ad0 0 n6 % amplitude detector at f=0Hz
ad      ad10k $freq n6 % amplitude detector at f=10kHz
pd      pd1 n6 % simple photo detector
pd1     pd10k $freq n6 % photo detector with demodulation at 10kHz

xaxis  12 phi lin 0 180 100 % changing the phase of the 12-beam

yaxis  abs:deg % plotting amplitude and phase
```

5 Basic Interferometers

The large interferometric gravitational-wave detectors currently in operation are based on two fundamental interferometer topologies: the *Fabry-Perot* interferometer and the *Michelson* interferometer. The main instrument is very similar to the original interferometer concept used in the famous experiment by Michelson and Morley, published in 1887 [119]. The main difference is that modern instruments use laser light to illuminate the interferometer to achieve much higher accuracy. Already the first prototype by Forward and Weiss has thus achieved a sensitivity a million times better than Michelson's original instrument [67]. In addition, the Michelson interferometer used in current gravitational-wave detectors has been enhanced by resonant cavities, which in turn have been derived from the original idea for a spectroscopy standard published by Fabry and Perot in 1899 [65]. The following section will describe the fundamental properties of the Fabry-Perot interferometer and the Michelson interferometer. A thorough understanding of these basic instruments is essential for the study of the high-precision interferometers used for gravitational-wave detection.

5.1 The two-mirror cavity: a Fabry-Perot interferometer

We have computed the field amplitudes in a linear two-mirror cavity, also called a *Fabry-Perot* interferometer, in Section 2.2. In order to understand the features of this optical instrument it is interesting to have a closer look at the power circulating in the cavity. A typical optical layout is shown in Figure 5.1; two parallel mirrors form the Fabry-Perot cavity. A laser beam is injected through the first mirror (at normal incidence).

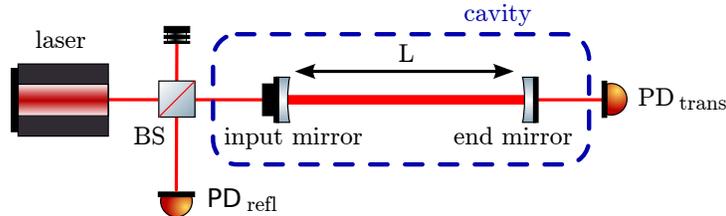


Figure 5.1: Typical optical layout of a two-mirror cavity, also called a Fabry-Perot interferometer. Two mirrors form the Fabry-Perot interferometer, a laser beam is injected through one of the mirrors and the reflected and transmitted light can be detected by photo detectors.

The behaviour of the (ideal) cavity is determined by the length of the cavity L , the wavelength of the laser λ and the reflectivity and transmittance of the mirrors. Using the mathematical description introduced in Section 2.2 and assuming an input power of $|a_0|^2 = 1$, we obtain the following equation for the circulating power:

$$P_1 = |a_1|^2 = \frac{T_1}{1 + R_1 R_2 - 2r_1 r_2 \cos(2kL)}, \quad (5.1)$$

with $k = 2\pi/\lambda$, P , $T = t^2$ and $R = r^2$, as defined in Section 1.3. Similarly we could compute the transmission of the optical system as the input-output ratio of the field amplitudes. For example, with a_0 the field injected into the cavity and a_2 the field transmitted by the cavity,

$$\frac{a_2}{a_0} = \frac{-t_1 t_2 \exp(-i k L)}{1 - r_1 r_2 \exp(-i 2kL)} \quad (5.2)$$

is the frequency-dependent transfer function of the cavity in transmission (the frequency dependence is hidden inside the $k = 2\pi f/c$).

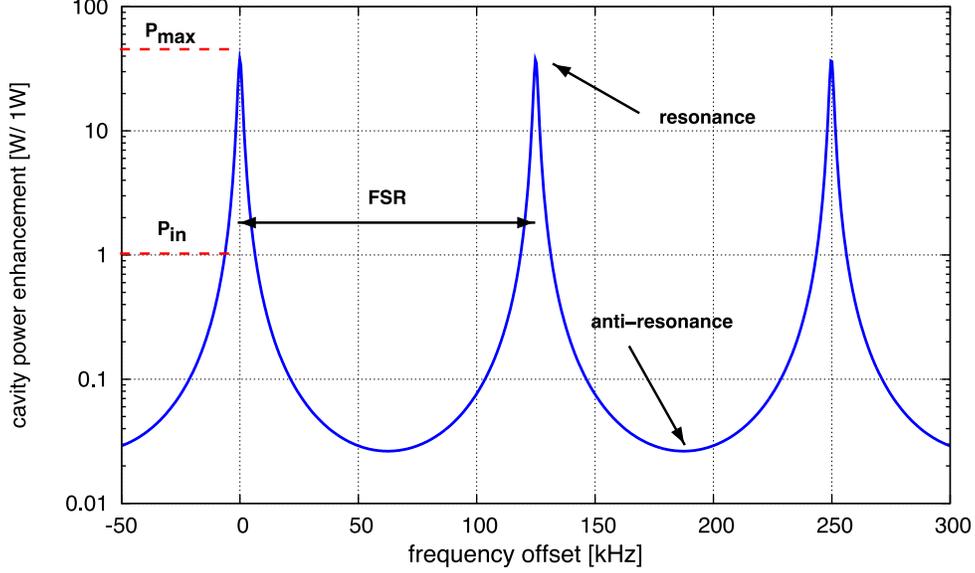


Figure 5.2: Power enhancement in a two-mirror cavity as a function of the laser-light frequency. The peaks marks the resonances of the cavity, i.e. modes of operation in which the injected light is resonantly enhanced. The frequency distance between two peaks is called *free-spectral range* (FSR).

Figure 5.2 shows a plot of the circulating light power P_1 over the laser frequency. The maximum power is reached when the cosine function in the denominator becomes equal to one, i.e. at $kL = N\pi$ with N an integer. This occurs when the round-trip length is an integer multiple of the wavelength of the injected light: $2L = N2\pi/k = N\lambda$. This is called the *cavity resonance*. The lowest power values are reached at *anti-resonance* when $kL = (N + 1/2)\pi$. We can also rewrite

$$2kL = \omega \frac{2L}{c} = 2\pi f \frac{2L}{c} = \frac{2\pi f}{\text{FSR}}, \quad (5.3)$$

with FSR being the *free-spectral range* of the cavity as shown in Figure 5.2. Thus, it becomes clear that resonance is reached for laser frequencies

$$f_r = N \cdot \text{FSR}, \quad (5.4)$$

where N is an integer.

Another characteristic parameter of a cavity is its linewidth, usually given as its *full width at half maximum* (FWHM) or its *pole frequency*, f_p . In order to compute the linewidth we have to ask at which frequency the circulating power becomes half the maximum:

$$|a_1(f_p)|^2 \stackrel{!}{=} \frac{1}{2} |a_{1,\max}|^2. \quad (5.5)$$

This results in the following expression for the full linewidth:

$$\text{FWHM} = 2f_p = \frac{2\text{FSR}}{\pi} \arcsin\left(\frac{1 - r_1 r_2}{2\sqrt{r_1 r_2}}\right). \quad (5.6)$$

The ratio of the linewidth to the free spectral range is called the *finesse* of a cavity:

$$F = \frac{\text{FSR}}{\text{FWHM}} = \frac{\pi}{2 \arcsin\left(\frac{1 - r_1 r_2}{2\sqrt{r_1 r_2}}\right)}. \quad (5.7)$$

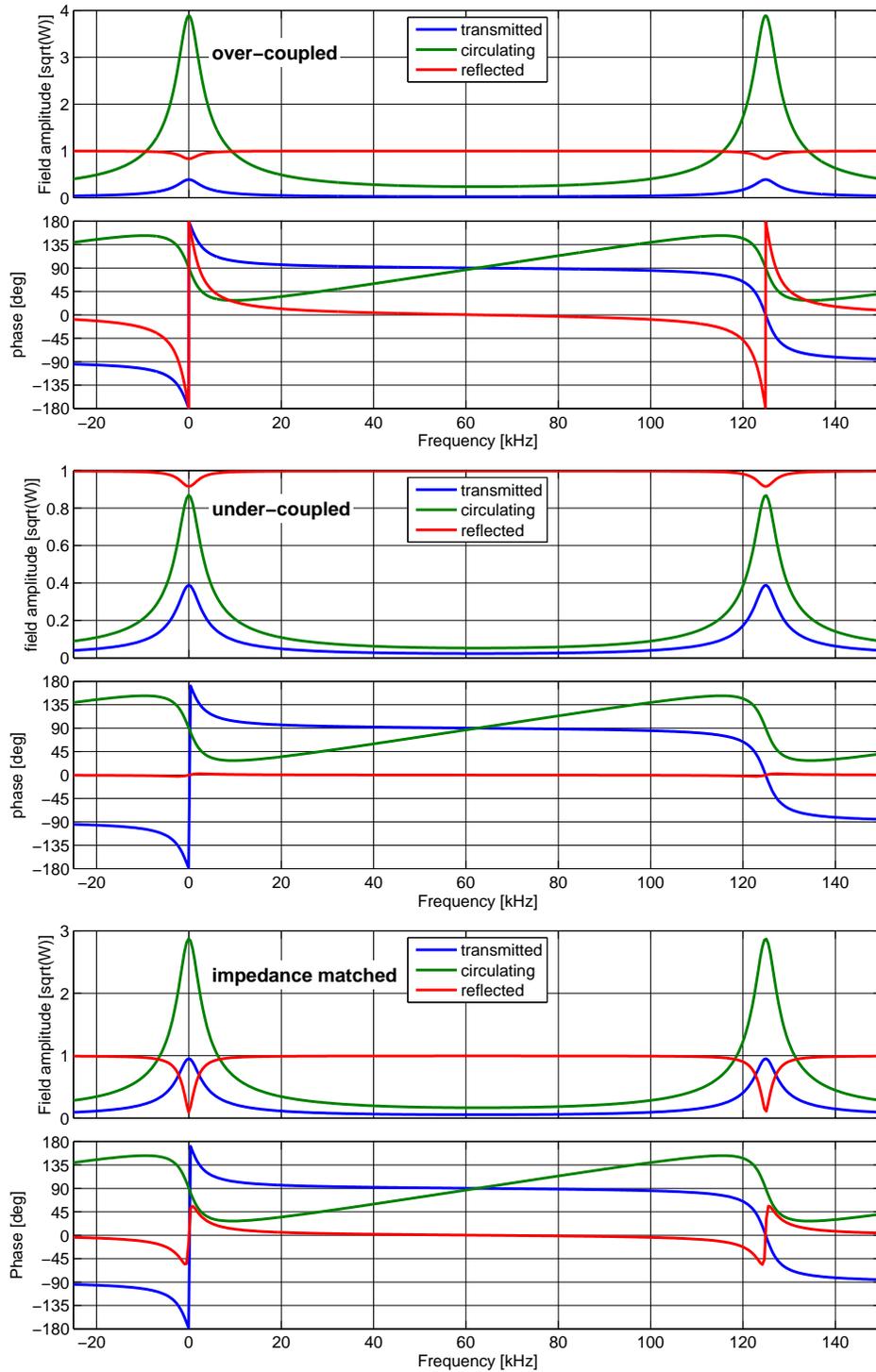


Figure 5.3: This figure compares the fields reflected by, transmitted by and circulating in a Fabry-Perot cavity for the three different cases: over-coupled, under-coupled and impedance matched cavity (in all cases $T_1 + T_2 = 0.2$ and the round-trip loss is 1%). The traces show the phase and amplitude of the electric field as a function of laser frequency detuning.

In the case of high finesse, i.e. when r_1 and r_2 are close to 1, we can use the fact that the argument of the arcsin function is small and make the approximation

$$F \approx \frac{\pi\sqrt{r_1 r_2}}{1 - r_1 r_2} \approx \frac{\pi}{1 - r_1 r_2}. \quad (5.8)$$

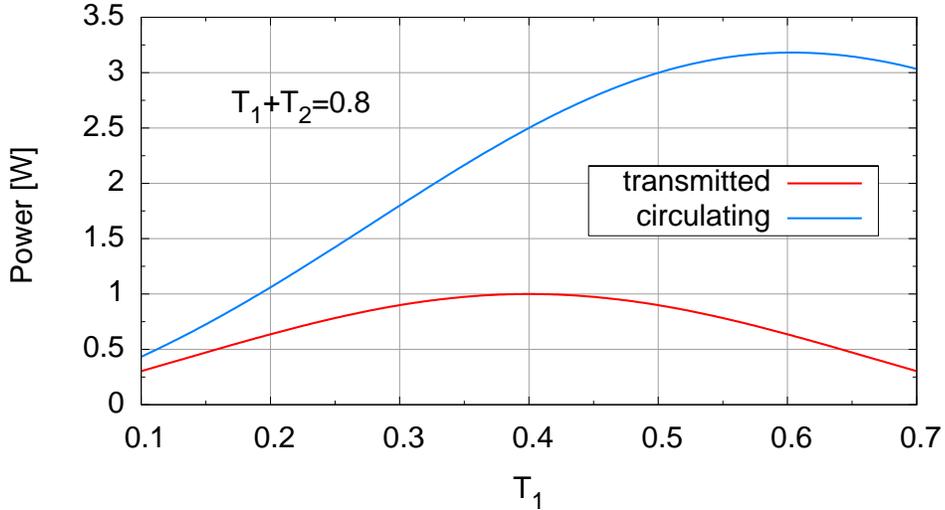


Figure 5.4: Power transmitted and circulating in a two mirror cavity with input power 1 W. The mirror transmissions are set such that $T_1 + T_2 = 0.8$ and the reflectivities of both mirrors are set as $R = 1 - T$. The cavity is undercoupled for $T_1 < 0.4$, impedance matched at $T_1 = T_2 = 0.4$, and overcoupled for $T_1 > 0.4$. The transmission is maximised in the impedance-matched case and falls similarly for over or undercoupled settings. However, the circulating power (and any resonance performance of the cavity) is much larger in the overcoupled case.

The behaviour of a two mirror cavity depends on the length of the cavity (with respect to the frequency of the laser) and on the reflectivities of the mirrors. Regarding the mirror parameters, one distinguishes three cases⁵:

- when $T_1 < T_2$ the cavity is *undercoupled*
- when $T_1 = T_2$ the cavity is *impedance matched*
- when $T_1 > T_2$ the cavity is *overcoupled*

The differences between these three cases can seem subtle mathematically but have a strong impact on the application of cavities in laser systems. One of the main differences is the phase evolution of the light fields, as shown in Figure 5.3. The circulating power shows that the resonance effect is better used in over-coupled cavities; this is illustrated in Figure 5.4, which shows the transmitted and circulating power for the three different cases. Only in the impedance-matched case can the cavity transmit (on resonance) *all* the incident power. Given the same total transmission $T_1 + T_2$,

⁵ Please note that in the presence of losses the coupling is defined with respect to the transmission and losses. In particular, the impedance-matched case is defined as $T_1 = T_2 \times \text{Loss}$, so that the input power transmission exactly matches the light power lost in one round-trip.

the overcoupled case allows for the largest circulating power and thus a stronger ‘resonance effect’ of the cavity, which is useful, for example, when the cavity is used as a mode filter. Hence, most commonly used cavities are impedance matched or overcoupled.

5.2 Michelson interferometer

We came across the Michelson interferometer in Section 2.4 when we discussed the phase relation at a beam splitter. The typical optical layout of the Michelson interferometer is shown again in Figure 5.5, a laser beam is split by a beam splitter and sent along two perpendicular *interferometer arms*. The four directions seen from the beam splitter are often labelled North, East, West and South. Another common naming scheme, also shown in Figure 5.5 refers to the interferometer arms as X and Y; the two outputs are labelled as the symmetric port (towards the laser input) and anti-symmetric port respectively. Both conventions are common in the literature and we will make use of both in this article.

The ends of the interferometer arms (North and East or Y and X) are marked by highly reflective *end mirrors*, sometimes called *end test masses* (ETM), The laser beams are reflected by the end mirrors and then recombined at the central beam splitter. Generally, the Michelson interferometer has two outputs, namely the so far unused beam splitter port (*South port* or *anti-symmetric port*) and the input port (*West port* or *symmetric port*). Both output ports can be used to obtain interferometer signals; however most setups are designed such that the main signals are detected in the South port⁶.

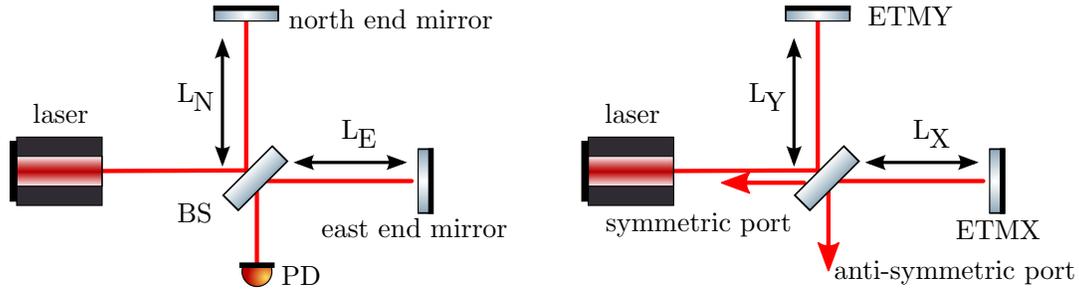


Figure 5.5: Optical layout and two common naming convention sfor a Michelson interferometer: a laser beam is split into two and sent along two perpendicular interferometer arms. We will sometimes label the directions in a Michelson interferometer as North, East, West and South, as shown in the left plot. The end mirror,s or end test masses (ETMs), reflect the beams towards the beam splitter, where they recombine. The South and West ports of the beam splitter are possible output port; however in many cases only the South port is used. The plot on the right shows an alternative naming scheme commonly used, in which the two arms are labelled X and Y, the output towards the laser is called the *symmetric port* and the other output is referred to as the *anti-symmetric port*.

The Michelson interferometer output signal is determined by the laser wavelength λ , the reflectivity and transmittance of the beam splitter and the end mirrors, and the relative length of the interferometer arms. In many cases the end mirrors are highly reflective and the beam splitter is ideally a 50:50 beam splitter. In this case, we can compute the output for a monochromatic field

⁶The term ‘main signals’ refers to the optical signal providing the readout of the interferometric measurement, for example, of a position or length change. In addition, other output signals exist: for example, the light power reflected back into the West port can be recorded for monitoring the interferometer status.

as shown in Section 2.4. Using Equation (2.17) we can write the field in the South port as

$$E_S = E_0 \frac{i}{2} (e^{i2kL_N} + e^{i2kL_E}). \quad (5.9)$$

We define the common and differential arm lengths as

$$\begin{aligned} \bar{L} &= \frac{L_N + L_E}{2} \\ \Delta L &= L_N - L_E, \end{aligned} \quad (5.10)$$

which yield $2L_N = 2\bar{L} + \Delta L$ and $2L_E = 2\bar{L} - \Delta L$. Thus, we can further simplify to get

$$E_S = E_0 \frac{i}{2} e^{i2k\bar{L}} (e^{ik\Delta L} + e^{-ik\Delta L}) = E_0 i e^{i2k\bar{L}} \cos(k\Delta L). \quad (5.11)$$

The photo detector then produces a signal proportional to

$$S = E_S E_S^* = P_0 \cos^2(k\Delta L) = P_0 \cos^2(2\pi\Delta L/\lambda). \quad (5.12)$$

This signal is depicted in Figure 5.6; it shows that the power in the South port changes between zero and the input power with a period of $\Delta L/\lambda = 0.5$. The tuning at which the output power drops to zero is called the *dark fringe*. Current interferometric gravitational-wave detectors operate their Michelson interferometer at or near the dark fringe.

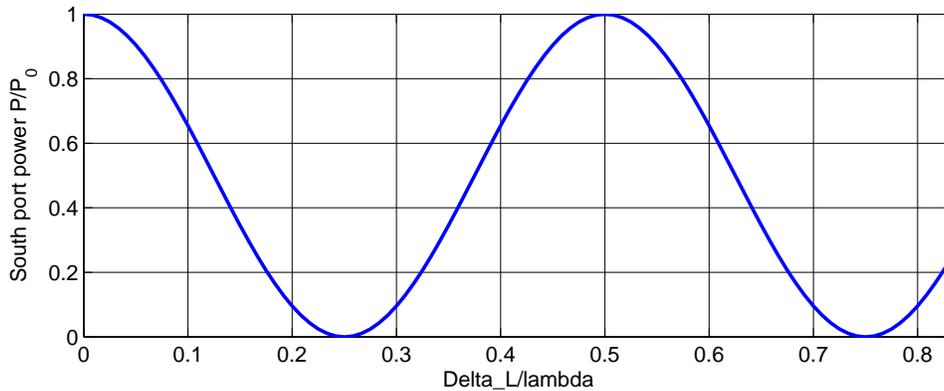


Figure 5.6: Power in the South port of a symmetric Michelson interferometer as a function of the arm length difference ΔL . When the interferometer is set to $\Delta L/\lambda = 0.25$ the input light is not transmitted into the South port: this condition is called the *dark fringe*.

The above seems to indicate that the macroscopic arm-length difference plays no role in the Michelson output signal. However, this is only correct for a monochromatic laser beam with infinite coherence length. In real interferometers care must be taken that the arm-length difference is well below the coherence length of the light source. In gravitational-wave detectors the macroscopic arm-length difference is an important design feature; it is kept very small in order to reduce coupling of laser noise into the output but needs to retain a finite size to allow the transfer of phase modulation sidebands from the input to the output port; this is illustrated in the FINESSE example below and will be covered in detail in Section 8.9.

5.3 NEW: Michelson interferometer and the sideband picture

In the context of gravitational wave detection the Michelson interferometer is used for measuring a very small differential change in the length of one arm versus the other. The very small amplitude

of gravitational waves (or the equivalent small differential change of the arm lengths) requires additional optical techniques to increase the sensitivity of the interferometer. In this section we briefly introduce the interferometer configurations and review their effect on the detector sensitivity.

The Michelson interferometer can achieve its best sensitivity when operated in a quasi stationary mode, i.e. when the positions of mirrors and beamsplitters are carefully controlled so that the key parameters, for example the light power inside the interferometer and at the output ports, are nearly constant. We call such an interferometer state, described by a unique set of the key parameters, an *operating point* of the interferometer (see Section 8 for a discussion of the control systems involved to reach and maintain an operating point). For an interferometer in a steady state it is possible to describe and analyse the behaviour using a *steady state model*, describing the light field coupling in the frequency domain and making use of the previously introduced concept of sidebands, see Section 3.1.

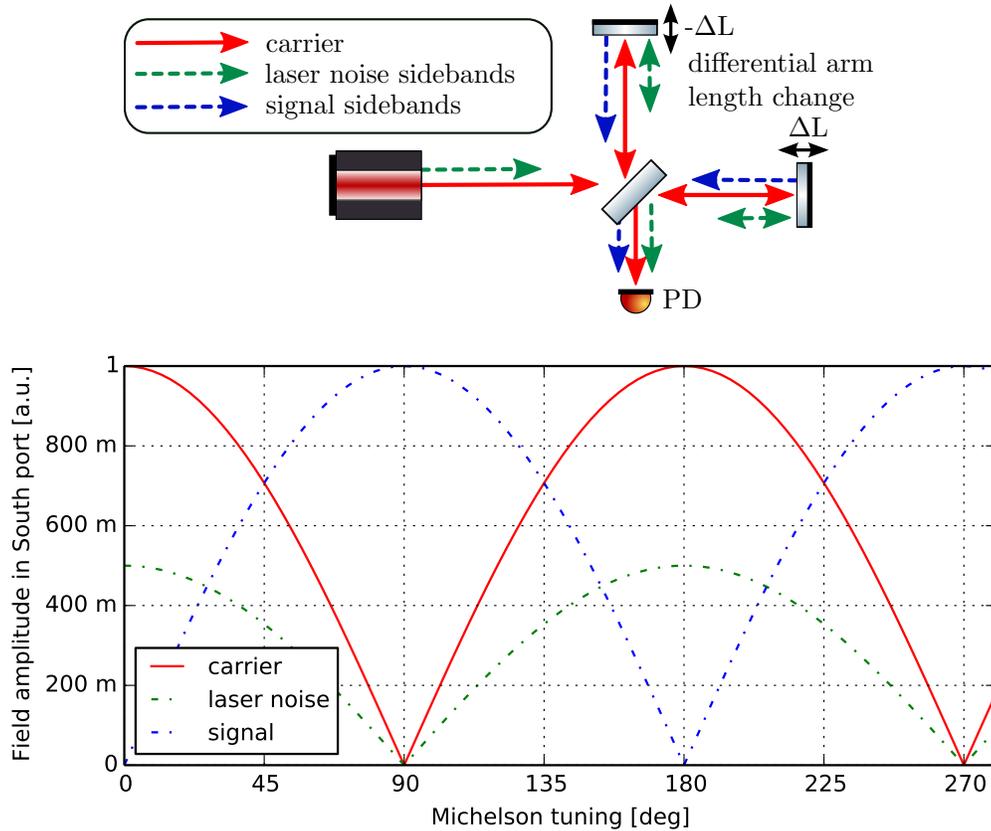


Figure 5.7: A Michelson interferometer shown with three types of light field: the ‘carrier’, representing the undistorted laser input field, ‘laser phase noise sidebands’, which enter the interferometer with the carrier, and ‘signal sidebands’, which are phase modulation sidebands caused by differential arm length motion. All three fields leave the interferometer through both output ports (here only the detector in the South port is shown). The graph shows the amplitude of the three light fields in the South port as a function of the Michelson tuning (differential arm length change). At 0 degrees the Michelson is on a *bright fringe* and at 90 degrees on a *dark fringe*.

Consider a Michelson interferometer which is to be used to measure a differential arm length change. As an example for a signal to noise comparison we consider the phase noise of the injected

laser light. For this example the noise can be represented by a sinusoidal modulation with a small amplitude at a single frequency, say 100 Hz. Therefore we can describe the phase noise of the laser by a pair of sidebands superimposed with the main carrier light field entering the Michelson interferometer. Equally the change of an interferometer arm represents a phase modulation of the light reflected back from the end mirrors and the generated optical signal can be represented by a pair of phase modulation sidebands, see Section 5.5.

In order to get an estimation of the signal to noise ratio we can trace the individual sidebands through the interferometer and compute their amplitude in the output port. Figure 5.7 shows the setup of a basic Michelson interferometer, indicating the insertion of the noise and signal sidebands. It also provides a plot of the sideband amplitude in the South output port as a function of the differential arm length of the Michelson interferometer. We can see that a tuning of 90 degrees corresponds to the dark fringe, the state of the interferometer in which the injected light (the carrier and laser noise) is reflected back towards the laser and is not transmitted into the South port. The plot reveals two advantages of the dark fringe as an operating point: first of all the transmission of the signal sidebands to the photo detector is maximised while the laser phase noise is minimised. More generally at the dark fringe, all common mode effects, such as laser noise, or common length changes of the arms, produce a minimal optical signal at the output port, whereas differential effects in the arms are maximised. Furthermore at the dark fringe the least amount of carrier light is transmitted to the photo detector. This is an advantage because it is technically often easier to make an accurate light power measurement when the total detected power is low.

It should be noted that typically one set of sidebands alone does not create a strong signal during detection. In the case of gravitational wave detection these sidebands are many orders of magnitude smaller than the amplitude of the carrier. Instead we require a beat between the signal sidebands and another field, a so-called *local oscillator*, to generate a strong electronic signal proportional to the amplitude of the signal sidebands. The local oscillator can be created in different ways, the most common are:

- Apply an RF modulation to the laser beam, either before injecting it into the interferometer or inside the interferometer. A small macroscopic length asymmetry between the two arms (Schnupp asymmetry, see Section 8.13) allows a significant amount of the RF sidebands to reach the South port when the interferometer is operating on the dark fringe for the carrier. The RF sideband fields can be used as a local oscillator.
- Set the Michelson such that it is close to, but not exactly on, the dark fringe. The carrier leaking into the South port can thus be used as a local oscillator. This scheme preserves the advantages of the dark fringe but relies on very good power stability of the carrier light.
- Superimpose an auxiliary beam onto the output before the photodetector. For example, a pick-off beam from the main laser can be used for this. The main disadvantage of this concept is that it requires a very stable auxiliary beam (in phase as well as position) thus creating new control problems.

5.4 NEW: Michelson interferometer signal readout with DC offset, or RF modulation

As discussed in Section 4.1, one method for providing a local oscillator is to use a small microscopic DC offset to tune the Michelson interferometer slightly away from the dark fringe. This allows a small amount of carrier to leak through to the output port to beat with the signal sidebands. The differential arm length difference required is

$$\Delta L = \frac{\pi}{2k_0} + \delta_{\text{off}}, \quad (5.13)$$

where $k_0 = \omega_0/c$ is the wavenumber of the carrier field and the DC offset is $\delta_{\text{off}} \ll 1$. The field at the output port of a Michelson (as shown in figure 2.8) for a single carrier field and one pair of signal sidebands is:

$$\begin{aligned}
E_6 &= itrE_0e^{-i2k_0\bar{L}} (2 \cos(k_0\Delta L) + s^+ + s^-) e^{i\omega_0 t}, \\
&= itrE_0e^{-i2k_0\bar{L}} \left(2 \cos\left(\frac{\pi}{2} + k_0\delta_{\text{off}}\right) + s^+ + s^- \right) e^{i\omega_0 t}, \\
&= itrE_0e^{-i2k_0\bar{L}} (2 \sin(k_0\delta_{\text{off}}) + s^+ + s^-) e^{i\omega_0 t},
\end{aligned} \tag{5.14}$$

where s^\pm are the complex amplitudes (magnitude and phase) of the upper and lower sidebands that reach the output port, for example, sidebands generated by a gravitational wave signal or via the modulation of a mirror position. The power in this field as measured by a photodiode will then contain the beats between the carrier and both sidebands. As the magnitude of any signal sideband is assumed to be very small, $|s^\pm| \ll 1$, we only need to consider terms linear in s^\pm . The DC power and terms linear in the s^\pm are then given by:

$$E_6E_6^* = TR|E_0|^2 (4 \sin^2(k_0\delta_{\text{off}}) + 2 \sin(k_0\delta_{\text{off}}) (s^+ + s^-) + O(s^2)). \tag{5.15}$$

As expected the signal sideband terms are not visible in the power if $\sin(k_0\delta_{\text{off}}) = 0$, because, if we operate purely at the dark fringe for the carrier field, no local oscillator is present to beat with the signal. The signal amplitude and phase can then be read out by demodulating the photocurrent at the signal frequency. In practice the choice of δ_{off} depends on a number of technical issues, in particular the laser power in the main output port and the transfer of common mode noise into the output.

Another option for providing a local oscillator is by phase modulating the input laser light, which is typically done at radio-frequencies (RF). This method of readout is also referred to as a *heterodyne readout scheme*. The RF sidebands will have a different interference condition at the beamsplitter compared to the carrier, and the interferometer can be setup so that the RF sidebands are present at the output port, to be used as a local oscillator, whilst the carrier field is at a dark fringe.

Consider a phase modulated beam with modulation index b and modulation frequency ω_b , the input field will be:

$$E_0 = E'_0 e^{i\omega_0 t} (1 + ib(e^{i\omega_b t} + e^{-i\omega_b t})). \tag{5.16}$$

The propagation of these three input fields to the output port can be treated separately and is similar to equation 5.14, except that we must keep track of their different frequencies: $k_0 = \omega_0/c$ and $k_b = \omega_b/c$ for the upper and lower RF sidebands. Ignoring the signal sidebands the fields present at the output port are

$$\begin{aligned}
E_6 &= E'_6(\omega_0) + E'_6(\omega_0 + \omega_b) + E'_6(\omega_0 - \omega_b) \\
E'_6(\omega_0) &= i2rtE'_0 \cos(k_0\Delta L) \\
E'_6(\omega_0 \pm \omega_b) &= i2bE'_0 e^{-i2(k_0 \pm k_b)\bar{L}} \cos((k_0 \pm k_b)\Delta L) e^{i(\omega_0 \pm \omega_b)t}
\end{aligned} \tag{5.17}$$

For using an RF readout scheme we want to set the Michelson to be on the dark fringe for $E'_6(\omega_0) = 0$. This is done by using a differential arm length difference of $\Delta L = (2N + 1)\frac{\pi}{2k_0}$ so

that $\cos(k_0\Delta L) = 0$, where N is any integer. The condition for the RF sidebands is now:

$$\begin{aligned}\cos((k_0 \pm k_b)\Delta L) &= \cos\left((k_0 \pm k_b)(2N + 1)\frac{\pi}{2k_0}\right) \\ &= \cos\left(\frac{\pi}{2} + N\pi \pm (2N + 1)\frac{\pi k_b}{2k_0}\right) \\ &= \sin\left(N\pi \pm (2N + 1)\frac{\pi k_b}{2k_0}\right) \\ &= \pm(-1)^N \sin(k_b\Delta L_N)\end{aligned}\tag{5.18}$$

$$\Delta L_N \equiv (2N + 1)\frac{\lambda_0}{4},\tag{5.19}$$

where λ_0 is the wavelength of the carrier light field. Thus the $\sin(k_b\Delta L_N)$ term now determines the amplitude of the RF sidebands that will be present at the output port, where N is our free variable to choose. Although ΔL_0 is a microscopic distance the actual differential arm length difference required to allow a reasonable amount of sidebands through requires a large choice of N as $k_b\Delta L_N \ll 1$ for radio frequency modulations. For example, the GEO 600 detector, which uses such an RF modulation scheme, operates with $\Delta L = 13.5\text{cm}$ [107]. The final step of including the signal sidebands is not elaborated on here but can be included with some careful algebra, remembering that there will be signal sidebands created around the carrier and both RF sidebands that could be present at the output port.

See Section 8.13 for an more detailed comparison of the DC and RF techniques to produce control signals and Section 8.16 for detailed arguments for the advantages and disadvantages of both techniques.

5.5 NEW: Response of the Michelson interferometer to a gravitational waves signal

In this section we derive how the sideband picture can be used to describe how the length modulation caused by a gravitational wave affects a laser beam travelling through space. This method can then be applied to any interferometer setup, for example to compute how the signal readout of a Michelson interferometer when using a DC offset. Modulating a space of proper length L will induce a phase modulation to any laser beam travelling along it. The phase such a beam accumulates along a path modulated by a gravitational wave signal $h(t)$ is [121]

$$\varphi = -k_0L \mp \frac{\omega_0}{2} \int_{t-L/c}^t h(t) = -k_0L \mp \delta\varphi,\tag{5.20}$$

with $k_c = \omega_0/c$ being the wavenumber of the light field and $\delta\varphi$ being the additional phase accumulated due to the modulation of the path. For our analysis here we can assume the gravitational wave signal is a simple sinusoidal function

$$h(t) = h_0 \cos(\omega_{gw}t + \varphi_{gw}),\tag{5.21}$$

where ω_{gw} and φ_{gw} are the frequency and phase of the gravitational wave. The phase accumulated from propagating along the space is then⁷

$$\delta\varphi = \frac{\omega_0 h_0}{\omega_{gw}} \cos\left(\omega_{gw}t + \varphi_{gw} - \omega_{gw}\frac{L}{2c}\right) \sin\left(\omega_{gw}\frac{L}{2c}\right).\tag{5.22}$$

⁷Derivations of the accumulated phase can be found in many works, a simple example is presented in [29].

Thus an oscillating, time dependent phase is present in the light fields travelling along the space. Section 3.2 describes how such a modulation generates sideband fields; the respective modulation index and phase are

$$m = -\frac{\omega_0 h_0}{\omega_{gw}} \sin\left(\frac{k_{gw} L}{2}\right), \quad (5.23)$$

$$\varphi = -\frac{k_{gw} L}{2} + \varphi_{gw}, \quad (5.24)$$

with $k_{gw} = \omega_{gw}/c$ being the wavenumber for the gravitational wave signal sidebands. Using equation 3.10 the unscaled amplitude and phase of the upper, α_{gw}^+ , and lower, α_{gw}^- , sidebands generated by a gravitational wave are then

$$A_{gw} = -\frac{w_0 h_0}{2\omega_{gw}} \sin\left(\frac{k_{gw} L}{2}\right), \quad (5.25)$$

$$\Phi_{gw}^\pm = \frac{\pi}{2} - L\left(k_0 \pm \frac{k_{gw}}{2}\right) \pm \varphi_{gw}, \quad (5.26)$$

$$\alpha_{gw}^\pm = A_{gw} e^{i\Phi_{gw}^\pm} e^{\pm i\omega_{gw} t}. \quad (5.27)$$

Note that α_{gw}^\pm must be scaled by the carrier field that is propagating into the space for the complete sideband amplitude.

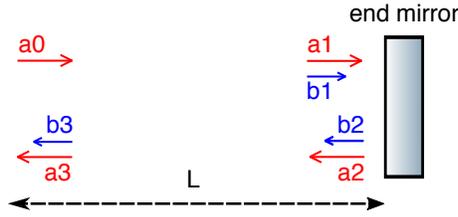


Figure 5.8: Simplified sketch of a single arm of the Michelson interferometer, the arrows show the carrier fields, denoted by a , and the signal sidebands b at the locations where they are computed.

To compute how a Michelson responds to a gravitational wave we must first consider the modulation of the carrier field travelling in both directions along the arms. Both the carrier and the created signal sideband fields propagate along each arm, as shown in Figure 5.8, and are reflected by a mirror with amplitude reflectivity r_{etm} . The relevant carrier fields are

$$a_3 = a_2 \exp(-i k_0 L), \quad (5.28)$$

$$a_2 = r_{etm} a_1, \quad (5.29)$$

$$a_1 = a_0 \exp(-i k_0 L). \quad (5.30)$$

The sidebands that are generated along such an arm are

$$\begin{aligned} b_1^\pm &= a_0 \alpha_{gw}^\pm, \\ b_2^\pm &= r_{etm} b_1^\pm, \\ b_3^\pm &= b_2^\pm \exp(-i(k_0 \pm k_{gw})L) + a_2 \alpha_{gw}^\pm, \\ &= 2r_{etm} a_0 \alpha_{gw}^\pm \exp\left(-i k_0 L \mp i \frac{k_{gw} L}{2}\right) \cos\left(\mp i \frac{k_{gw} L}{2}\right) \end{aligned} \quad (5.31)$$

and by substituting the sideband amplitude α_{gw}^\pm , see Equation 5.27, we find that:

$$b_3^\pm = -i \frac{r_{etm} a_0 w_0 h_0}{2\omega_{gw}} \sin(k_{gw} L) \exp(-i 2k_0 L) \exp(\pm(\omega_{gw} t - i k_{gw} L + \varphi_{gw})). \quad (5.32)$$

These are the sidebands that will leave the arm due to some gravitational wave modulating the space of an arm. One point to note is that the gravitational wave-induced sidebands can cancel themselves out for frequencies $f_{gw} = \frac{Nc}{2L}$.

Now we assume the Michelson interferometer is operated with a DC offset for the signal readout, see Section 5.4. For such a setup the field at the output port is given by equation 5.14 which when applied here gives:

$$E_{out} = i 2rt E_0 \cos(k_0 \Delta L) + b_N^+ + b_N^- + b_E^+ + b_E^- \quad (5.33)$$

The gravitational wave signal sidebands created in the north and east arms with perfect end mirrors, $r_{etm} = 1$, is given by 5.32 where care should be taken to use the correct lengths and carrier term: $b_N^\pm \equiv b_3^\pm$ with $L = L_N$, $a_0 = rE_0$ and $b_E^\pm \equiv b_3^\pm$ with $L = L_E$, $a_0 = itE_0$. These sidebands at the output port, once transmitted or reflected at the central beamsplitter again, are

$$b_N^\pm = \frac{rt E_0 w_0 h_0}{2\omega_{gw}} \sin(k_{gw} L_N) \exp(-i 2k_0 L_N) \exp(\pm(\omega_{gw} t - i k_{gw} L_N + \varphi_{gw})), \quad (5.34)$$

$$b_E^\pm = -\frac{rt E_0 w_0 h_0}{2\omega_{gw}} \sin(k_{gw} L_E) \exp(-i 2k_0 L_E) \exp(\pm(\omega_{gw} t - i k_{gw} L_E + \varphi_{gw})). \quad (5.35)$$

Note that an extra minus sign is included for the east arm sidebands because the gravitational wave modulate the north and east arms differentially. Next we will write the arm lengths in terms of a macroscopic differential ΔL , and common mode \bar{L} , lengths: $L_N = \bar{L} + \Delta L/2$ and $L_E = \bar{L} - \Delta L/2$. Along with this we also assume that the central beamsplitter has a 50:50 splitting ration $r = t = 1/\sqrt{2}$, that the common mode length is an integer number of wavelengths for the carrier light $\exp(i k_0 \bar{L}) = 1$, that $\bar{L} \gg \Delta L$, and that the gravitational wave's wavelength is much larger than ΔL , so $k_{gw}(\bar{L} + \Delta L/2) \approx k_{gw} \bar{L}$. Taking these assumptions into account the sideband terms become

$$b_N^\pm = \frac{E_0 w_0 h_0}{4\omega_{gw}} \sin(k_{gw} \bar{L}) \exp(-i k_0 \Delta L) \exp(\pm(\omega_{gw} t - i k_{gw} \bar{L} + \varphi_{gw})), \quad (5.36)$$

$$b_E^\pm = -\frac{E_0 w_0 h_0}{4\omega_{gw}} \sin(k_{gw} \bar{L}) \exp(i k_0 \Delta L) \exp(\pm(\omega_{gw} t - i k_{gw} \bar{L} + \varphi_{gw})). \quad (5.37)$$

Finally the sum of the sidebands at the output is

$$b_N^+ + b_N^- + b_E^+ + b_E^- = \frac{i E_0 w_0 h_0}{\omega_{gw}} \sin(k_{gw} \bar{L}) \sin(k_0 \Delta L) \cos(\omega_{gw} t - k_{gw} \bar{L} + \varphi_{gw}). \quad (5.38)$$

Now that we know the signal sideband fields at the output port, we can combine them with the carrier field that is also present:

$$\begin{aligned} E_{out} &= i E_0 \cos(k_0 \Delta L) + b_N^+ + b_N^- + b_E^+ + b_E^- \\ &= i E_0 \left[\cos(k_0 \Delta L) + \frac{w_0 h_0}{\omega_{gw}} \sin(k_{gw} \bar{L}) \sin(k_0 \Delta L) \cos(\omega_{gw} t - k_{gw} \bar{L} + \varphi_{gw}) \right]. \end{aligned} \quad (5.39)$$

A photodiode placed at the output of the Michelson will then measure the power in this beam from which we want to extract the gravitational wave amplitude, h_0 and phase, φ_{gw} . The power

in the beam contains multiple beat frequencies between all the carrier and signal sidebands, with the terms oscillating at the frequency ω_{gw} , are those linearly proportional to h_0 :

$$P_{gw} = |E_0|^2 \frac{w_0 h_0}{\omega_{gw}} \sin(k_{gw} \bar{L}) \sin(2k_0 \Delta L) \cos(\omega_{gw} t - k_{gw} \bar{L} + \varphi_{gw}). \quad (5.40)$$

As we are using DC readout, the differential arm length is chosen to operate slightly away from the dark fringe of the carrier field $\Delta L = \frac{\pi}{2k_0} + \delta_{\text{off}}$ as discussed in Section 5.4. The choice of DC offset is typically $\delta_{\text{off}} \ll \lambda_0$, the wavelength of the carrier light. So for small DC offset the power signal can be approximated as

$$P_{gw} \approx 2k_0 \delta_{\text{off}} |E_0|^2 \frac{w_0 h_0}{\omega_{gw}} \sin(k_{gw} \bar{L}) \cos(\omega_{gw} t - k_{gw} \bar{L} + \varphi_{gw}). \quad (5.41)$$

As described before, we now see that some DC offset is required to measure the signal; the DC offset provides the local oscillator field for the signal sidebands to beat with. Finally, the transfer function from a gravitational wave signal to the output photodiode, $T_{gw \rightarrow P}$, shows that the diode measures $T_{gw \rightarrow P}$ Watts per unit h_0 at frequency ω_{gw} :

$$T_{gw \rightarrow P}(\omega_{gw}) \approx k_0 \delta_{\text{off}} |E_0|^2 \frac{w_0}{\omega_{gw}} \sin(k_{gw} \bar{L}) e^{-i k_{gw} \bar{L}}. \quad (5.42)$$

For an example on how to model the response of a Michelson to a gravitational wave modelled using FINESSE see Section 5.6.3.

5.6 Finesse examples

5.6.1 Cavity power

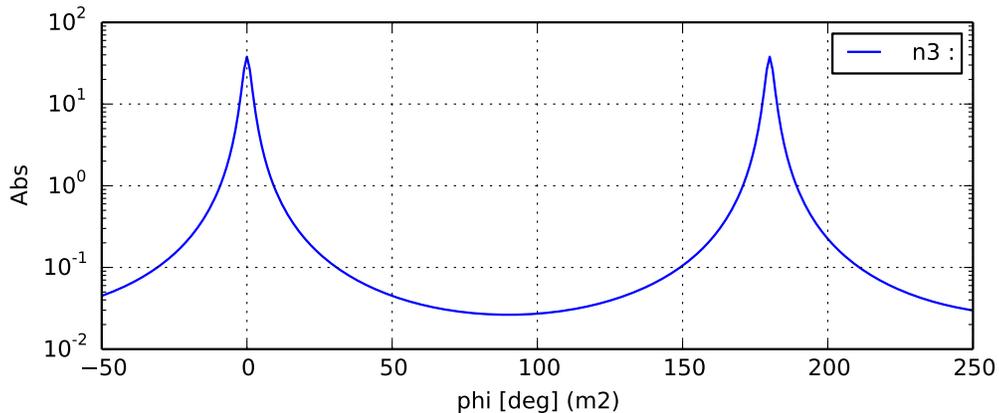


Figure 5.9: FINESSE example: Cavity power.

This is a simple FINESSE example showing the power enhancement in a two-mirror cavity as a function of the microscopic tuning of a mirror position (the position is given in degrees with 360 degrees referring to a change of longitudinal position by one wavelength). Compare this plot to the one shown in Figure 5.2, which instead shows the power enhancement as a function of the laser frequency detuning.

Finesse input file for ‘Cavity power’

```
laser l1 1 0 n1 % laser with P=1W at the default frequency
space s1 1 1 n1 n2 % space of 1m length
mirror m1 0.9 0.1 0 n2 n3 % cavity input mirror
space L 1200 1 n3 n4 % cavity length of 1200m
mirror m2 1.0 0.0 0 n4 dump % cavity output mirror
pd P n3 % photo diode measuring the intra-cavity power

yaxis log abs
xaxis m2 phi lin -50 250 300 % changing the microscopic tuning of mirror m2
```

5.6.2 Michelson power

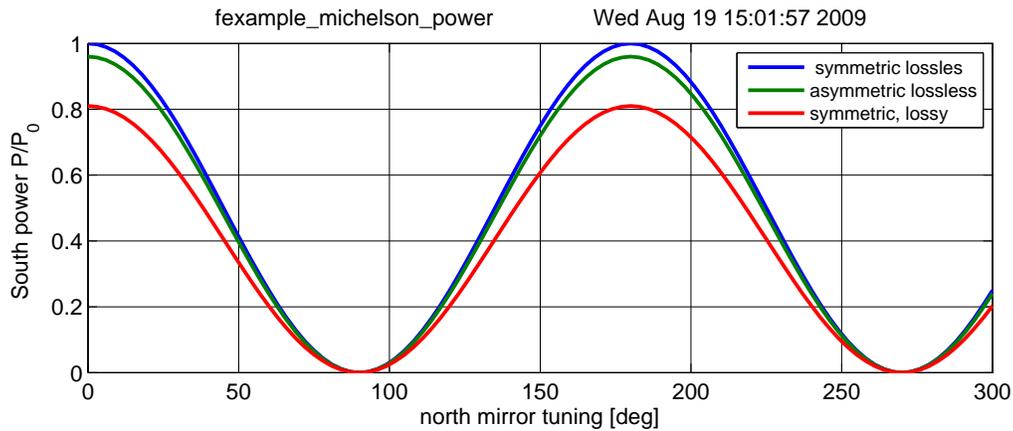


Figure 5.10: FINESSE example: Michelson power.

The power in the South port of a Michelson detector varies as the cosine squared of the microscopic arm length difference. The maximum output can be equal to the input power, but only if the Michelson interferometer is symmetric and lossless. The tuning for which the South port power is zero is referred to as the *dark fringe*.

Finesse input file for ‘Michelson power’

```
laser l1 1 0 n1 % laser with P=1W at the default frequency
space s1 1 1 n1 n2 % space of 1m length
% first trace: symmetric BS
bs b1 0.5 0.5 0 0 n2 nN1 nE1 nS1 % 50:50 beam splitter
% second trace:
%bs b1 0.4 0.6 0 0 n2 nN1 nE1 nS1 % 40:60 beam splitter
% third trace:
%bs b1 0.45 0.45 0 0 n2 nN1 nE1 nS1 % 45:45 beam splitter
space LN 1 1 nN1 nN2 % north arm
space LE 1 1 nE1 nE2 % east arm
```

```

mirror mN 1 0 0 nN2 dump % north end mirror, lossless
mirror mE 1 0 0 nE2 dump % east end mirror, lossless
space s2 1 1 nS1 nout
pd South nout % photo detector in South port
xaxis mN phi lin 0 300 100 % changing the microscopic position of mN

```

5.6.3 NEW: Michelson gravitational wave response

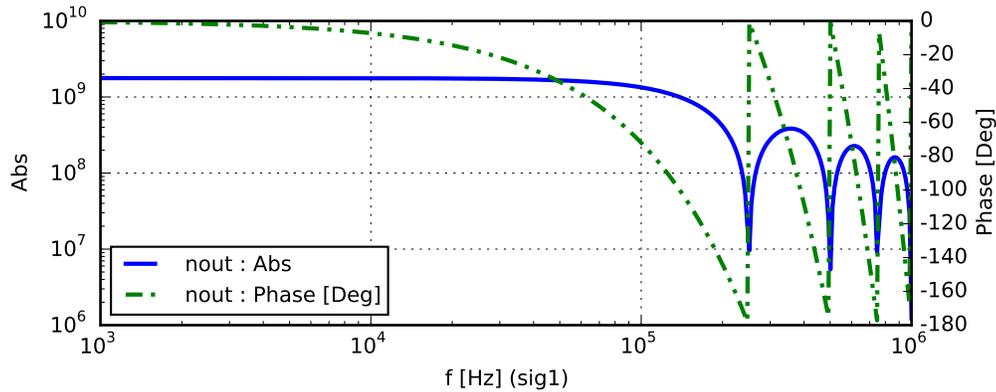


Figure 5.11: FINESSE example: Michelson sideband output from a gravitational wave

This is a simple FINESSE example showing how the arm spaces can be modulated to produce the effect a gravitational wave would have on it. It outputs the amplitude and phase of the upper sideband that reaches the output port.

Finesse input file for ‘Michelson gravitational wave response’

```

laser l1 1 0 nin
space s0 1 nin n1
bs BS 0.5 0.5 0 45 n1 ny1 nx1 nout
s syarm 600 ny1 ny2
m1 ETMy 100e-6 0 0 ny2 ny3
s sxarm 600 nx1 nx2
m1 ETMx 100e-6 0 90 nx2 nx3
# Apply a signal each arm with 180 phase difference between them
fsig sig1 syarm 1 180
fsig sig1 sxarm 1 0
# output the upper sideband
ad upper 0 nout
xaxis sig1 f log 1k 1M 400
# sets the ad detector frequency to the upper sideband freq.
put upper f $x1
yaxis log abs:deg

```

6 NEW: Radiation pressure and quantum fluctuations of light

Once classical noise sources are sufficiently reduced, the quantum fluctuations of light become one of the limiting noise sources for interferometric gravitational-wave detectors [36, 93, 116, 129]. To reduce this quantum noise the basic Michelson interferometer has been significantly altered over time, as we discuss in Section 7. This section aims to outline what quantum noise is and how its effects can be calculated.

The coupling of the quantum fluctuations of light into the output signal of the detector has traditionally been described as two separate effects: shot noise in the output current of the photodiodes and radiation pressure effects due to the use of suspended optics. Caves has shown that both noises can be understood as originating from vacuum fluctuations coupling into the dark port of the Michelson interferometer [46] and the two-photon formalism suggested by Cave and Schumaker [47] has led to a large body of work towards understanding and reducing quantum noise in gravitational wave interferometers [118, 113, 51, 127, 53, 43].

In the following we outline a method to compute quantum noise in interferometer output ports using sidebands and the classical framework presented in Sections 2, 3 and 4. We apply this method to investigate the quantum noise limits of several interferometer readout schemes and finally discuss how suspended optics effect the quantum noise.

The interested reader can explore this topic further with a modern and comprehensive treatment of quantum noise in the review provided in [55] and the following references: the standard quantum limit [46, 93] squeezing [105, 156] and quantum non-demolition interferometry [37, 77].

6.1 Quantum noise sidebands

The two quadratures of the light field, its amplitude and phase, form an observable conjugate pair thus both cannot be measured simultaneously without some uncertainty in the result [47]. This quantum noise of a single mode laser can be depicted as a phasor with the coherent carrier field and the addition of some stochastic Gaussian distributed noise which affects both its phase and amplitude [20, 116]. σ_ϕ^2 and σ_a^2 are the variances that characterise fluctuations in phase and amplitude respectively. The noise present in a light field with an equal, minimum σ_ϕ and σ_a is known as *vacuum fluctuation* or *vacuum noise*. Vacuum noise can be understood as the photon at all frequencies being incoherently created and annihilated. Therefore vacuum noise is all pervasive, existing at all locations in space, frequency and spatial mode. Such photons also enter our interferometer and limit the sensitivity of any measurement of a field's amplitude or phase.

Consider a carrier field at one location with amplitude a_0 and frequency ω_0 along with a continuum of noise fields (the positive frequency spectrum):

$$E(t) = \frac{a_0}{2} e^{i\omega_0 t} + \frac{1}{2} \int_0^\infty q(\omega) e^{i\omega t} d\omega + c.c. \quad (6.1)$$

where $q(\omega)$ is the Fourier component of a stochastic process, representing the vacuum fluctuation of the electric field.

We can rewrite the continuum of noise in reference to the carrier field frequency:

$$E(t) = \frac{a_0}{2} e^{i\omega_0 t} + \frac{e^{i\omega_0 t}}{2} \int_{-\omega_0}^\infty q(\omega_0 + \omega) e^{i\omega t} d\omega + c.c. \quad (6.2)$$

where we can view our quantum noise fields as sidebands of the carrier instead. For gravitational wave detectors the bandwidth B of the signals induced by a gravitational wave is of the order of

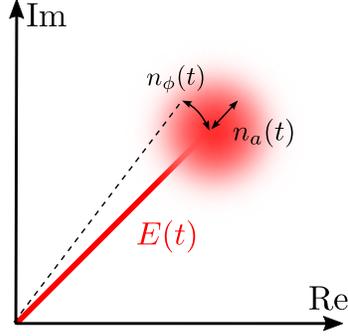


Figure 6.1: Phasor diagram of equation 6.4 depicting the Gaussian random amplitude and phase fluctuations due to vacuum noise. Here $n_{a,\phi}(t)$ are random gaussian noises in either the phase or amplitude of the carrier. Shown is only the positive frequency part of the carrier field, as $E(t)$ is real a conjugate negative frequency term also exists.

several kHz and thus $B \ll \omega_0$. Hence, we can focus on a small range of the noise sidebands that will actually affect our sensitivity:

$$E(t) = \frac{1}{2} \left[a_0 + \int_{-B}^B q(\omega_0 + \Omega) e^{i\Omega t} d\Omega \right] e^{i\omega_0 t} + c.c. \quad (6.3)$$

Here Ω will be used in notation to refer to frequencies in the signal bandwidth with $-B < \Omega \leq B \ll \omega_0$. We can also represent the quantum fluctuations as noise in both amplitude and phase:

$$E(t) = [a_0 + n_a(t)] e^{i\omega_0 t + n_\phi(t)/a_0} + c.c = [a_0 + n_a(t) + i n_\phi(t)] e^{i\omega_0 t} + c.c., \quad (6.4)$$

With n_a, n_ϕ being real amplitudes of the amplitude and phase fluctuations (of the stochastic process) with $n_a, n_\phi \ll 1$. This equation is represented in the phasor diagram in Figure 6.1.

We can now related the amplitude and phase fluctuation to the complex quantum noise $q(\omega)$:

$$q(\omega) = n_a(\omega) + i n_\phi(\omega) \quad (6.5)$$

Both $n_{a,\phi}(\omega)$ of a vacuum noise sideband are characterised by a Gaussian probability density function with a mean $\mu_{a,\phi} = 0$ and variance $\sigma_{a,\phi}^2$. Note that that the sidebands for the quantum noise are not representing a coherent and deterministic signal. This semi-classical approach is sufficient to motivate the design choices in laser interferometers for gravitational wave detection. A rigorous approach would require to use operators instead of sidebands. This approach is beyond the scope of this article, and instead fully covered in the review article [55].

The variances $n_{a,\phi}(\omega)$ are limited by the minimum uncertainty in the relation

$$\sigma_\phi \sigma_a \geq \frac{\hbar\omega}{2}, \quad (6.6)$$

which gives for an integration time of one second, $\sigma_\phi^2 = \sigma_a^2 = \hbar\omega/2$. As the phase and amplitude of $q(\omega)$ is random we can only compute its *expected value* or *ensemble value* at a particular frequency:

$$\langle q(\omega) \rangle = \langle \mu_a \rangle + i \langle \mu_\phi \rangle = 0, \quad (6.7)$$

which is zero as the mean of the noise is zero, hence on average no sidebands are actually observed. We can also consider the covariance between any two sidebands at frequency ω and ω' . As $q(\omega)$ is a

complex value there are multiple ways the covariance can be taken when considering the conjugates of either sideband, for example $\langle q(\omega)q^*(-\omega') \rangle$, $\langle q^*(\omega)q(-\omega') \rangle$, etc.. However as the fluctuations in amplitude and phase at different frequencies are independent, the covariance between any two vacuum noise sidebands are:

$$\langle q(\omega)q^*(\omega') \rangle = \frac{\hbar\omega}{2}\delta(\omega - \omega'), \quad (6.8)$$

$$\langle q(\omega)q(\omega') \rangle = 0, \quad (6.9)$$

The delta function in the covariance signifies there is no correlation between different frequencies. The auto-covariance is then $\langle q(\omega)q^*(\omega) \rangle \propto \delta(\omega - \omega) = \infty$, which may seem odd at a first glance. However, this can be better understood in the time domain picture, as we are measuring our signal over an idealistic infinite time span and as our noise is Markovian (and therefore also ergodic), the time average of the power of a signal will be infinitely large.

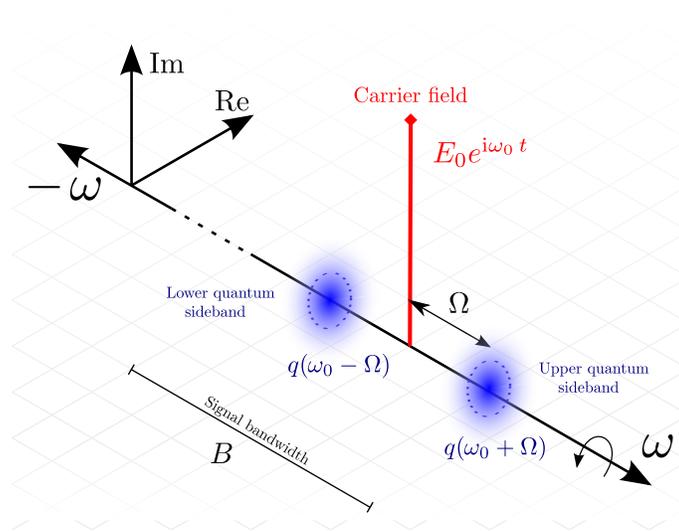


Figure 6.2: This diagram depicts a carrier field as shown in Figure 6.1 but expanded to show the vacuum noise sideband phasors that contribute towards the noise. The amplitude and phase of each sideband is a stochastic Gaussian noise so that its real and imaginary parts are described by some probability distribution depicted by the blue faded region, the dashed circle represents the standard deviation of such fluctuations. The signal bandwidth B can be imagined as containing an infinite number of such vacuum noise sidebands, each oscillating with a random phase and amplitude. Pictured are two upper and lower sidebands selected from this continuum of vacuum noise. The negative frequency phasors are not shown, they would be the mirrored conjugate versions of the positive phasors.

Noise power spectral densities

Noise, i.e. a random signal, can be quantified using a *power spectral density* (PSD) which is a measure of the power in a signal per frequency. The definition of a single-sided PSD of some frequency domain value $x(\omega)$ is:

$$S_{xx}(\omega)\delta(\omega - \omega') = 2 \langle x(\omega)x^*(\omega') \rangle, \quad (6.10)$$

with units $[x]^2/\text{Hz}$. The cross-spectral-density between two values $x(\omega)$ and $y(\omega)$ is similarly:

$$S_{xy}(\omega)\delta(\omega - \omega') = 2 \langle x(\omega)y^*(\omega') \rangle. \quad (6.11)$$

The eventual physical noise we wish to compute is the noise in the demodulated photocurrent of the photodiode measuring the interferometer output signal, here we will consider only photodiodes with 100% quantum efficiency⁸. The photocurrent I is proportional to the detected light power $I(t) \sim P(t)$ and the PSD of the noise in the photocurrent is:

$$S_I(\omega)\delta(\omega - \omega') = 2 \langle I(\omega)I^*(\omega') \rangle \quad (6.12)$$

The DC and $\omega \pm \Omega$ terms of the power on a photodiode for a single carrier with quantum noise sidebands is:

$$\begin{aligned} P(t) = E(t)E^*(t) &= |a_0|^2 + a_0^* \int_{-B}^B q(\omega_0 + \Omega)e^{i\Omega t} d\Omega \\ &+ a_0 \int_{-B}^B q^*(\omega_0 + \Omega)e^{-i\Omega t} d\Omega + O(q^2), \end{aligned} \quad (6.13)$$

terms of the order q^2 are assumed to be a negligibly small contribution. The positive half of the photocurrent spectrum for $0 < \Omega \leq B$ is given by its Fourier transform:

$$I(\Omega) \equiv \mathcal{F}[I(t)] = a_0^*q(\omega_0 + \Omega) + a_0q^*(\omega_0 - \Omega) \quad (6.14)$$

The spectrum for frequencies in the signal bandwidth is thus defined by just quantum noise scaled by the carrier field. From this point on for the sake of brevity we will define the following notation without the carrier frequency, as we are only using a single carrier for this derivation:

$$q(\omega_0 \pm \Omega) \Rightarrow q_{\pm} \quad \text{and} \quad q(\omega_0 \pm \Omega') \Rightarrow q'_{\pm} \quad (6.15)$$

Using equations 6.12 and 6.14, the PSD of the photocurrent is:

$$S_I(\Omega)\delta(\Omega - \Omega') = 2P_0(\langle q_+q_+^* \rangle + \langle q_-q_-^* \rangle) + 2a_0^2\langle q_-q_+^* \rangle^* + 2a_0^2\langle q_+q_-^* \rangle. \quad (6.16)$$

Now applying equations 6.8 and 6.9 in equation 6.16 the noise PSD for a single carrier field with vacuum noise is:

$$\begin{aligned} S_I(\omega_0 \pm \Omega)\delta(\Omega - \Omega') &= 2P_0 (\langle q_+q_+^* \rangle + \langle q_-q_-^* \rangle), \\ &= P_0 (\hbar(\omega_0 + \Omega) + \hbar(\omega_0 - \Omega)) \delta(\Omega - \Omega') \\ S_I(\omega_0 \pm \Omega) &= 2P_0\hbar\omega_0 \end{aligned} \quad (6.17)$$

Here we see that the quantum noise of a single carrier field does not depend on the sideband frequency Ω . The vacuum fluctuations interfering with our carrier field produces a broadband frequency-independent noise source proportional to the carrier power and frequency. It should also be noted that equation 6.17 is the same result as the semi-classical Schottky shot-noise equation, equation 6.44. An interesting aspect to note here are the differing reasons for the presence of this quantum or shot noise. The Schottky formula derives this noise from the Poisson statistics of electrons generated in the photocurrent due to the light field power. Whereas the quantum approach reasons that such fluctuations in the photocurrent are in fact due to vacuum noise superimposing itself onto our light fields introducing a noise into our measurements.

The description of quantum noise with semi-classical sidebands has the advantage that the propagation of a stochastic signal through a linear system is described by the same transfer functions as for a deterministic signal. Therefor we can use the classical model of the optical system to compute the propagation of the quantum noise as well as any signal.

⁸ It is proportional to a factor χ , the photodiodes quantum efficiency, which states how many Amps per Watt of incident power is output by the photodiode. We will assume here the efficiency is perfect, $\chi = 1$, for simplicity.

6.2 Vacuum noise and gravitational wave detector readout schemes

Let us now consider a Michelson interferometer, as described in Section 5.2, and the limiting sensitivity due to vacuum noise leaking into the detector. Figure 6.3 depicts two exemplary readout schemes for measuring the gravitational wave signal. For both schemes we can identify the sources of vacuum noise that will enter the interferometer. The input is assumed to be a perfect single mode laser whose noise is purely vacuum noise. The end mirrors in the arms are taken to be perfectly reflective thus no vacuum noise enters through them; however if $r < 1$ any vacuum noise leaking out would be replaced with an equal amount of uncorrected noise injected back in. The output port is fully open and thus allow vacuum noise to enter into the system proving the primary contribution of noise in Michelson setup used for gravitational wave detectors. This is due to the fact that such the Michelson is operated on the dark fringe for the input carrier, meaning any the laser noise will leave the system back towards the laser, whereas the noise entering through the output port will return to the output port.

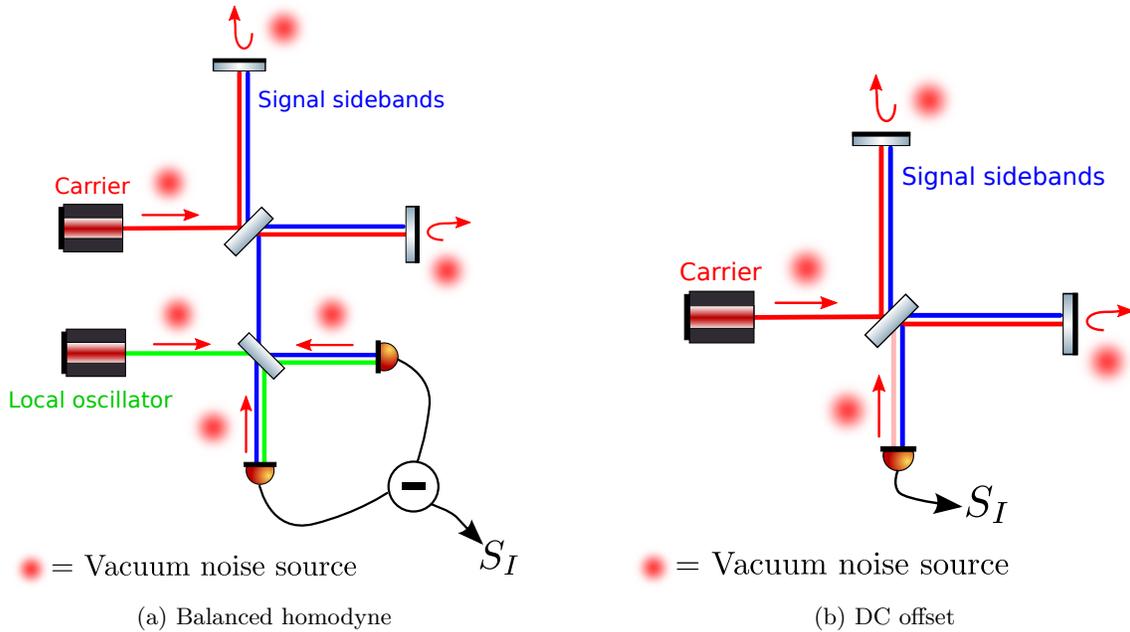


Figure 6.3: Shown are two possible readout schemes that can be used to extract signal sideband information from a Michelson along with the various classical fields and sources of vacuum noise.

When no non-linear optical effects (effects proportional to the beams power) are present in an interferometer and the only quantum noise present is uncorrelated vacuum noise, there will always be the same amount of vacuum noise incident on any photodiode. This is irrespective of the topology of the interferometer or components used because noise can never be effectively lost from the system; an equivalent amount of uncorrelated noise is always injected back in. In such cases propagation of the noise sidebands through the interferometer do not need to be computed. Instead, when computing S_I at any of the photodiodes shown in Figure 6.3 we only need to consider pure vacuum noise sidebands and the local oscillator field, E_{LO} ; the source of location of the vacuum noise sources is not of importance. This is why for early generation gravitational wave detectors, which had negligible non-linear optical effects, the semi-classical Schottky expression could be used to estimate the quantum noise correctly.

The detailed computation of quantum noise limited sensitivity of a detector depends on the

readout scheme used. Early generations of gravitational wave detectors such as LIGO, Virgo, GEO 600 and TAMA300 used heterodyne readout schemes, where RF modulation sidebands applied to the input field are used as local oscillators at the output (see Sections 5.4). However, such schemes included some technical challenges, the oscillator noise of the RF modulator being one of them, and also increase the shot-noise level when demodulating the photocurrent [116, 129, 136, 43]. Thus the next generation of detectors opted for a DC readout scheme [73, 90], see Section 8.16. Both schemes depicted in Figure 6.3 use a form of DC readout, which we will analyse in more detail in the following sections. We do not cover the computation of quantum noise with RF modulation readout schemes, the interested reader should see [84, 136, 43].

Noise-to-signal ratio for DC offset

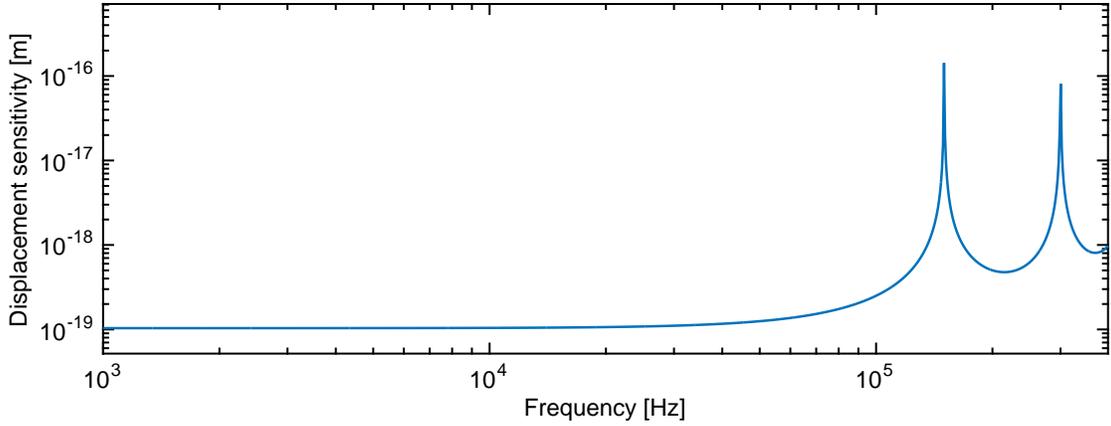


Figure 6.4: Shot-noise limited sensitivity of a Michelson, see Equation 6.21, with $\bar{L} = 1000$ m, $R = T = 0.5$ and $P_0 = 1$ W.

A DC offset in the main Michelson interferometer (see Section 5.4) provides a local oscillator by operating slightly away from the dark fringe for the carrier allowing some to leak through to the output port along with any signal sideband fields. The sources of vacuum noise that will contribute to the quantum noise are shown in Figure 6.3b; however, as stated previously the total amount of noise present at the photodiode will be just pure vacuum noise as no non-linear optical effects are assumed. The local oscillator field at the output is given by Equation 5.11 and along with the vacuum noise sidebands the output field is:

$$E_{out} = \left[i E_0 e^{-i2k\bar{L}} \sin(k_0 \delta_{off}) + q_+ e^{i\Omega t} + q_- e^{-i\Omega t} \right] e^{i\omega_0 t}. \quad (6.18)$$

where we have used the dark fringe offset as stated in Equation 5.13. The quantum noise PSD when using a DC offset is now essentially the same scenario as when deriving Equation 6.17, where a single carrier and noise sidebands were considered; except that the carrier power now depends on δ_{off} :

$$S_{P,DC} = \langle |P_{out}(\Omega)|^2 \rangle = 2P_0 \sin^2(k_0 \delta_{off}) \hbar\omega_0 \approx 2P_0 (k_0 \delta_{off})^2 \hbar\omega_0, \quad (6.19)$$

where P_0 is the power of the laser injected into the Michelson and $k_0 \delta_{off} \ll 1$.

To compute the noise-to-signal (NSR) ratio, which is used to describe the sensitivity of our Michelson, the transfer function from a signal we want to measure to the photodiode output is

required. Here we will use the gravitational wave signal transfer function from equation 5.42 which describes the Watts of power per unit of strain, h , at the output detector

$$|T_{gw \rightarrow P}(\omega_{gw})| \approx k_0 \delta_{\text{off}} P_0 \frac{w_0}{\omega_{gw}} \sin\left(\frac{\omega_{gw} \bar{L}}{c}\right) \text{ W/h.} \quad (6.20)$$

We note that $T_{gw \rightarrow P}$ refers to the *amplitude* of the differential length modulation that the arms experience. Thus the NSR should be computed with the *amplitude spectral density* given as $\text{ASD} = \sqrt{\text{PSD}}$:

$$\text{NSR} = \frac{\sqrt{S_{P,DC}}}{T_{gw \rightarrow P}} = \sqrt{\frac{2\hbar}{P_0 \omega_0} \frac{\omega_{gw}}{\sin(\omega_{gw} \bar{L}/c)} \frac{h}{\sqrt{\text{Hz}}}} \quad (6.21)$$

The displacement sensitivity does not depend on the DC offset and can be improved, for example, by increasing the laser power. However, eventually building a more powerful laser is not possible without sacrificing its required stability in power and frequency. Instead we can also use Fabry-Perot cavities to increase the effective power inside the interferometer, see Section 7.

Noise-to-signal ratio for balanced homodyne

Balanced homodyne readout involves the use of an external local oscillator whose optical frequency is the same as the main carrier light in the interferometer. The main Michelson interferometer is operated on the dark fringe for the carrier so no carrier light is present at the output port. This local oscillator is mixed with the signal sidebands using a beamsplitter, such a setup is depicted in Figure 6.3a and in more detail for the readout in Figure 6.5. As the signal sidebands are now split into two optical paths we require two photodiodes to measure the signal, otherwise half the signal will be lost instantly. The balanced aspect of this readout scheme refers to the fact that the two photocurrents I_a and I_b are combined in such a way that the noise from either the local oscillator port or the signal port can be completely removed from the measurement.

No current generation gravitational-wave detector uses this form of homodyne readout for extracting gravitational wave signals. This has been due to the additional technical challenges which are not present when using DC readout. It is however used extensively for quantum noise measurements when non-vacuum states are injected into interferometers [151, 52] and offers potential benefits over DC readout if the technical challenges can be overcome, as we show later in this section. Although not currently used, such a readout scheme is a current topic of investigation for future generations of detectors for extracting gravitational wave signals [76].

There are two possible sources for the local oscillator field when using balanced homodyne detection: a separate laser system or a pick-off of the same carrier field used in the interferometer. The former is technically challenging as the separate system must be locked to the input laser to ensure temporal coherence when beating with the signal sidebands. The latter option of using a pick-off beam does not have this issue as it is from the same laser. Other technical challenges that exist for both options are [114] that the beamsplitter is exactly 50:50; that the signal sidebands and local oscillator fields have a particularly good spatial overlap, also referred to as *mode-matching* and that the local oscillator does not back-scatter into the output port of the interferometer.

Assuming a perfect 50:50 beamsplitter and a coherent local oscillator which is well aligned to some signal beam we want to measure, both the incoming signal and local oscillator include vacuum noise. To calculate the photocurrent noise S_I we describe the noise sidebands are as shown in Figure 6.5:

$$\begin{aligned} E_a &= [r(n_1^+ e^{i\Omega t} + n_1^- e^{-i\Omega t}) + i t(E_{LO} + n_2^+ e^{i\Omega t} + n_2^- e^{-i\Omega t})] e^{i\omega_0 t} \\ E_b &= [r(E_{LO} + n_2^+ e^{i\Omega t} + n_2^- e^{-i\Omega t}) + i t(n_1^+ e^{i\Omega t} + n_1^- e^{-i\Omega t})] e^{i\omega_0 t} \end{aligned} \quad (6.22)$$

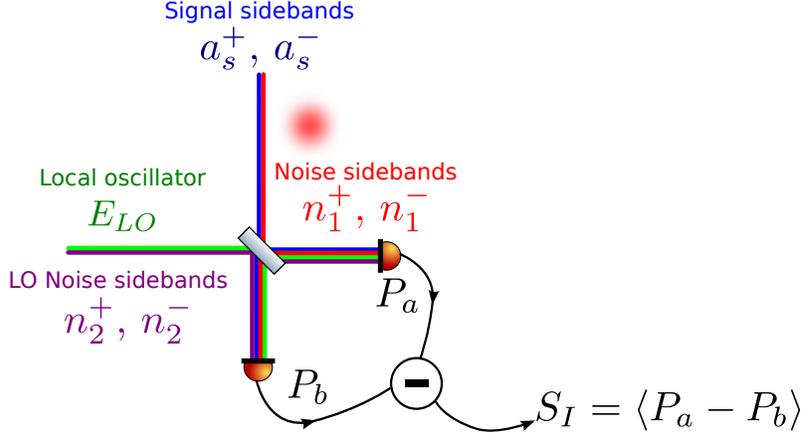


Figure 6.5: The signal and noise fields in the homodyne detector as used in the balanced homodyne readout scheme.

The photocurrent noise PSD is then proportional to:

$$S_I \propto \langle |E_a E_a^* - E_b E_b^*|^2 \rangle \quad (6.23)$$

The for the incident power on each photodiode we ignore noise terms that are not scaled by the local oscillator as negligible:

$$\begin{aligned} P_a(t) &= -itE_{LO}^* [r(n_1^+ e^{i\Omega t} + n_1^- e^{-i\Omega t}) + it(n_2^+ e^{i\Omega t} + n_2^- e^{-i\Omega t})] + c.c \\ P_b(t) &= rE_{LO}^* [it(n_1^+ e^{i\Omega t} + n_1^- e^{-i\Omega t}) + r(n_2^+ e^{i\Omega t} + n_2^- e^{-i\Omega t})] + c.c \end{aligned} \quad (6.24)$$

Assuming that each photodiode is identical in its response to the power, the photocurrents proportional to these two powers can then be subtracted or summed:

$$P_a(t) \pm P_b(t) = E_{LO}^* [irt(n_1^+ e^{i\Omega t} + n_1^- e^{-i\Omega t})(-1 \pm 1) + (n_2^+ e^{i\Omega t} + n_2^- e^{-i\Omega t})(T \pm R)] + (6.25)$$

This shows that either the noise from the local oscillator, n_2^\pm , or that coming along with the signal, n_1^\pm , can be removed. Typically the local oscillator noise will be larger than that accompanying the signal thus we can compute $P_a - P_b$ to remove it. It can also be seen here if the beamsplitter is not 50:50, $R \neq T$, the local oscillator noise cannot be fully removed. Finally the subtracted photocurrent for the sideband frequency Ω is:

$$P_{a-b}(\Omega) \equiv \mathcal{F}[P_a(t) - P_b(t)](\Omega) = -iE_{LO}^*(n_1^+ + n_1^{-*}), \quad (6.26)$$

where $r = t = 1/\sqrt{2}$. For pure vacuum noise, $n_1^\pm \Rightarrow q_\pm$, the resulting photocurrent noise PSD for this is that given by Equation 6.17:

$$\begin{aligned} S_I &= \langle |P_{a-b}(\Omega)|^2 \rangle = 2P_{LO} (\langle q_+ q_+^* \rangle + \langle q_- q_-^* \rangle), \\ &= 2P_{LO} \hbar \omega_0 \end{aligned} \quad (6.27)$$

Therefore if correctly balanced the quantum noise is no greater than what is present for a DC offset readout. If the local oscillator power P_{LO} is identical to the carrier power in the DC offset scheme, then the sensitivity for the balanced homodyne detection is the same as that for the DC offset detection, stated in Equation 6.21, because the transfer function from signal to the two

photodiodes is essentially the same. One aspect where it differs however is the phase of the local oscillator relative to the signal sidebands which is now a free parameter, which is known as the *homodyne angle* or the *readout phase*. When using a DC offset readout scheme the readout phase is essentially fixed. Having the ability to vary this readout phase provides an extra degree of freedom for optimising the quantum noise-to-signal ratio for gravitational wave signals. This is an assumed feature in some *quantum non-demolition* schemes [40, 38] which introduce new methods for reducing the quantum noise [135, 98, 97, 50, 51].

6.3 Quantum noise with non-linear optical effects or squeezed states

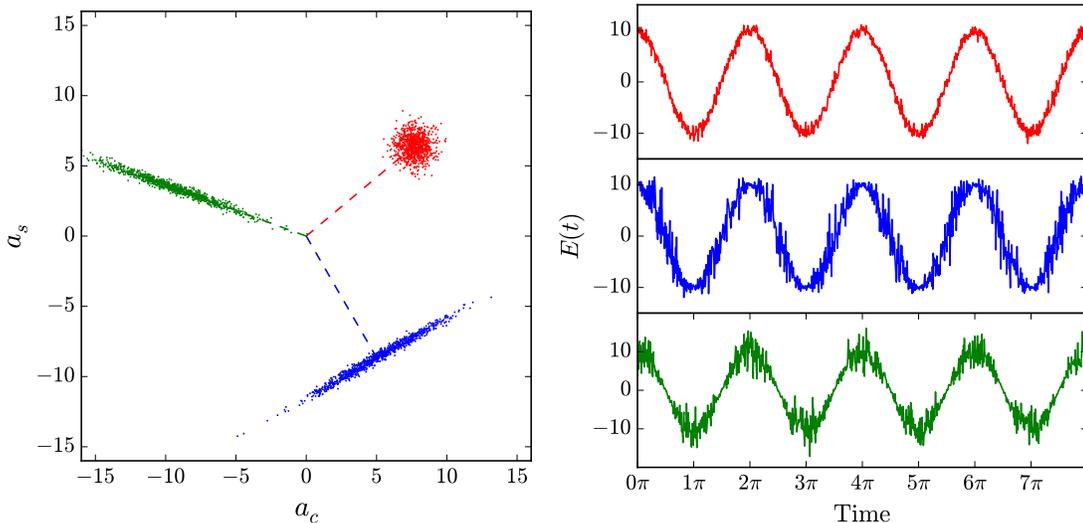


Figure 6.6: Depicted are the phasor and the time signals of pure vacuum noise (Red), amplitude-squeezed (Blue) and phase-squeezed (Green) noise. The effect here is greatly exaggerated to produce a visible noise thus the scaling on the axes do not represent any realistic values. The phasor diagram shows $E(t)$ at some arbitrary time value and each point is a sample retrieved from the probability density function of the noise. The squeezed states show clearly a correlation between phase and amplitude fluctuations; the area of each state is equal representing the minimum given by the uncertainty relation 6.6.

Up to this point we have only considered pure vacuum noise and linear optical effects, which are valid approximations for previous generations of gravitational wave detectors. As the effective laser power in the interferometer is increased to reduce shot noise, the radiation pressure exerted on suspended optics by the circulating laser beams will increase another noise significantly, the *radiation pressure noise*. Any fluctuations in the laser's power will couple back into itself as phase modulation due to the radiation pressure induced motion of the mirror, such noise is prominent at low frequencies. The effect is a non-linear process as the amplitude of the motion is proportional to the power in the beam, which leads to both the upper and lower sidebands becoming correlated with one another. Further details on this opto-mechanical coupling are outlined in Section 6.4.

Then there is also the possibility of *squeezing* the vacuum noise, whereby still satisfying the relationship 6.6, the uncertainty in either the phase or amplitude is increased whilst being and decreased in the other. This squeezed noise can be represented by correlated noise sidebands [47, 55], Figure 6.6 shows qualitatively the effect of squeezed vacuum noise on a coherent field. Injecting

squeezed noise into the output port of the interferometer can thus reduce the dominant vacuum noise. Upon returning to the output port the noise should still be squeezed, but to a slightly lesser degree due to various optical losses which degrade the amount of squeezing. If designed correctly the noise can be reduced below the typical shot-noise level of $2P_0\hbar\omega_0$, thus providing a broad improvement in shot-noise limited regions of the detectors sensitivity [46]. Although we will not cover squeezing in detail in this article, squeezed light injection has been used routinely by the GEO 600 detector for several years [155], and further upgrades to advanced gravitational wave detectors using squeezed light sources are actively being developed [130].

One important aspect to note here is that when either non-linear optical effects or non-vacuum states of light are considered the individual propagation of light fields through the interferometer now have to be considered. This is due to the fact such noise sidebands will be altered in amplitude and phase and the relative correlation between sidebands once propagated through the system becomes an important feature. This involves constructing the full interferometer matrix, see Section 2.3, for the noise sideband frequencies and including, if so required, the radiation pressure coupling at suspended mirrors as discussed in the next section.

6.4 Radiation pressure coupling at a suspended mirror

As the laser power is increased to reduce the shot-noise, the increased power results in a significant radiation pressure force being exerted on the interferometer mirrors. The frequency spectrum of the force exerted on a perfectly reflectivity mirror by a single beam with power $P(\Omega)$ is given by [117]

$$F_{rp}(\Omega) = \frac{2P(\Omega)}{c}. \quad (6.28)$$

In order to attenuate seismic vibrations and produce free-masses as probes for gravitational waves, the mirrors in gravitational wave detectors are suspended via a series of active and passive suspension systems. At frequencies well above the resonances of the suspension systems the mirrors can be considered to be free (or quasi-free). Any fluctuation in the light power induces a motion in the suspended mirrors. This process converts power fluctuations into phase fluctuations, and this coupling can lead to opto-mechanical effects such as *optical springs*, which couple the motion of multiple suspended optics together [144, 17].

The induced longitudinal motion of a suspended mirror due to N_f separate forces being applied to it is:

$$\delta z(\Omega) = H(\Omega) \sum_{n=0}^{N_f} F_n(\Omega), \quad (6.29)$$

where $H(\Omega)$ is the *mechanical susceptibility* or *mechanical transfer function* from a force applied to motion parallel to the mirrors surface normal. Similar relationships are possible for rotational motions considering torques applied to the mirror.

Mechanical transfer functions

The transfer function $H(\Omega)$ is determined by the specific setup of the suspension systems. The various resonances and features of the system can be represented with an expansion into *poles and zeros*:

$$\begin{aligned} H(\Omega) &= -\frac{1}{M\Omega^2} \frac{\prod_{k=1}^{N_z} (i\Omega - \mathcal{Z}_k)(i\Omega - \mathcal{Z}_k^*)}{\prod_{j=1}^{N_p} (i\Omega - \mathcal{P}_j)(i\Omega - \mathcal{P}_j^*)} \\ \mathcal{P}_k &= \Omega_{p,k} \left(i - \frac{1}{2Q_{p,k}} \right), \quad \mathcal{Z}_j = \Omega_{z,k} \left(i - \frac{1}{2Q_{z,k}} \right) \end{aligned} \quad (6.30)$$

where M is the mass of the mirror in kg, $\{\Omega_{p/z,i}\}_{i=1}^{N_{p/z}}$ is a set of frequencies for each pole and zero and $\{Q_{p/z,i}\}_{i=1}^{N_{p/z}}$ the respective quality factors. When the frequencies of interest (signal frequencies) are much higher than any pole or zero frequency, $\Omega \gg \Omega_{p/z}$, we can assume a *free mass*, $N_z = 0$ and $N_p = 0$:

$$H(\Omega) = -\frac{1}{M\Omega^2}. \quad (6.31)$$

Approximations for radiation pressure

With the mirror position change being proportional to the laser power, $\delta z \propto P$, the problem is non-linear in terms of the complex field amplitudes. Solving such a problem in a complex interferometer setup is challenging and not possible using the methods outlined in Section 2, as the frequency domain model is assuming a linear system. However, for gravitational wave detectors we can make some assumptions about the system:

- the motion of any optic is small, $|\delta z| \ll \lambda$, when the interferometer is controlled and well-behaved, and we can linearise equations in δz ,
- any high-frequency fluctuations in the beam are negligible due to $H(\Omega) \propto 1/\Omega^2$ and we ignore the effects of RF sidebands on the optics,
- any low-frequency fluctuations are very small, such that the magnitude of any sidebands is much less than the magnitude of its carrier field, which allows us to identify a well defined carrier field in our calculations.

These are all valid assumptions for gravitational wave detectors once they are operating in a steady state and have well controlled optics. For a single carrier with amplitude E_0 and frequency ω_0 and noise sidebands at frequency Ω , the incident field on a suspended mirror is:

$$E_i = (E_0 + q_+ e^{i\Omega t} + q_- e^{-i\Omega t}) e^{i\omega_0 t} + c.c. \quad (6.32)$$

As with the approximations listed above we can assume $|q_{\pm}| \ll |E_0|$ and $\omega_0 \gg \Omega$. The fluctuation in the beam power is then given by:

$$P(\Omega) = q_+ E_0^* + q_-^* E_0 \quad (6.33)$$

where we only consider sideband-carrier product terms and those with a frequency Ω . Substituting the fluctuating power 6.33 into the radiation pressure force 6.28 to compute the displacement 6.29 the motion of the mirror can be found. The amplitude of the motion at frequency Ω induced via radiation pressure for a perfectly reflective, free-mass mirror is

$$\delta z = -\frac{2}{Mc\Omega^2} (q_+ E_0^* + q_-^* E_0). \quad (6.34)$$

Such a moving mirror, as discussed in Section 3.2, creates phase modulation sidebands around any carrier that is reflected from it. The reflected field, using Equation 3.10, is:

$$E_r = E_i \left(1 + \frac{ik_0}{2} (\delta z^+ e^{-i\Omega t} + \delta z^- e^{i\Omega t}) \right) e^{i\omega_0 t}, \quad (6.35)$$

where to keep notation simpler, $\delta z^+ \equiv \delta z$ and $\delta z^- \equiv \delta z^*$.

Take the simple example of vacuum noise and a single carrier, with amplitude E_0 , incident on a free mass mirror of mass M and calculate the noise after being reflected. The amplitude of the

reflected upper and lower noise sidebands, $q_{r,\pm}$, using Equations 6.29 and 6.35, are:

$$\begin{aligned} q_{r,\pm} &= v_{\pm} + i E_0 k_0 \frac{\delta z^{\pm}}{2}, \\ &= v^{\pm} - i E_0 k_0 \frac{v_{\pm} E_0^* + v_{\mp}^* E_0}{M c \Omega^2}. \end{aligned} \quad (6.36)$$

where v_{\pm} are the incident pure vacuum noise sidebands. (6.36) shows that the reflected upper and lower noise sidebands are now a mix of the incident upper and lower sidebands, or that they after reflection they now correlated. Seen here is the additional phase noise now present which scales as $\propto |E_0|/\Omega^2$. Thus, this noise is relevant at low frequencies and when the beam power to mass ratio is significant.

The noise PSD for the reflected beam is computed using equation 6.16. This requires computing the various covariance and auto-covariances of the reflected noise sidebands 6.36 and their beating with the carrier field:

$$\langle q_{r,\pm} q'_{r,\mp} \rangle = -\frac{\hbar \omega_0 E_0^2}{M \Omega^2 c} \left(k_0 + \frac{|E_0|^2 k_0^2}{M \Omega^2 c} \right) \quad (6.37)$$

$$\langle q_{r,\pm} q_{r,\pm}^* \rangle = \frac{\hbar(\omega_0 \pm \Omega)}{2} + \frac{\hbar \omega_0 |E_0|^4 k_0^2}{M^2 c^2 \Omega^4}. \quad (6.38)$$

To simplify the above we will also assume the carrier has zero phase, $E_0^* = E_0$ and that $E_0 = \sqrt{P_0}$. The power noise PSD using equation 6.16 is then

$$\begin{aligned} S_I(\Omega) &= 2P_0(\langle q_{r,+} q_{r,+}^* \rangle + \langle q_{r,-} q_{r,-}^* \rangle) + 2P_0 \langle q_{r,-} q'_{r,+} \rangle^* + 2P_0^* \langle q_{r,+} q'_{r,-} \rangle \\ &= 2\hbar \omega_0 P_0. \end{aligned} \quad (6.39)$$

Thus the noise is still just a flat shot noise limit, as is expected. However, this only shows the amplitude noise in the beam, not any phase noise. To compute the phase quadrature the local oscillator must have an additional $\pi/2$ phase relative to the sidebands. Experimentally this could be achieved using the balanced homodyne readout as mentioned in previous sections. Here though we can cheat by simply adding an additional phase to the carrier to the beam *after* reflection, i.e. compute the PSD of a power fluctuation

$$P(\Omega) = q_+ E_0^* e^{-i\phi} + q_-^* E_0 e^{i\phi} \quad (6.40)$$

where ϕ is our additional homodyne phase. Computing the PSD of this with $\phi = \pi/2$ to compute the phase fluctuations we see:

$$S_{\phi}(\Omega) = 2P_0 \hbar \omega_0 + \frac{8\hbar P_0^3 \omega_0 k_0^2}{M^2 c^2 \Omega^4}. \quad (6.41)$$

Here there is a flat shot noise fluctuation plus additional phase noise due to the vacuum noise perturbing the mirror. In the limit of an infinitely heavy mirror we can see this radiation pressure noise is removed and we are left with the vacuum noise fluctuations in phase. It is these phase fluctuations that are converted from phase to amplitude noise at the Michelson dark port that then lead to quantum noise limited sensitivity of the detector at the output photodiode.

6.5 Semi-classical Schottky shot-noise formula

Shot noise historically has been described as the noise arising from the statistical distribution of electrons in photo detectors. The Schottky formula for the (single-sided) power spectral density of the fluctuation of the photocurrent for a given mean current \bar{I} is:

$$S_I(f) = 2e\bar{I}, \quad (6.42)$$

with e the electron charge. Here $S_X(f)$ denotes the single-sided power spectral density of X over the Fourier frequency f . The link between (mean) photocurrent \bar{I} and (mean) light power \bar{P} is given by the relation:

$$\bar{I} = eN = \frac{e \eta \lambda}{\hbar 2\pi c} \bar{P}, \quad (6.43)$$

with N as the number of photons and η the quantum efficiency of the diode. Instead of Planck's constant we write $\hbar 2\pi$ to avoid confusion with the typical use of $h(t)$ for the strain of a gravitational wave. We can now give a power spectral density for the fluctuations of the photocurrent:

$$S_P(f) = 2 \frac{2\pi \hbar c}{\lambda} \bar{P}. \quad (6.44)$$

As stated above this equation estimates the shot noise correctly when the interferometer does not contain any non-linear effects or squeezed input fields.

6.6 Optical springs

Optical springs are a result of a feedback loop being created by the optical field scattered by a suspended mirror being fed back in to itself. Using the opto-mechanical coupling laid out in the previous section it will be shown how this feedback process introduces a force that is analogous to a damped spring being attached to the mirror. This optical spring will have a particular resonance frequency and damping coefficient that depends on the optical and mechanical properties of the interferometer.

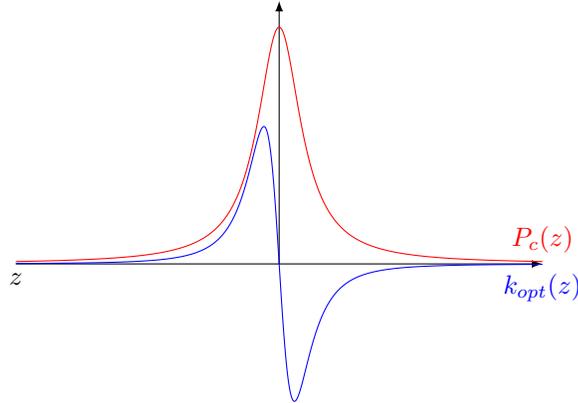


Figure 6.7: Illustrative example of the circulating power (red) in a Fabry-Perot cavity. The blue line shows the spring constant (blue). Not to scale.

Adiabatic optical spring

A Fabry-Perot cavity with a suspended end mirror is the simplest system which can feedback the sidebands created to the mirror. Firstly the case when the mirror is moving slowly compared to the round-trip time of the cavity is considered. In this case the optical response to a mirror moving is effectively instantaneous throughout the interferometer. The power circulating in a Fabry-Perot cavity, hence the power incident on the suspended mirror, as a function of a cavity length change z in meters is:

$$P_c(z) = \frac{P_0 T_1}{1 + R_1 R_2 - 2r_1 r_2 \cos(2kz)} \quad (6.45)$$

and shown in figure 6.7. As the radiation pressure force is $\propto P_c$ the force varies with respect to the end mirror's position. A position dependent force is the definition of a spring constant, thus for our optical spring we find:

$$k_{opt} = -\frac{dF(z)}{dz} = \frac{d}{dz} \left[\frac{-2P_c(z)}{c} \right] = \frac{-8P_0 r_1 r_2 k T_1 \sin(2kz)}{c(1 + R_1 R_2 - 2r_1 r_2 \cos(2kz))^2}. \quad (6.46)$$

Plotting the k_{opt} in figure 6.7, when the cavity is perfectly resonant for the carrier field there is no optical spring, for positive δz we have a restoring force, $k_{opt} < 0$, and anti-restoring force, $k_{opt} > 0$, with negative detunings.

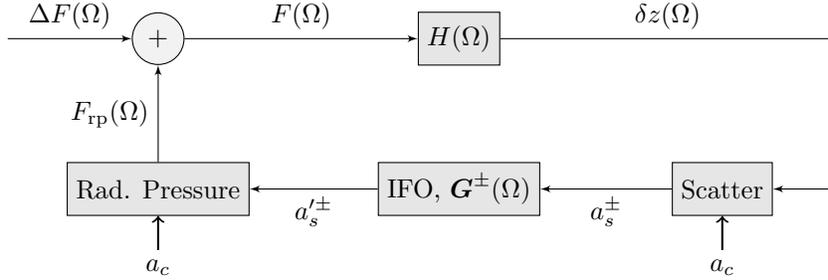


Figure 6.8: A generic view of a closed-loop opto-mechanical transfer function for a suspended mirror with mechanical susceptibility $H(\Omega)$. Due to some motion $\delta z(\Omega)$ of a mirror the light is scattered from the carrier. The IFO plant describes the optical transfer function of the sidebands propagating through the interferometer and back to the mirror in question. The interference of these then creates some radiation pressure force which is fed back into the mirror. Here a_c is the carrier field at the mirror in question.

Full steady state optical spring

To compute the full response of a suspended mirror we have to consider the propagation of the sidebands generated when the mirror moves, through the rest of the interferometer, and back to the mirror. This process of scattering and feedback is represented by the block diagram in figure 6.8. Here we have some force $F(\Omega)$ acting on a mirror with mechanical susceptibility $H(\Omega)$. The motion $\delta z(\Omega)$ combined with the incident carrier field a_c scatters light into the sidebands a_s^\pm . The IFO plant is the optical transfer functions from the port leaving the suspended mirror to the incoming port. Lastly these transformed sidebands, $a_s'^\pm = G^\pm(\Omega)a_s^\pm$, are combined again with the carrier field to compute the radiation pressure force $F_{rp}(\Omega)$ along with an external excitation $\Delta F(\Omega)$ to feedback into the mirror.

To illustrate this in more detail only a single carrier with a pair of sidebands describing a modulation at a frequency Ω will be considered. This optical field is incident on a perfectly reflective suspended. The incident and reflected optical fields are then:

$$a_s'^\pm = G^\pm(\Omega)a_s^\pm, \quad (6.47)$$

$$a_s^\pm = (a_s'^\pm + ikZ^\pm a_c). \quad (6.48)$$

Here the mirror displacement is $\delta z(\pm\Omega) \equiv Z^+ \equiv Z^{-*}$. Removing the circular dependence of the fields with 6.47 and 6.48

$$a_s'^\pm = \frac{ikG^\pm Z^\pm a_c}{1 - G^\pm}. \quad (6.49)$$

The radiation pressure force exerted on the mirror is

$$F_{\text{rp}}(\Omega) = \frac{4}{c} \left[a_s'^+ a_c^* + a_s'^-* a_c \right], \quad (6.50)$$

substituting in 6.49 the force is

$$F_{\text{rp}}(\Omega) = \frac{4i k P_c}{c} \left[\frac{G^+ - G^{-*}}{1 - rG^+ - rG^{-*} + RG^+G^{-*}} \right] z \equiv \kappa(\Omega)z. \quad (6.51)$$

This shows the radiation pressure force is linearly dependent on z for an arbitrary interferometer layout described with G^\pm . The complex valued scaling factor, $\kappa(\Omega)$, represents how the dynamics of the suspended mirror is altered. Those terms independent of Ω define the stiffness of the optical spring. Terms $\propto \Omega$ describe any damping, c_{opt} being the optical damping coefficient:

$$\kappa(\Omega) = k_{\text{opt}} + i\Omega c_{\text{opt}}(\Omega) + \mathcal{O}(\Omega^2). \quad (6.52)$$

Higher order terms can also exist here depending on the optical feedback that can alter the inertial behaviour too with terms $\propto \Omega^2$. Such manipulation of the opto-mechanical coupling here can be exploited to improve the sensitivity of gravitational wave detectors [108].

The above is applicable for a single optical field. In the case of multiple optical fields the sum of the multiple radiation pressure forces must be considered to compute the overall κ value. The result (6.51) is only applicable when fields are incident on a single side of a perfectly reflective mirror. As can be imagined this is particularly time consuming analytically for more detailed cases like a 50:50 suspended beamsplitter, multiple suspended optics, or multiple carrier frequencies with HOMs. Tools such as FINESSE take all these effects into account to ease studying such systems.

Optical spring in a cavity

Computing the optical spring constant for a suspended cavity is then just a case of determining the transfer functions G^\pm . The optical transfer function describes the propagation of the light reflected from the suspended end mirror, with reflectivity r_2 , to the field incident upon it. Thus a propagation along the cavity length L , reflection from the input mirror and finally another propagation is given by:

$$G^\pm(\Omega) = r_1 e^{-i2\frac{\Omega}{c}L} e^{i2\phi}. \quad (6.53)$$

Here ϕ is some detuning of the input mirror position. Substituting this into (6.51) we find:

$$\frac{G^+ - G^{-*}}{1 - r_2 G^+ - r_2 G^{-*} + R_2 G^+ G^{-*}} = \frac{i 2r_1 e^{-i2\frac{\Omega}{c}L} \sin(2\phi)}{1 + R_1 R_2 e^{-i4\frac{\Omega}{c}L} - 2r_2 r_1 e^{-i2\frac{\Omega}{c}L} \cos(2\phi)} \quad (6.54)$$

and:

$$\kappa(\Omega) = -\frac{8kP_c r_1 r_2 \sin(2\phi)}{c} \frac{e^{-i2\frac{\Omega}{c}L}}{1 + R_1 R_2 e^{-i4\frac{\Omega}{c}L} - 2r_2 r_1 e^{-i2\frac{\Omega}{c}L} \cos(2\phi)}. \quad (6.55)$$

When the cavity is on resonance, $\phi = 0$, we see no optical spring when there is no power. Likewise, in the DC limit $\Omega \rightarrow 0$, we find an agreement with (6.45). Shown in figure 6.9 is an example of a force-to-displacement transfer function for the suspended end mirror when a force is applied.

6.7 Finesse examples

6.7.1 Optical Spring

A simple example for an optical spring in a two mirror cavity with suspended mirrors. The cavity is slightly detuned which is required for creating the spring. The output is the motion of a mirror

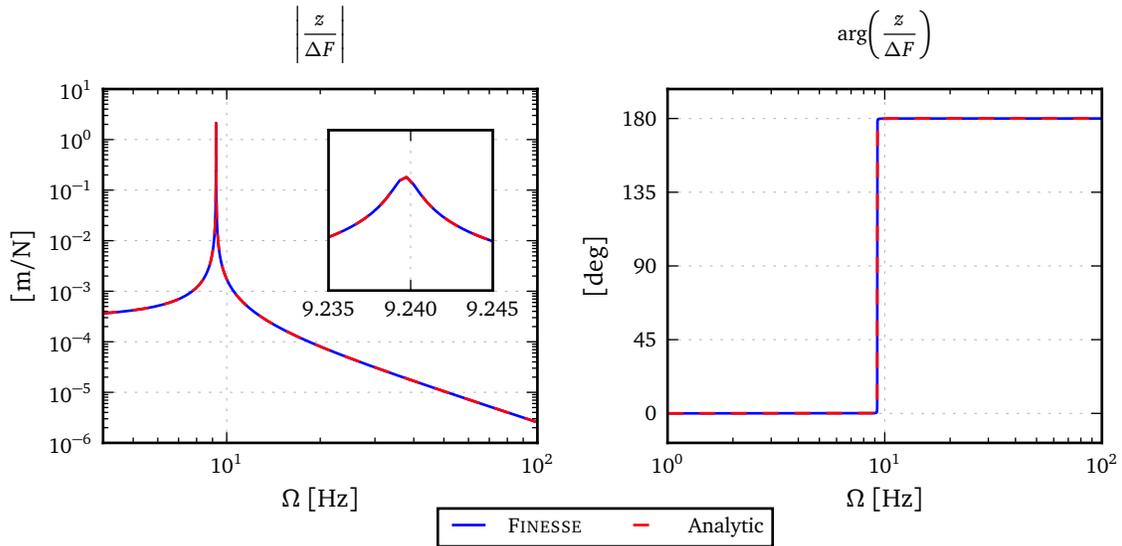


Figure 6.9: Analytic v.s. numeric (FINESSE) comparison of an optical spring. This is for a fixed input and suspended (free-mass) end mirror. A force is applied to the end mirror and shown is the force-to-displacement of the end mirror transfer function. Inset plot shows zoomed region around the peak which shows a good agreement with the peak shape and position.

while it is excited with a force of constant amplitude. The resonance feature shown in Figure 6.10 is the result of the opto-mechanical coupling of the mirror with the cavity field.

FINESSE input file for ‘optical spring’

```

l l1 1 0 n1
m ITM 0.99 0.01 0 n1 n2
s s1 1 n2 n3
m ETM 1 0 -0.048 n3 n4
% Set the mass of the ETM in kg
attr ETM mass 1
% Here we are applying a force to the end mirror
fsig aforce ETM Fz 1 0 1
% A detector for force-to-motion transfer function
xd ETMz ETM z
% scanning the frequency of the force
xaxis aforce f log 1 100 100000
yaxis log abs:deg

```

6.7.2 Homodyne detector and squeezed light

A laser and a squeezed light source are mixed with a beam splitter and then detected with a homodyne detector. The nominal quantum noise of an unsqueezed light field in the units of the blue trace are $2\hbar f$. The squeezing level of the squeezed light source is 10 dB, which means that the noise in one quadrature is 10 times lower than this whereas the other quadrature should be 10 times higher. With the phase of the local oscillator the homodyne detector can be tuned to measure the different quadratures. The green trace shows a computation of an effective squeezing

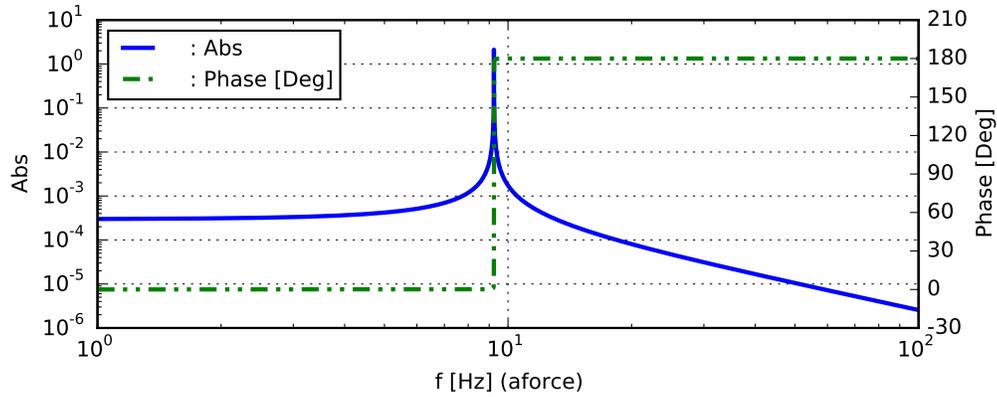


Figure 6.10: FINESSE example: Fabry-Perot cavity with an optical spring. The two traces show the amplitude and phase of the mechanical response of one cavity mirror to an exciting force. The resonance feature close to 10 Hz is the result of the opto-mechanical coupling of the mirror with the cavity field.

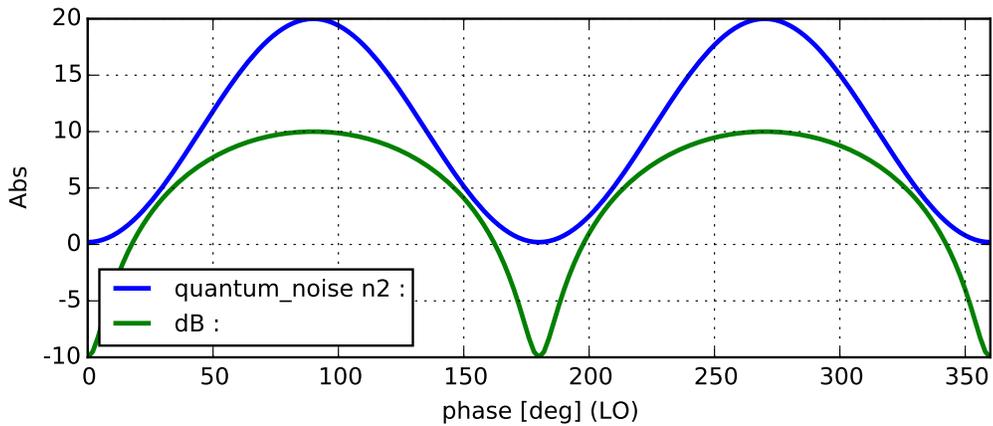


Figure 6.11: FINESSE example: Homodyne detector with a squeezed light input. The blue trace shows the quantum noise in units of $\hbar f$ with a range of 0.2 to 20, compared to a quantum noise of $2\hbar f$ for an unsqueezed source. The green trace instead has the units 'dB' and shows an effective squeezing level, inferred from the detected quantum noise.

level from the detected quantum noise using the Schottky equation.

Finesse input file for ‘homodyne detector and squeezed light’

```

l LO 1 0 n1
sq sqz 0 10 0 n4
bs bs1 0.5 0.5 0 0 n1 n2 n3 n4
% homodyne detector attached to the two bs outputs
qhd quantum_noise 180 n2 n3
% what noise frequency (Omega) do we plot
fsig noise 1
% Output noise in units of hbar*f
scale PSD_hf quantum_noise
% varying the LO phase
xaxis LO phase lin 0 360 180
% compute the squeezing level
set QN_re quantum_noise re
func dB = 10 * log10(($QN_re + 1E-20)/2)

```

6.7.3 Quantum-noise limited interferometer sensitivity

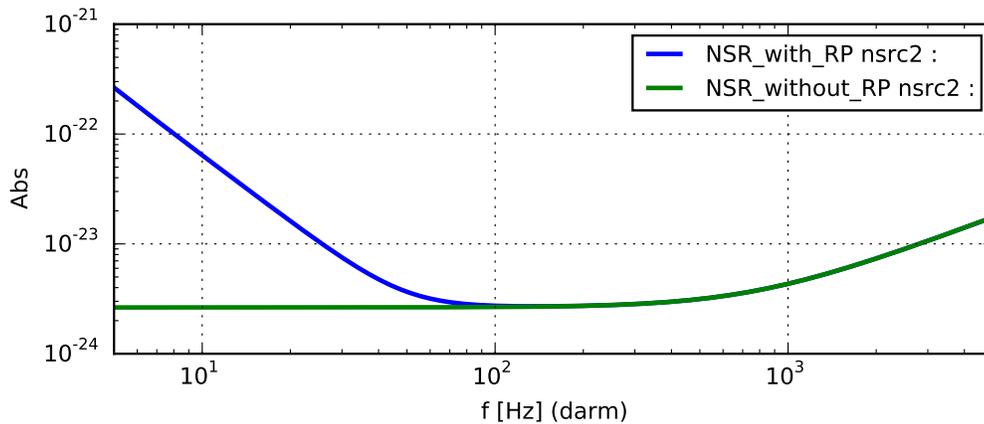


Figure 6.12: FINESSE example: Quantum limited sensitivity of a (simplified) Advanced LIGO interferometer. The interferometer setup is similar to a broadband RSE configuration of LIGO. The blue trace shows the full quantum-noise-limited sensitivity. For comparison the green trace shows the shot-noise-limited sensitivity.

This example shows the quantum-noise limited sensitivity of an Advanced LIGO detectors. See Appendix B for the optical layout of the detector and Section 8.10 for more details about the interferometer operation. The model is loosely based on the Advanced LIGO design file and thus we expect to see the peak sensitivity around 100 Hz at a sensitivity of about $10^{-23}/\sqrt{\text{Hz}}$. We can see the both the ‘qnoised’ and ‘qshot’ detectors agree at high frequencies, where the sensitivity is purely limited by shot noise. At low frequencies the two traces differ because only ‘qnoised’ takes into account the radiation pressure effects.

The FINESSE input file for this example is more complex than for other examples because it contains a more complex interferometer setup and uses relatively advanced concepts such as setting

mechanical transfer function. See Appendix A for more information on FINESSE and where to find the documentation, such as the syntax reference, required to follow this example.

Finesse input file for ‘quantum-limited interferometer sensitivity’

```

l l1 $Pin 0 nin
s s1 0 nin nprc1
# Power recycling mirror
m1 prm $prmT 37.5u 90 nprc1 nprc2
s prc $lprc nprc2 nbsin
# Central beamsplitter
bs bs1 .5 .5 0 45 nbsin n0y n0x nbsout
# X-arm
s ichx $lmichx n0x n1x
m1 itmx $itmT 37.5u 90 n1x n2x
s armx $Larm n2x n3x
m1 etmx 5u 37.5u 89.999875 n3x n4x
attr itmx mass $Mtm zmech sus1
attr etmx mass $Mtm zmech sus1
# Y-arm
s ichy $lmichy n0y n1y
m1 itmy $itmT 37.5u $michy_phi n1y n2y
s army $Larm n2y n3y
m1 etmy 5u 37.5u 0.000125 n3y n4y
attr itmy mass $Mtm zmech sus1
attr etmy mass $Mtm zmech sus1
# Signal recycling mirror
s src $lsrc nbsout nsrc1
m1 srm $srmT 37.5u $srm_phi nsrc1 nsrc2
# Force-to-position transfer function for longitudinal
# motions of test masses
tf sus1 1 0 p $mech_freq $mech_Q
const mech_freq 1
const mech_Q 1M # Guess for suspension Q factor
# offsets for DC readout: 100mW = michy_phi 0.07 OR darm_phi .00025
const michy_phi 0
const darm_phi .00025
const Larm 3995
const itmT 0.014
const srmT 0.2
const prmT 0.03
const Pin 125
const Mtm 40
const srm_phi -90
const lmichx 4.5
const lmichy 4.45
const lprc 53
const lsrc 50.525
# A squeezed source could be injected into the dark port
sq sq1 0 0 90 nsrc2
# Differentially modulate the arm lengths

```

```
fsig darm armx 1 0
fsig darm2 army 1 180
# Output the full quantum noise limited sensitivity
qnoisedS NSR_with_RP 1 $fs nsrc2
# Output just the shot noise limited sensitivity
qshotS NSR_without_RP 1 $fs nsrc2
# We could also display the quantum noise and the signal
# separately by uncommenting these two lines.
# qnoised noise $fs nsrc2
# pd1 signal 1 $fs nsrc2
xaxis darm f log 5 5k 1000
yaxis log abs
```

7 NEW: Advancing the interferometer layout

The first generation of interferometric gravitational wave detectors was limited in the upper-frequency band by shot noise, one manifestation of the quantum noise of the laser light, see Section 6. To improve the ratio between gravitational-wave signal and shot noise we must increase the light energy stored in the interferometer arms. This can be achieved in several ways, for example, by increasing the arms' length or by increasing the injected laser power. The lengths of the arms is typically limited by the associated costs of the building the infrastructure. High-power lasers are used; however do not come near the power levels required for the anticipated sensitivity. For example, the design sensitivity of Advanced LIGO requires a light power of several hundred kilowatts in the interferometer arms. The Advanced LIGO laser can provide up to 200 W of power, and represents a state of the art system (for a CW laser with the required stability in frequency, amplitude and beam profile) [102].

In order to increase the laser power inside the arms further we can utilise the concept of resonant light enhancement in the Fabry-Perot cavity: so-called advanced interferometer topologies are created by introducing optical cavities to the Michelson interferometer. In the following we will briefly introduce the most common concepts, which are used by modern gravitational wave detectors today.

We have shown in Section 5.2 how the dark fringe operating point allows to maximise the throughput of differential signals (with respect to common mode noise), using the sideband picture. Similarly we can compute the transfer functions of the signal sidebands to illustrate the concepts behind the advanced interferometer layout. The motivation for all the advanced concepts shown below is the improvement of the ratio between signal and shot noise. However, we will ignore here the detailed computation of the shot noise and quantum noise discussed in Section 6. Instead we will compute only the transfer functions of the signal to the photo detector using the sideband picture. We will ignore radiation pressure noise and shot-noise contributions from any light field but the local oscillator. Thus the amplitude of the signal sidebands in the detection port give a good figure of merit for the shot-noise limited sensitivity of the detector.

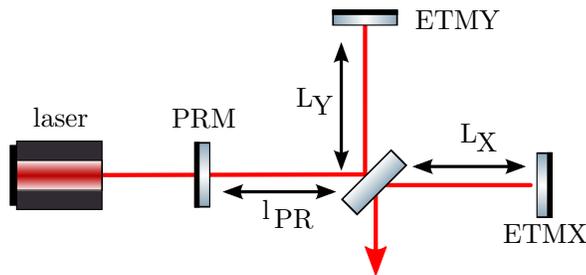


Figure 7.1: Optical layout of a Michelson interferometer with arm power recycling.

7.1 Michelson interferometers with power recycling

The Michelson interferometer, when held on the dark fringe and ignoring internal losses, reflects all the incoming light back into the laser port; seen from the laser it acts like a highly reflective mirror. It was soon realised we can utilise this fact to increase the light power inside the interferometer: an additional mirror inter the input port, the so-called power-recycling mirror (PRM), will generate an optical cavity with the Michelson interferometer acting as a second 'mirror'. This scheme which is now called *power recycling* was first proposed in 1983 independently by Schilling [25] and Drever [60]. The newly formed cavity is often called *power-recycling cavity*. The optical layout of a

power-recycled Michelson interferometer is shown in Figure 7.1. Figure 7.2 shows the amplitude of signal sidebands for different levels of power recycling, as a function of the frequency of the signal. We will compare this to similar plots for other techniques described below.

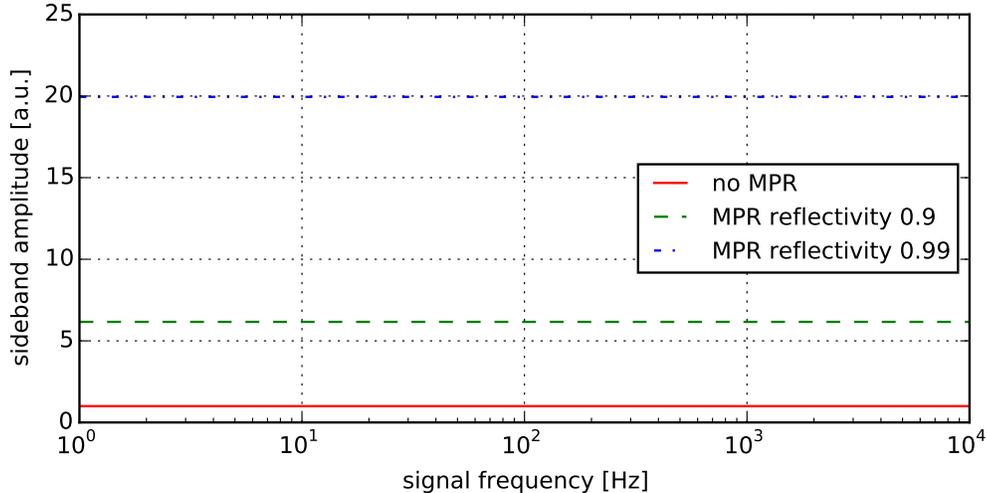


Figure 7.2: This graph shows the signal sideband amplitude for a differential arm length change, as detected in the anti-symmetric output port, as a function of the frequency of the signal. The solid red trace at an amplitude of 1 refers to the case without power recycling. The other two traces show the increased amplitude for different reflectivity's of the power-recoiling mirror. Compare this plot also with Figures 7.4 and 7.6 below.

As we have discussed in Section 5.1, the power circulating inside a cavity can be much higher than the injected light power. The power enhancement is given by the finesse of the cavity which is given by the optical losses in the interferometer and the reflectivity of the power-recycling mirror. When the losses inside the Michelson interferometer are negligible the cavity formed by the Michelson and the power-recycling mirror is over-coupled and the power enhancement in the interferometer arms, also called *power-recycling gain* computes as

$$G_{\text{PR}} = \frac{4}{T_{\text{PRM}}} \approx \frac{2\mathcal{F}}{\pi} \quad (7.1)$$

with \mathcal{F} the finesse of the power-recycling cavity.

When the optical losses can not be ignored the maximum power-recycling gain can be reached by impedance matching, i.e. setting the transmission of the power-recycling mirror equal to the round trip losses of the power-recycling cavity and the gain becomes

$$G_{\text{PR}} = \frac{1}{T_{\text{PRM}}} \approx \frac{\mathcal{F}}{\pi} \quad (7.2)$$

The power in the signal sidebands proportional to the carrier power and thus scales with the power-recycling gain as well. The amplitudes plotted in Figure 7.2 thus show values of $\sqrt{4/0.1} \approx 6.32$ and $\sqrt{4/0.01} = 20$.

Power-recycling has further advantages: the cavity effect can be used to reduce beam jitter and to filter laser frequency noise. The disadvantage is that another mirror position needs to be carefully maintained by a feedback control system. In addition, the increase in circulating power

also increases the laser power with the substrate of the beam splitter which can cause thermal distortions which lead to higher-optical losses. In practise this often limits the achievable power-recycling gain.

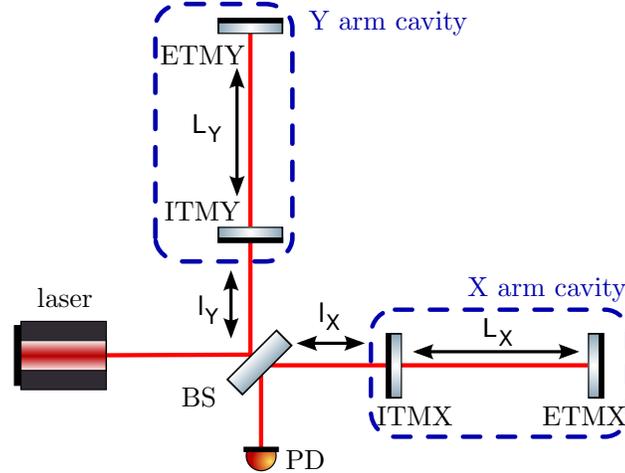


Figure 7.3: Optical layout of a Michelson interferometer with arm cavities.

7.2 Michelson interferometers with arm cavities

Another way to employ cavities to enhance the light power circulating in the interferometer arms is to place optical cavities into these arms, as so-called *arm cavities*, as shown in Figure 7.3. This optical configuration sometimes referred to as *Fabry-Perot Michelson interferometer*. Similar to power-recycling the finesse of the cavity determines the enhancement of the light.

The arm cavities have another effect on the detector sensitivity: they affect not only the power of the circulating carrier field, but also that sidebands generated by a length change. This results in a further increase of the sensitivity for signals with a frequency within the linewidth of the arm cavities but to a decrease in sensitivity regarding signals with frequencies that fall outside the linewidth of the cavities. This can be shown again very clearly with the sideband amplitudes detected at the interferometer output as shown in Figure 7.4. We can compare this results to the power-recycling case (Figure 7.2): when the reflectivity of the PRM and ITMs is set to $R = 0.99$, the expected gain for the carrier field inside the cavities must be the same and equal to 400, assuming an over-coupled case. At low frequencies the signal sidebands will experience the same enhancement, namely by a factor of 400 in power. Thus the total enhancement for the signal sidebands in the Michelson with arm cavities is 16000, which gives the amplitude of 400 shown for sideband amplitude in Figure 7.4. Therefore the arm cavities also change the detector response function in a way that limits the possible sensitivity increase.

The limited bandwidth of the arm cavities is a disadvantage when compared to the power-recycling technique; however, the arm cavities have the significant advantage of not increasing the light power in the beam splitter substrate. In practise the two techniques are commonly used together, with the finesse of the arm cavities and the reflectivity of the power-recycling mirror the result of a trade-off analysis between the bandwidth reduction of the arm cavities and the light power increase in the beam splitter substrate. Such an optical layout is also called *power-recycled Fabry-Perot Michelson interferometer*.

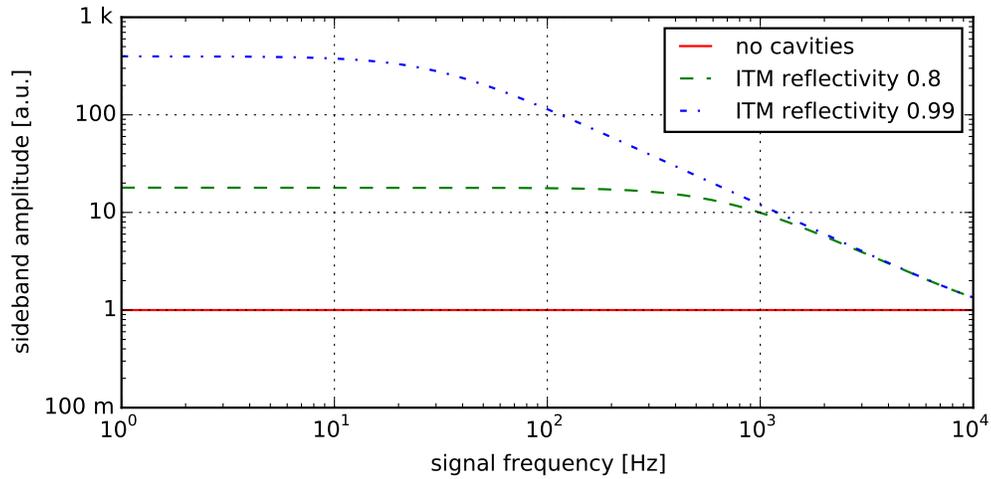


Figure 7.4: This graph shows the signal sideband amplitude for a Fabry-Perot Michelson interferometer. The signal is a differential arm length change detected in the anti-symmetric output port, as a function of the frequency of the signal. The solid red trace at an amplitude of 1 refers to the case without arm cavities. The other two traces show the increased amplitude for different reflectivities of the cavities' input mirrors. Compare this also with Figures 7.2 and 7.6.

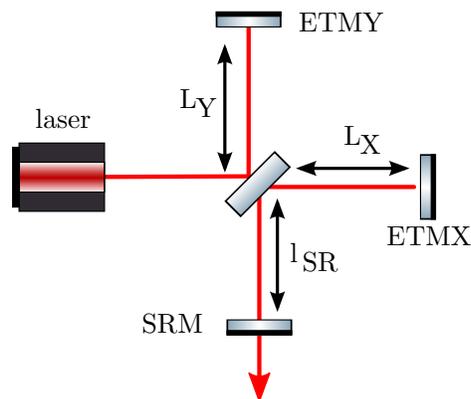


Figure 7.5: Optical layout of a Michelson interferometer with signal recycling.

7.3 Signal recycling, dual recycling and resonant sideband extraction

Soon after the development of power recycling in which an additional mirror is used to ‘recycle’ the laser light leaving the Michelson interferometer through the symmetric port, Brian Meers recognised that it would be of interest to employ a similar technique employed in the anti-symmetric port. In the ideal Michelson interferometer on the dark fringe, the carrier light and the signal sidebands become separated at the central beam splitter and leave the interferometer through different ports. Meers suggested [115] to add a *signal-recycling mirror* into the anti-symmetric port, which would form a signal-recycling cavity with the Michelson interferometer. Similar to the power-recycling cavity the signal-recycling cavity could resonantly enhance the light circulating within, i.e. the signal sidebands. The optical layout of a signal-recycled Michelson interferometer is shown in Figure 7.5.

It is somewhat counterintuitive that placing a highly-reflective mirror in front of the photo detector would increase the power detected on same photo detector. This is because the signal sidebands are created within the interferometer, and thus within the signal recycling cavity, by a parametric effect, in which light is transferred from much larger reservoir, the carrier field. Gerhard Heinzel’s provides in Appendix D of his thesis [87] a clear and compact mathematical overview of a two-mirror cavity including this effect.

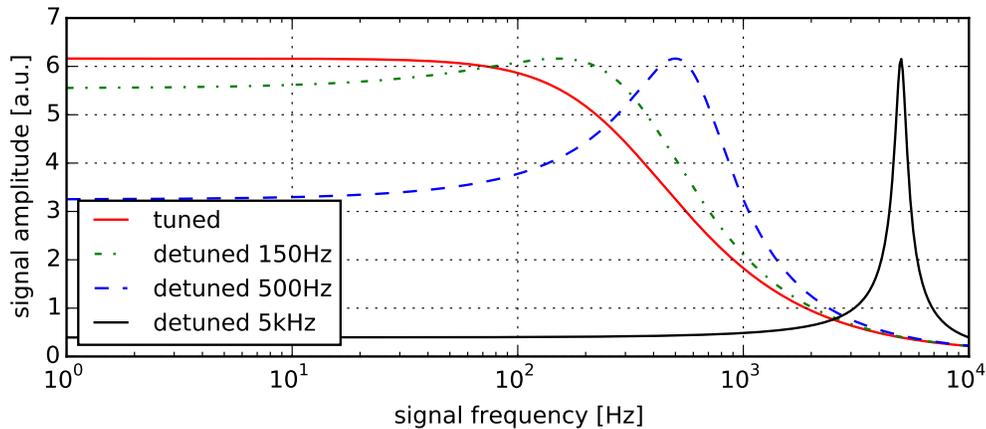


Figure 7.6: This graph shows the signal sideband amplitude for a Michelson interferometer with different signal-recycling configurations. For all 4 traces the reflectivity of the signal-recycling mirror was set to $R = 0.9$. The red trace shows the *tuned* case in which the signal-recycling cavity is resonant for the carrier light and thus maximises signals around DC. The other red traces show different detunings, microscopic offsets to the longitudinal positions of the signal-recalling mirror. The maximum amplitude and bandwidth of the trace is the same in all four cases, just the frequency of the peak sensitivity is shifted by the detuning. Compare this the plots for arm cavities in Figures 7.4 and power recycling, Figure 7.2.

When both recycling techniques are used together, power recycling for enhancing the carrier power and signal recycling for increasing the signal interaction time, the combination of the two methods is called *dual recycling*. It was actually the concept of dual recycling which Meers proposed in 1988 [115], and this was demonstrated first as a table-top experiment by the Glasgow group in 1991 [152].

The combination of arm cavities and a signal-recycling mirror is sometimes also called *resonant sideband extraction* [123]. The difference between signal-recycling and resonant sideband extraction is that in the latter case the arm cavities have a very high finesse and the signal-recycling mirror

is tuned to or near the anti-resonant operating point, thus effectively increasing the bandwidth of the detector for the signal sidebands. An analysis of the different techniques can be found in the thesis of Jun Mizuno [121]. It is interesting to note that for all variants of the signal recycling the total integrated gain remains constant. For example, the areas under curves for the different detunings shown in Figure 7.6 are constant⁹. This means that signal-recycling is used to *shape* the response function of the detector with respect to the signal-to-shot-noise ratio.

The main interferometer of an Advanced LIGO detector is based on a Michelson interferometer with arm cavities plus power and signal recycling. This configuration is most commonly called *dual-recycled Fabry-Perot Michelson interferometer* even though the signal recycling mirror is here used in the resonant sideband extraction mode, see Figure B.3 for a schematic of this layout.

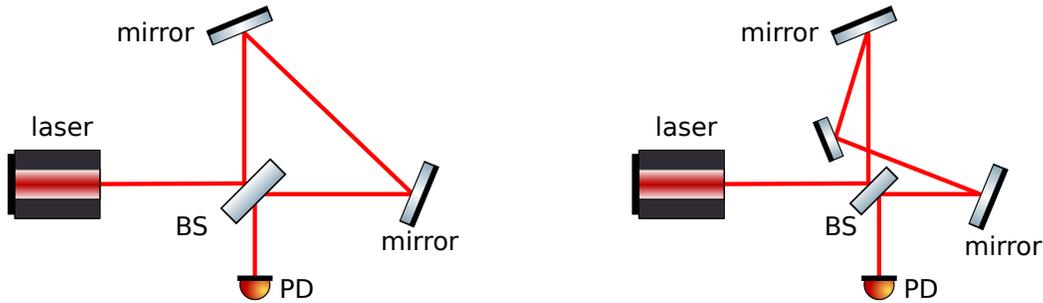


Figure 7.7: The left sketch shows a typical layout of the original Sagnac interferometer: similar to the Michelson interferometer the injected light is split and recombined at a central beam splitter. However, unlike the Michelson the Sagnac has not two different interferometer arms, but the two split beams travel along the same path, in different direction. This makes the Sagnac interferometer insensitive to the actual path length, instead is sensitivity to rotation of the whole interferometer. The sketch on the right shows a so-called *zero-area* Sagnac interferometer: an additional mirror is used so that the beam path is folded reducing the effective circulated area (see text).

7.4 Sagnac interferometer

Another interferometer type which has a similar-looking optical layout to the Michelson interferometer is the *Sagnac* interferometer, see Figure 7.7. Originally proposed by Sagnac for measuring rotation [140, 141] it became of interested to the gravitational-wave community as a possible alternative to the Michelson interferometer: in 1995 successful experimental tests of a zero-area Sagnac demonstrated a different mode of operation, in which it becomes insensitive to rotation but sensitive to mirror motion [154]. Further investigations into the performance and technical limitations of a Sagnac interferometric gravitational wave detector have been undertaken [122, 132, 131] and the community interest was renewed after understanding that the Sagnac topology can be used as a speed-meter with the potential to suppress radiation pressure noise in future detectors [50, 54, 165, 164, 56].

7.5 Finesse examples

7.5.1 Michelson interferometer with arm cavities

This example shows how to setup a Michelson interferometer, tune it to the dark fringe and compute a transfer function from the differential length change to the output signal, using the

⁹The tuned case is slightly special, because the integrated area is half compared to the others, because the plot shows only the positive half of the total linewidth seen by signal sidebands.

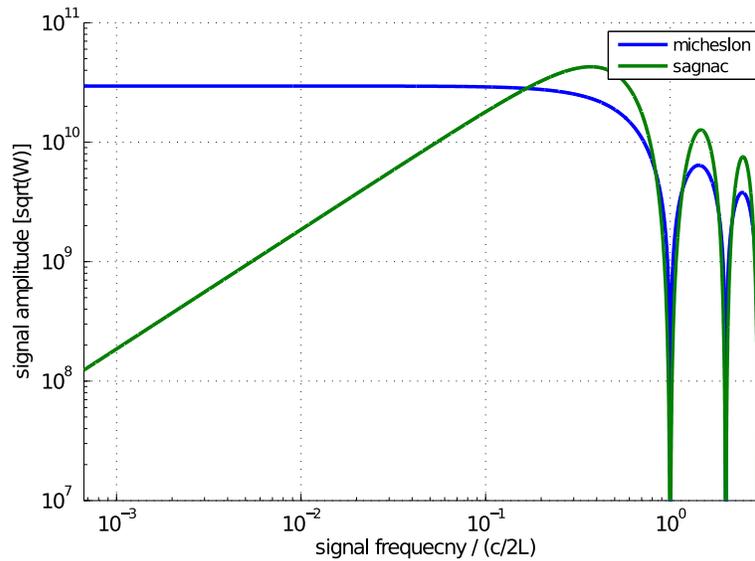


Figure 7.8: Transfer function of a Michelson and Sagnac interferometer for a gravitational-wave signal to the main output channel. It can be seen that the Sagnac response falls off for lower frequencies and reached twice the peak response; however at relatively large frequency, in the case of Advanced LIGO the peak would be at $f=c/2L \approx 37.5$ kHz, i.e. above the measurement window.

sideband amplitude for simplicity.

Finesse input file for ‘Michelson interferometer with arm cavities’

```

laser l1 1 0 n1      % laser with P=1W at the default frequency
space si1 1 n1 n2    % space of 1m length
mirror MPR 0 1 0 n2 n3
space si2 50 n3 n4

bs b1 0.5 0.5 0 0 n4 nY1 nX1 n01 % 50:50 beam splitter
space s1Y 7 nY1 nY2
space s1X 7 nX1 nX2
mirror ITMY 0.99 0.01 0 nY2 nY3 % Y input mirror, lossless
mirror ITMX 0.99 0.01 90 nX2 nX3 % X input mirror, lossless
space LY 4k nY3 nY4    % Y arm
space LX 4k nX3 nX4    % X arm
mirror ETMY 1 0 0 nY4 dump % Y end mirror, lossless
mirror ETMX 1 0 90 nX4 dump % X end mirror, lossless, tuned for dark fringe
space sol 1 n01 nout

fsig sig1 ETMX 100 0
fsig sig2 ETMY 100 180
ad signal 100 nout

xaxis sig1 f log 1 10k 300

```

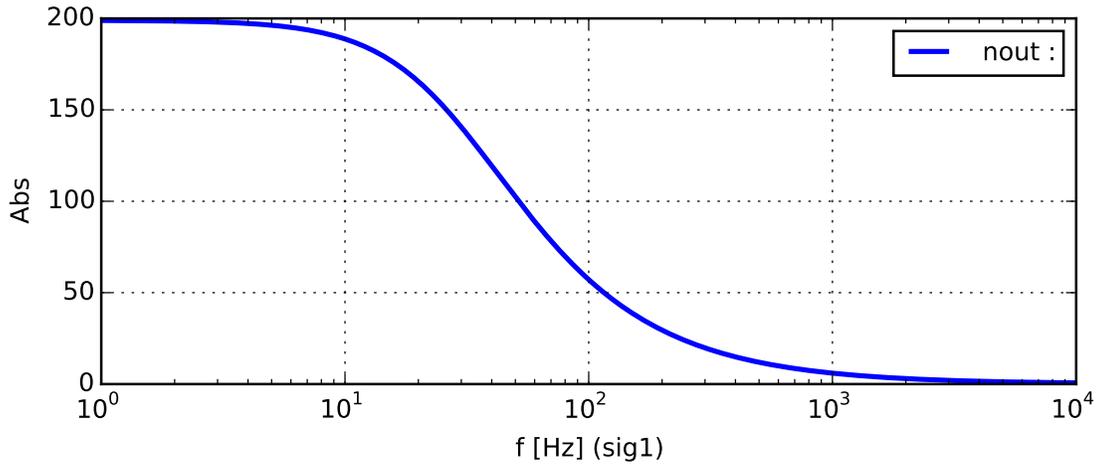


Figure 7.9: FINESSE example: Michelson interferometer with arm cavities. The trace shows the signal sideband amplitude in the anti-symmetric port as a function of signal frequency.

```
put signal f $x1
```

7.5.2 Michelson interferometer with signal recycling

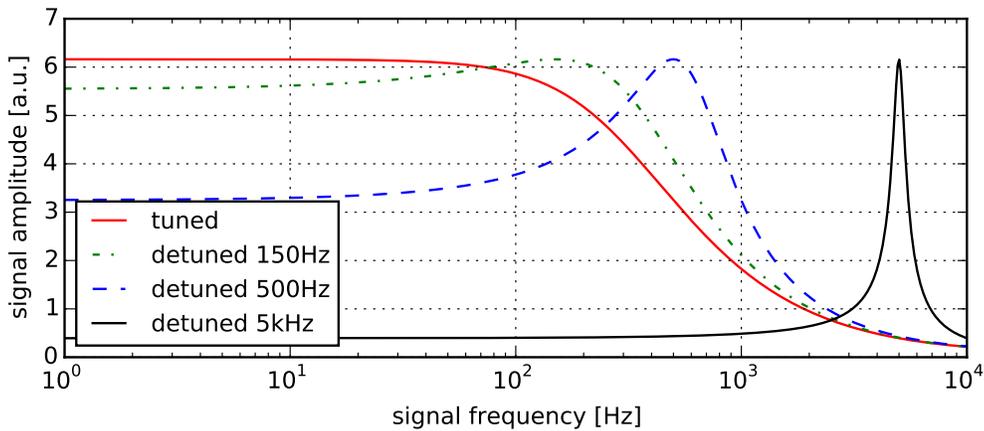


Figure 7.10: FINESSE example: This graph shows the signal sideband amplitude for a Michelson interferometer with different signal-recycling configurations, see Figure 7.6.

This example recreates the plot shown in Figure 7.6, the four traces show the transfer function for a Michelson interferometer with different signal recycling tunings.

Finesses input file for ‘Michelson with signal recycling’

```
laser l1 1 0 n1 % laser with P=1W at the default frequency
space si1 1 n1 n2 % space of 1m length
mirror MPR 0 1 0 n2 n3
```

```

space si2 50 n3 n4

bs b1 0.5 0.5 0 0 n4 nY1 nX1 n01 % 50:50 beam splitter
space sLY 7 nY1 nY2
space sLX 7 nX1 nX2
mirror ITMY 0 1 0 nY2 nY3 % Y input mirror, lossless
mirror ITMX 0 1 90 nX2 nX3 % X input mirror, lossless
space LY 4k nY3 nY4 % Y arm
space LX 4k nX3 nX4 % X arm
mirror ETMY 1 0 0 nY4 dump % Y end mirror, lossless
mirror ETMX 1 0 90 nX4 dump % X end mirror, lossless, tuned for dark fringe
space so1 50 n01 n02
% change the signal recycling mirror for th 4 traces
mirror MSR 0.9 0.1 0 n02 n03 % tuned
%mirror MSR 0.9 0.1 0.73026 n02 n03 % detuned to 150 Hz
%mirror MSR 0.9 0.1 2.4342 n02 n03 % detuned to 500 Hz
%mirror MSR 0.9 0.1 24.342 n02 n03 % detuned to 5 kHz
space so2 1 n03 nout

fsig sig1 ETMX 100 0
fsig sig2 ETMY 100 180
ad signal 100 nout

xaxis sig1 f log 1 10k 600
put signal f $x1

```

7.5.3 Sagnac interferometer

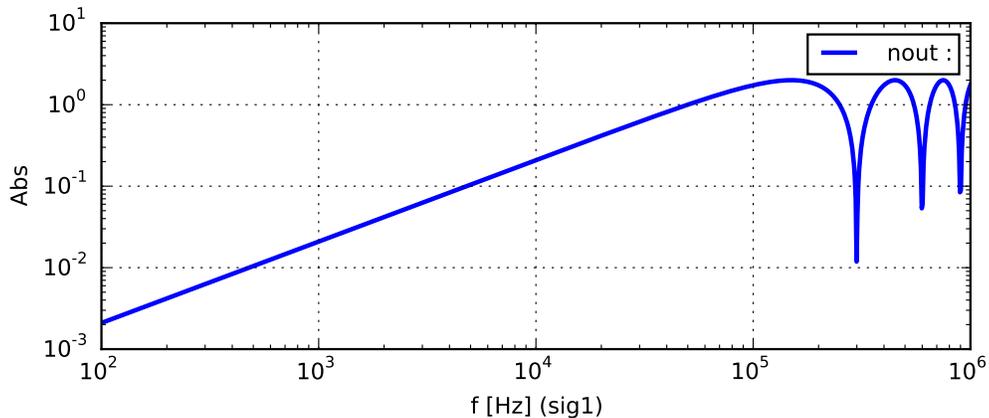


Figure 7.11: FINESSE example: Frequency response of a Sagnac interferometer: transfer function from differential mirror position change to signal sideband amplitude in the main output port.

This example demonstrates how compute the frequency response of a simple Sagnac interferometer.

Finesse input file for Sagnac interferometer

```
laser l1 1 0 n1
space s1 1 n1 n2
bs b1 0.5 0.5 0 0 n2 nN1 nE1 nS1 % 50:50 beam splitter
space LN 1k nN1 nN2 % north arm
space LE 1k nE1 nE2 % east arm
bs mN 1 0 0 0 nN2 nN3 dump dump % north end mirror
space link 1k nN3 nE3 % third arm
bs mE 1 0 0 0 nE2 nE3 dump dump % east end mirror
space s2 1 nS1 nout

fsig sig1 mE 100 0
fsig sig2 mN 100 180
ad signal 100 nout

xaxis sig1 f log 100 1M 1000
put signal f $x1
yaxis log abs
```

8 Interferometric Length Sensing and Control

In this section we introduce interferometers as length sensing devices. In particular, we explain how the Fabry-Perot interferometer and the Michelson interferometer can be used for high-precision measurements and that both require a careful control of the base length (which is to be measured) in order to yield their large sensitivity. In addition, we briefly introduce the general concepts of *error signals*, *transfer functions* and relevant elements of *control theory*, which are used to describe most essential features of length sensing and control.

In addition to sensing and controlling the distances between the components of an interferometer, alignment sensing and control is required for correct operation. While we do not deal with this aspect in detail, all of the ideas we develop for length sensing and control can be applied. The essential differences are that split photo-detectors are required to sense the relative angles of optical wavefronts, and control is by means of actuators that are able to adjust the angles of optical components. For an introduction to the essential ideas see Section 9.2 for an introduction to the relevant theory and [125], for details of a practical implementation.

8.1 NEW: An overview of the control problem

A complete interferometer can have a large number of control loops for the various mirrors and beam-splitters, their suspension systems and many other components, such as the laser, active vibration-isolation systems etc. For practical purposes these are usually divided into two broad classes that are often considered separately in the design process. These divisions reflect a degree of independence of the various categories of control and simplify the design process by allowing the problem to be split into a number of more easily tractable design elements.

The set of control loops that obtain signals from the detection of interference conditions or other properties of the light within the interferometer, and act on the major optical components of the interferometer to control those properties, is usually called *global control*. As an example, a description of the global control system of Virgo can be found in [16]. On the other hand, loops that sense properties associated with a single component, and act on that component are called *local* loops. A good example of local control is the system employed to damp the rigid-body modes of a mirror suspension, for an example from Advanced LIGO see [18]. By ‘cooling’ or quieting the motion of individual mirrors, the task faced by the global control system can be simplified. Further division of global interferometer control is frequently made between systems that control longitudinal degrees of freedom, i.e. relative positions of the mirrors and beam-splitters along the direction of propagation of the light, and angular (alignment) control systems that are designed to stabilise the pointing of components.

Due to the presence of strong nonlinearity throughout much of the phase-space volume, there has been no attempt thus far to solve the multi-dimensional control problem as a whole. At least up to the present, the problem has been divided into several smaller parts, with methods developed to deal with the particular details of each facet of the system, and each stage of operation from completely uncontrolled to held at the operating point – a condition that is called ‘locked’.

This leads to yet another division: it is normal to separate the start-up phase i.e. the process called *acquisition of lock* from the stable running condition (‘in lock’). This split is motivated, at least in part, by the consideration that signal sizes can differ greatly between the two stages. During acquisition electronic signals tend to be large – corresponding to adjusting mirror positions by of order wavelengths, or more. By contrast, in operation the signals representing residual motion in the sensitive frequency band may exceed about 12 orders of magnitude smaller than the wavelength of the light, to deliver the required measurement sensitivity¹⁰.

¹⁰The typical light wavelength is $\sim 10^{-6}$ m while all ground-based interferometers built or planned have target displacement noise spectral densities below $\sim 10^{-19}$ m/ $\sqrt{\text{Hz}}$ in a frequency band of order 100 Hz wide.

The jump in signal size between these two states is often dealt with by switching gain levels or even substituting large parts of the control system: starting with large-range but noisy methods for acquisition and switching to low-noise, but small-range controls for operation. A good example of a more substantial transition is the *arm length stabilization* (ALS) scheme in Advanced LIGO, which employs additional lasers, mirror coatings and interferometric methods to provide wavelength-range sensing during the acquisition phase [104]. When the long cavities (see Appendix B) are locked, the control systems are switched over to the high-sensitivity, low-noise signals derived from the main interferometer systems.

During acquisition of lock, the instantaneous operating point frequently lies in a non-linear region of the control space. Several methods have been developed to cope with this problem.

The simplest approach, employed in the early interferometer prototypes, was to wait for a random co-incidence of suitable values to occur then to catch the system quickly enough to hold it in the desired state. As the complexity of the interferometer topologies increased, and with that the number of degrees of freedom, the probability of the desired state occurring in a conveniently short time became rare. This led to the development of more sophisticated techniques for the first long-baseline interferometers.

As a first step it was realised that digital logic (implemented directly in electronics or as software) could be employed to identify when one or more degrees of freedom happened to fall close to the desired operating point, and to activate the relevant control loop. This prevents false signals, frequently present in regions of phase space close to the desired operating point, being fed back to the actuators and perturbing the system. In Pound-Drever-Hall locking, for example, when the phase modulation sidebands pass through resonance in the cavity, the error signal has the opposite sign from that produced by a carrier resonance. The acquisition process can be improved by enabling the control system only when the circulating power within the cavity has exceeded the maximum possible power that a sideband can produce. By this means the control system is only activated close to the desired operating point, improving the chances of a successful lock.

A second way to improve matters is to linearise the behaviour, and so to increase the capture range: i.e. the volume of phase space within which the various control signals are valid. This improvement can be accomplished by normalising the relevant error signal according to some estimate of its slope, as measured by another signal such as the circulating optical power. As an example, the linear range in the Pound-Drever-Hall signal for locking a cavity may be extended by normalising with respect to the power within the cavity, as measured by probing the light transmitted by the cavity.

Another approach, that has behaviour or by first locking in a region of phase space that is relatively smooth, compared to the region in phase space surrounding the final operating point. This was an enabling technique for GEO 600 when it was first operated in dual-recycled mode. It was found that by locking with signal recycling detuned by a few kHz, an initial lock was possible. The tuning was then stepped towards the target value, in steps chosen to be small enough to avoid perturbing the lock. By this means it was possible to reach a location in phase space which would essentially never have occurred by chance [83].

After lock has been achieved by one or more of the above means, the control task is generally managed by linear control systems that may be analysed using standard *linear time invariant* (LTI) control theory. Two generic approaches have been employed with success. In one approach there is a set of separate single-input single output (SISO) controllers, one for each degree of freedom. The alternative is to deal with several degrees of freedom in a single multi-input multi-output (MIMO) controller. Recently, since the advent of computer-based, digital control systems, the MIMO approach has become much more practical than it would be if implemented in analogue electronics. An important difference between the SISO and MIMO approaches concerns how cross-coupling between the degrees of freedoms can be dealt with.

Cross-coupling is commonly seen in both sensing and actuation, and considerable effort is

needed to develop control systems that operate correctly in the presence of undesired mixing of signals. The main approaches to solving these problems with MIMO controllers is described in Section 8.11. Otherwise we discuss SISO controllers to provide illustrative examples of control in idealised interferometers where there is no mixing of degrees of freedom at the point of sensing or actuation.

We introduce standard terminology from control theory. In each control loop a point of reference is taken, called the *error point* at which we measure how the gain of the loop acts to suppress deviations from the desired operating point. Since a loop has no end, the selection of this point is somewhat arbitrary, but it is usually convenient to take the output from a photo-detector or its associated demodulator.

Likewise, we choose an actuation or *feedback point* at the interface between the control electronics and the interferometer – again the precise division is somewhat arbitrary, but the electronic signal input to an actuator is frequently employed as the point of reference.

With these points defined, the part of the loop from error-point to feedback-point is called the *controller* or just the feedback, and the rest of the loop from feedback point to the error point (in the causal direction) is called the *plant*.

Before a loop is activated, the signal that would be measured at the error point is called the *error signal*. In interferometry this is usually derived as an output from the optical system and its photo-detectors, as explained in Section 8.5.

8.2 NEW: Linear time-invariant control theory – introductory concepts

A full description of linear time-invariant (LTI) theory is beyond the scope of this article, therefore we restrict our description to a short summary of the essential concepts, with some relevant examples presented in the following sections.

In LTI models the superposition principle applies, frequencies do not mix and it is possible to represent any physical time-domain signals in the frequency domain through their Fourier transforms. The time-invariance means that the response of a system to an input does not depend on the time at which that input is applied. This implies that the differential equations describing the system are linear and homogeneous with coefficients that are constant in time. In this case it is common to solve these equations by employing methods based on the Laplace transform. The response of the system is represented by its *transfer function* which is the Laplace transform of its *impulse response* – i.e. the output produced in the time domain when the input is a Dirac-delta function. We look at transfer functions in more detail in Section 8.5.

For LTI systems the eigenfunctions or basis functions of the solution are the complex exponentials. Consider an input of the form

$$S_I = Ae^{st}, \quad (8.1)$$

where A is a complex factor, s the Laplace transform variable and t is time, to a particular system. If the output is

$$S_O = Be^{st}, \quad (8.2)$$

with different complex factor B , the system is described in full by the transfer function

$$T = \frac{S_O}{S_I} = \frac{Be^{st}}{Ae^{st}} = \frac{B}{A}, \quad (8.3)$$

which is not a function of time.

By implication, if the input to the system is a sinusoid (a single Fourier component) the output is also a sinusoid with, generally, different amplitude and phase as described by the transfer function. If the system consists of a series of optical, electronic and mechanical stages or sub-systems, the overall transfer function is the product of the individual transfer functions. If there is feedback,

then *loop-algebra* can be applied, and this represents summation of the signal from one point in a loop into an earlier point (feedback), or in the case of feed-forward to a later point. This is also a linear operation, and so the system with feedback or feed-forward retains its LTI property. The most complicated case that need be considered is when there are two or more nested feedback loops (or equivalently two or more actuators that adjust one degree of freedom [143]), in this case there are loop-algebraic techniques that allow the system to be reduced to a single equivalent loop, such that nested loops of any practical topology may be considered step by step.

In modelling LTI systems it is common to pick a *representation* from one of a mathematically-equivalent set of options. The alternatives are described in, e.g. [68]. To give some examples, individual loops or blocks with one input and one output (called SISO - single input, single output systems), are commonly represented by their transfer functions.

For LTI systems, the transfer functions can be written as rational polynomials in the complex frequency variable s . The polynomials on both the numerator and denominator of the transfer function can be factorised. This leads to an equivalent mathematical representation of the transfer function as a list of zeros (zeros of the numerator) and poles (zeros of the denominator). In addition an overall gain factor, independent of frequency, is usually required. The poles and zeros may be represented by their coordinates in the complex (s)-plane, or more phenomenologically by their resonant frequencies and damping factors. This leads to the so-called (z, p, k) -notation, where z represents one or more zeros, p the poles, and k represents the gain factor.

For MIMO systems arrays of transfer functions can be employed to describe all possible input-output relations, but it is more common to use the *state-space* representation. Here a single set of matrices encapsulates the behaviour of the entire system. A description of this important method is beyond the scope, but full detail is given in [68].

In briefest summary, the state-space method involves writing the set of N second order differential equations representing the internal dynamics of a system which has N degrees of freedom. These are reduced to $2N$ first-order equations by introducing the time derivatives, i.e. generalised velocities, of the displacement-like coordinates. The solution of the resulting set of equations is then usually carried out numerically, using matrix methods.

8.3 NEW: Digital signal processing for control

In the past two decades digital control systems have been introduced into the control of interferometers, in modern instruments the majority of control systems contain digital processing elements, although the interfaces with the interferometer remain analogue in almost all cases. The essential principles remain the same as in the continuous-time systems, and a common approach to the design of digital control systems starts by designing and simulating a continuous-time analogue model. When this model operates as required in simulation, the result is transformed to the discrete-time mathematics of digital control. The resulting filters are then implemented in software and hardware. In discrete-time models only a finite set of frequencies exist, limited at high frequencies by the Nyquist frequency, i.e. half of the sampling rate in the digital system.

Digital models also have finite amplitude resolution, with the practical resolution limits occurring at the analogue-digital and digital-analogue interfaces (ADC, DAC respectively), rather than in the digital signal processing. These limitations are generally handled by *whitening* the signal at the input and *de-whitening* at the output. For example, input signals with predominant low-frequency content may be high-pass filtered to render their spectral content relatively uniform, i.e. white, before sampling to make best use of the available resolution. The converse process can be applied at the output, with sufficient low-pass filtering applied to ensure that white noise resulting from the output conversion (DAC) is suppressed within the gravitational wave band.

In the description of digital controllers, the discrete mathematics of the z -plane replaces the continuous nature of the s -plane [68]. Transforming from one space to the other is something of

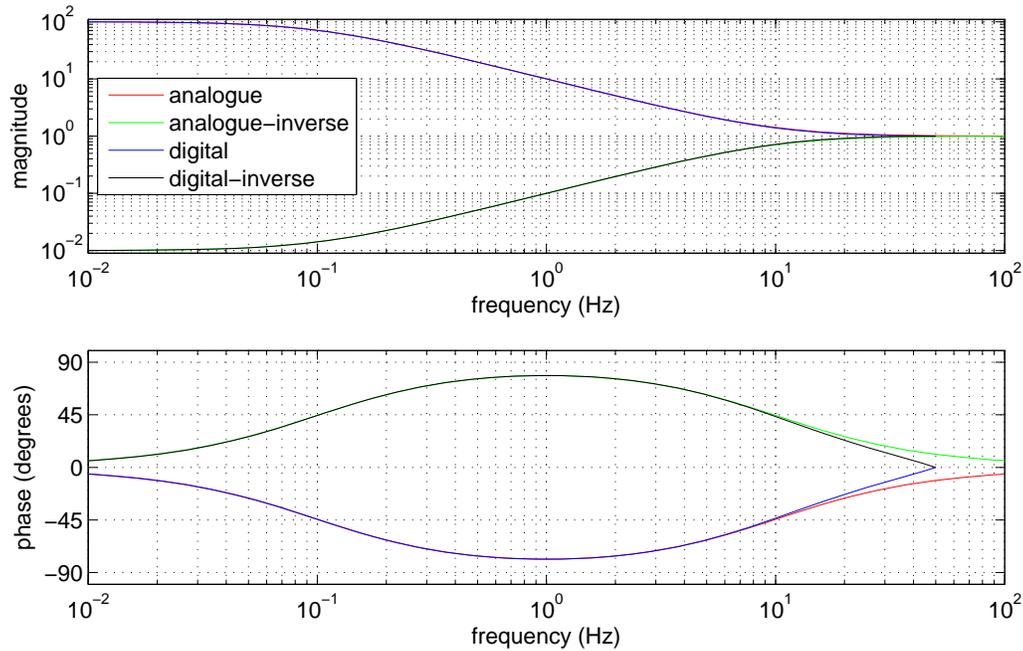


Figure 8.1: Bode plots to compare a digital representations with a first-order analogue transfer function and its inverse. The analogue system has a single real pole at 0.1 Hz and single real zero at 10 Hz. When the transfer function is inverted the pole becomes a zero, and the zero a pole. The bilinear transform is employed to produce the digital equivalents, with a sampling frequency of 100 Hz. The highest frequency that can be represented in this case is 50 Hz and it can be seen that the digital response becomes a poor approximation to the analogue one at frequencies approaching this limit. Note that, in a practical digital system, there would be a finite time delay and corresponding phase-lag, not included here, and that further delays may be present from anti-aliasing and anti-imaging filters – see text.

an art, mainly due to the consequences of finite precision in the associated calculations. A bilinear transformation is commonly employed. To avoid problems of numerical accuracy in the associated calculations, complicated systems are broken down in to a series of second-order sections. These subsystems have up to two poles and two zeros, i.e. the transfer functions have no higher order than quadratic numerator and denominator. Such subsystems can be transformed more reliably.

The finite time-steps in digital processing limit the filter transfer functions that may be produced at frequencies approaching the Nyquist limit – see Figures 8.1 and 8.2. Note however that with modern computers the sampling rate is often limited by the analogue interfaces rather than the speed of processing. Where this is true the data stream can be up-sampled (interpolated) to a higher sampling rate for filtering, and then down-sampled (decimated) to the original sampling rate before conversion back to the analogue domain. This process can be used to improve the high-frequency response of digital filters.

One further consequence of discrete time is that there is a finite delay associated with the analogue to digital, signal processing and digital to analogue steps. This must be considered in the development of feedback loops based on digital controls. In practice, even more severe limits to high-frequency performance often arise from anti-aliasing or anti-imaging filters that may be

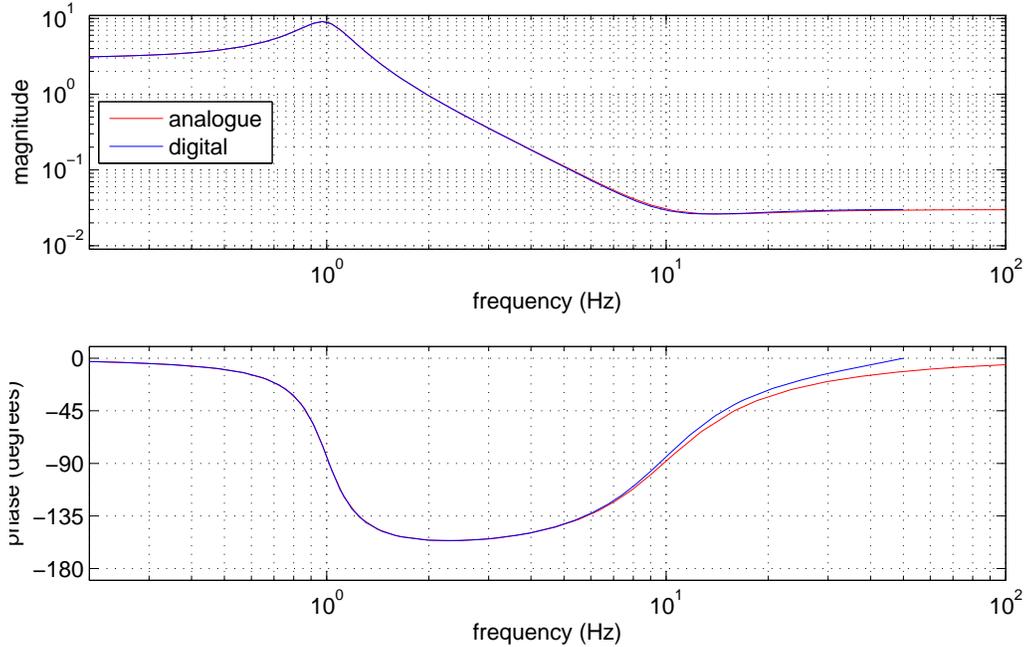


Figure 8.2: Bode plots for a second-order analogue system, and a digital approximation thereto. Here there is a complex pair of poles at 1 Hz with a resonance quality factor $Q = 3$, and a pair of zeros at 10 Hz, $Q = 1$. There is an overall gain factor of 3. The digital sampling frequency is 100 Hz.

required on the analogue input and outputs, respectively.

Aliasing occurs when the ingoing signal contains significant amplitude components at Fourier frequencies above the Nyquist limit. If these are not filtered out, they are incorrectly recorded their beat frequencies with the nearest harmonic of the sampling frequency. At the output, the digital signal has discrete steps from one sample to the next. To properly reconstruct the required analogue signal these steps require to be removed by the low-pass action of an anti-imaging (or reconstruction) filter. Further detail of the sampling and reconstruction processes is found in [68].

8.4 NEW: Degrees of freedom and operating points

We consider the optical components to be rigid bodies, each with six degrees of freedom. With practical, high-quality spherical surfaces, only three degrees of freedom per component are important: position along the direction of propagation of the light, referred to as the *longitudinal* coordinate, the *yaw* angle with respect to that direction, i.e. in the horizontal plane, and the *pitch* angle in the vertical plane. The other three degrees of freedom (vertical, horizontal normal to the beam and roll around the axis of the beam) may be important with respect to noise coupling into the length measurement in the case of imperfect mirrors. As discussed in Section 11.5, the mirrors typically have only small deviations from ideal spheres, so the coupling factors are small and do not significantly affect the control of the interferometer.

In the interferometer as a whole, one component, for example, a mirror or beam-splitter, may be chosen as the origin for the coordinate system. This allows one position and a pair of angles to be pre-defined. The positions and angles of the other components may then be described with

respect to this origin. Note, however, that the longitudinal degrees of freedom are measured with an optical ‘ruler’ that is based on the wavelength of the light, and so the wavelength should be counted as one longitudinal degree of freedom in the system as a whole (in the sense that the light has the same frequency everywhere which is usually true to a good approximation in the ultra-stable environment of a gravitational wave detector). Similarly the direction of the light beam entering the interferometer defines two angles.

To take an example, a simple cavity that is to be held on resonance with in-going light has two meaningful longitudinal degrees of freedom. For a cavity in isolation it would be usual to consider the the position of one mirror relative to the other and the frequency, or wavelength, of the light as the important parameters. Mathematically there are other equivalent choices, but in the control and operation of interferometers the point is to find a convenient set of control variables.

Similarly, a simple Michelson interferometer has three components and three longitudinal degrees of freedom. Again it would be usual to consider one component as a reference. If the beam-splitter is fixed, the three degrees of freedom are the two arm-lengths and the optical wavelength, or frequency.

If a pair of cavities were to be placed, one each, into the arms of the simple Michelson, the single degree of freedom of each mirror is replaced with the two of the cavity, for a total of five: once again, the same as the number of components. Fixing the beam-splitter, these are the laser wavelength, the two distances from the beam-splitter to the near mirrors of the cavities and the two lengths of the cavities.

An example of the degrees of freedom relevant to longitudinal control of a more complex system is shown in Section 8.10.

The choice between employing absolute or relative coordinates for the positions (and angles) of interferometer components is reflected in differences of approach in the available modelling software. In a FINESSE model of a two-mirror cavity, for example, the longitudinal positions of the two mirrors are specified, and adjusting either of them changes the resonant condition of the cavity (see, for example, Section 5.6.1). Likewise, adjusting the position of the input mirror changes the phase of both the light in the cavity, and the light reflected from the cavity. See Section 2.1 for a discussion of this point.

An operating interferometer requires various interference conditions to be maintained, e.g. cavities should be kept on resonance, the dark-fringe condition in a Michelson interferometer must be met, and so forth. For each degree of freedom this implies that there is an optimum value for best sensitivity or an *operating point* in the multi-dimensional space representing the degrees of freedom. This point is not usually unique: for example, signals repeat modulo one round-trip wavelength, see below.

As most or all degrees of freedom are subject to movement or drift, they must be controlled, generally by designing and implementing a separate control loop for each one. These loops must be designed to hold the value of the degree of freedom close to such an operating point, where ‘close’ is determined by tolerance bounds that must be determined by calculation.

In most cases it is possible to evaluate a tolerance interval around the operating point. The limits usually arise in the consideration of the coupling of some kind of noise into the sensitive measurement (frequency noise, power noise, beam direction noise, etc.). For example, in the case of the dark fringe, sensitivity to laser power noise is at a minimum at the perfectly dark condition, and the tolerable increase in this coupling may be used to set bounds on deviations from the operating point.

Bounds may also be set by considering the required linearity of signals. Non-linearity can lead to beating, which mixes noise into the measurement band. For example if there is a narrow spectral feature or ‘line’, such as a calibration line that may be applied to monitor instrumental sensitivity, or a suspension violin mode ¹¹ in the measurement band, beating this with low frequency motion

¹¹To minimise thermal noise in suspensions, low-loss materials and techniques are employed to avoid dissipation.

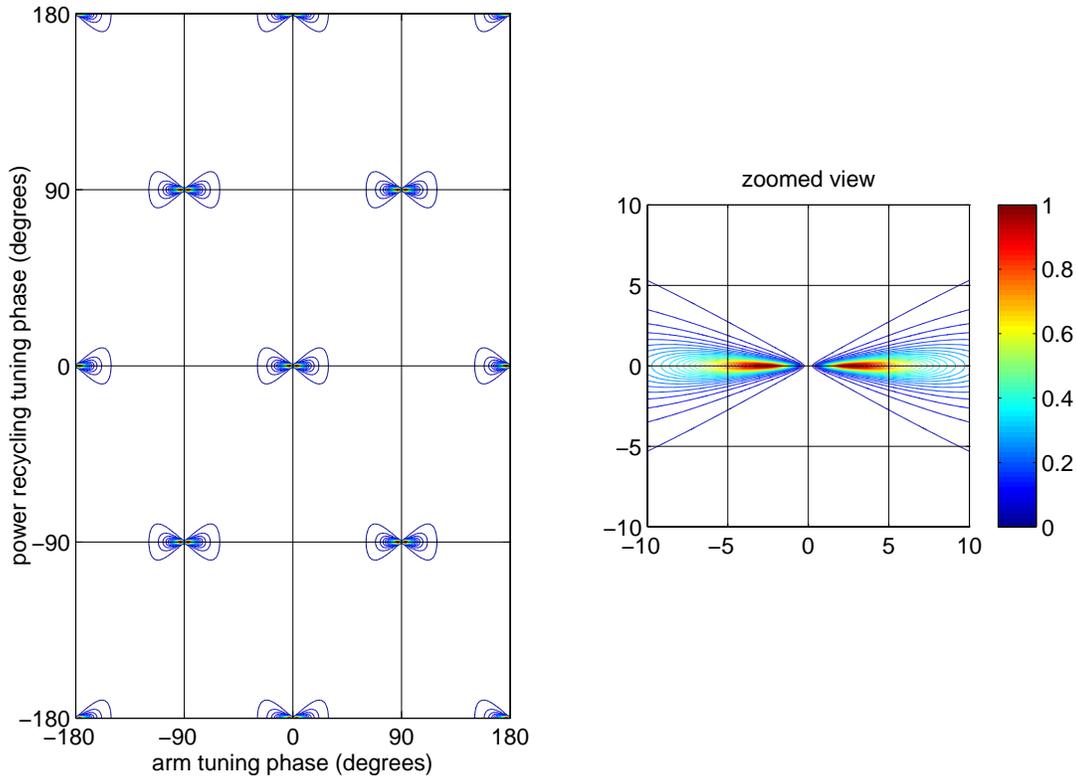


Figure 8.3: Simplified example illustrating the restricted phase space volume in which interferometer control signals are expected to achieve significant magnitudes. In the left panel we show the modulus of the light amplitude emerging at the detection/output port of a power recycled Michelson interferometer as a function of both the length difference between the arms (in the plot, the two end mirrors have their tuning phase shifted by the amount shown, but in opposition) and the tuning of the power recycling (the mirror has its tuning phase shifted by the amount shown). The normalised amplitude is shown on a linear scale from zero to one. These two degrees of freedom are swept over 2 cycles from the nominal operating point at (0,0). The other possible longitudinal degrees of freedom, namely the common mode arm length and the optical frequency are kept constant. The size of a signal designed to sense the differential degree of freedom, and allow the interferometer to be locked at the operating point, would have significant magnitude only in the region of the features like the one near (0,0) where there is a significant gradient in the horizontal direction in the plot. In this example, the power recycling mirror has a transmission of 1%, and other components have no loss. In a practical detector there would be several other degrees of freedom. Typically there would also be cavities of higher finesse, leading to even narrower features. The right panel shows a magnified view of one of the ‘islands’ of useful signal, the operating point is a small region at coordinates (0,0) where the light power is low.

of suspended components will produce sidebands on either side of the narrow feature, and these may be of higher amplitude than the noise background at the frequencies of interest near the line. Non-linear operation may also cause problems for control systems, as its presence implies that the gain of control loops will depend on the magnitude of deviations from the nominal operating point. In the following (Section 8.5) it will be seen that the normal process of sensing the length of a cavity is reasonably linear only within a very narrow range, in comparison to the wavelength of light, around the operating point, at least for a cavity of high finesse – a range of distance of order λ/F (see Section 5.1), or smaller.

In designing a control system for an interferometer, one can in principle consider the space of possible values of all the degrees of freedom in an interferometer, but it is more usual to work with a sub-space, e.g. only the longitudinal degrees. In the angular case there is usually a unique operating point per degree of freedom corresponding to one optimal alignment, but in the longitudinal case operating points are repeated as the relevant round-trip phase change steps in multiples of 2π , i.e. one wavelength change in round-trip optical path distance. In this case it is usual to consider the (hyper-)volume containing one repeat in each dimension: for km-long interferometers there is very little difference between adjacent volumes. In a typical interferometer designed for gravitational wave detection, the number of degrees of freedom in combination with requirements on noise coupling and linearity mean that only a vanishingly small volume within the phase space corresponds to the acceptable region around the desired operating point. This suggests one of the important questions in operating a gravitational wave detector: how to bring every degree of freedom to the desired operating point.

The diminutive scale of the useful volume in phase space can be illustrated by means of a simplified example. Here we consider the case of two degrees of freedom in a power recycled Michelson interferometer. Even fixing the location of the beam-splitter, there are three degrees of freedom (i.e. common arm length, differential arm length and longitudinal position of the power recycling mirror). However, we choose to produce a contour plot showing signal sizes as a function of just two degrees of freedom, Figure 8.3. Here we vary the difference in the lengths of the two arms while keeping the average (or common mode) arm length fixed, and also to vary the position of the power recycling mirror. In a practical interferometer there would be several other degrees of freedom associated with, for example, arm cavities, signal recycling and control of the common-mode arm length (or laser frequency), and in most cases the cavities would be of higher finesse producing even narrower features – see, for example, the parameters for Advanced LIGO in Appendix B.

The complexity of sensing and control becomes apparent when one considers that, in the common case of the freely-suspended optical components in a ground-based interferometric gravitational wave detector, the initial condition, at the point of ‘switching on’ the controls can be any random point within the space, with – in addition – a wide range of initial velocities associated with each degree of freedom: up to perhaps of order one wavelength per second, in a typical ground-based instrument. How this is dealt with is summarised in Section 8.1.

8.5 Error signals and transfer functions

In general, we will call an *error signal* any measured signal suitable for stabilising a certain experimental parameter p with a servo loop. The aim is to maintain the variable p at a user-defined value, the *operating point*, p_0 . Therefore, the error signal must be a function of the parameter p . In most cases it is preferable to have a bipolar signal with a zero crossing at the operating point.

The resonant modes of these suspensions are seen in the frequency domain as narrow spectral features, or lines. The violin modes are transverse oscillations of the stretched suspension fibres that support the mirrors, which vibrate much like a violin string. The frequencies of these modes typically lie between 300 and 800 Hz, and they are often conspicuous in the spectra of signals from gravitational wave detectors.

The slope of the error signal at the operating point is a measure of the ‘gain’ of the sensor, which in the case of interferometers is a combination of optics and electronics.

Transfer functions describe the propagation of a periodic signal through a *plant* and are usually given as plots of amplitude and phase over frequency, e.g. as Bode plots (see the following section). By definition a transfer function describes only the linear coupling of signals inside a system. This means a transfer function is independent of the actual signal size. For small signals or small deviations, most systems can be linearised and correctly described by transfer functions.

Experimentally, network analysers are commonly used to measure a transfer function: one connects a periodic signal (the *source*) to an actuator of the plant (which is to be analysed) and to an input of the analyser. A signal from a sensor that monitors a certain parameter of the plant is connected to the second analyser input. By mixing the source with the sensor signal the analyser can determine the amplitude and phase of the input signal with respect to the source (amplitude equals one and the phase equals zero when both signals are identical).

Mathematically, transfer functions can be modelled similarly: applying a sinusoidal signal $\sin(\omega_s t)$ to the interferometer, e.g., as a position modulation of a cavity mirror, will create phase modulation sidebands with a frequency offset of $\pm\omega_s$ to the carrier light. If such light is detected in the right way by a photodiode, it will include a signal at the frequency component ω_s , which can be extracted, for example, by means of demodulation (see Section 4.2).

Transfer functions are of particular interest in relation to error signals. Typically a transfer function of the error signal is required for the design of the respective electronic servo. A ‘transfer function of the error signal’ usually refers to a very specific setup: the system is held at its operating point, such that, on average, $\bar{p} = p_0$. A signal is applied to the system in the form of a very small sinusoidal disturbance of p . The transfer function is then constructed by computing for each signal frequency the ratio of the error signal and the injected signal. Figure 8.4 shows an example of an error signal and its corresponding transfer function. The operating point shall be at

$$x_d = 0 \quad \text{and} \quad x_{\text{EP}}(x_d = 0) = 0. \quad (8.4)$$

The optical transfer function T_{opt,x_d} with respect to this error signal is defined by

$$\tilde{x}_{\text{EP}}(f) = T_{\text{opt},x_d} T_{\text{det}} \tilde{x}_d(f), \quad (8.5)$$

with T_{det} as the transfer function of the sensor. In the following, T_{det} is assumed to be unity. At the zero crossing the slope of the error signal represents the magnitude of the transfer function for low frequencies:

$$\left| \frac{dx_{\text{EP}}}{dx_d} \right|_{x_d=0} = |T_{\text{opt},x_d}|_{f \rightarrow 0} \quad (8.6)$$

The quantity above will be called the *error-signal slope* in the following text. It is proportional to the *optical gain* $|T_{\text{opt},x_d}|$, which describes the amplification of the gravitational-wave signal by the optical instrument.

8.6 NEW: Bode plots – traditional control theory for SISO loops

An essential feature of a control system is stability, i.e. for a finite input the output should always be bounded. This is equivalent to requiring all of the transfer function poles to correspond to decaying exponentials, so their real parts must be strictly negative.

Prior to the routine application of computers, a number of tools (plots) were developed to facilitate control system design. Although the root-locus, Nyquist and Bode plots continue to be applied, computer models remove the practical (calculational) advantages of one over another. All of these methods present essentially equivalent information, and the choice of one over another is a

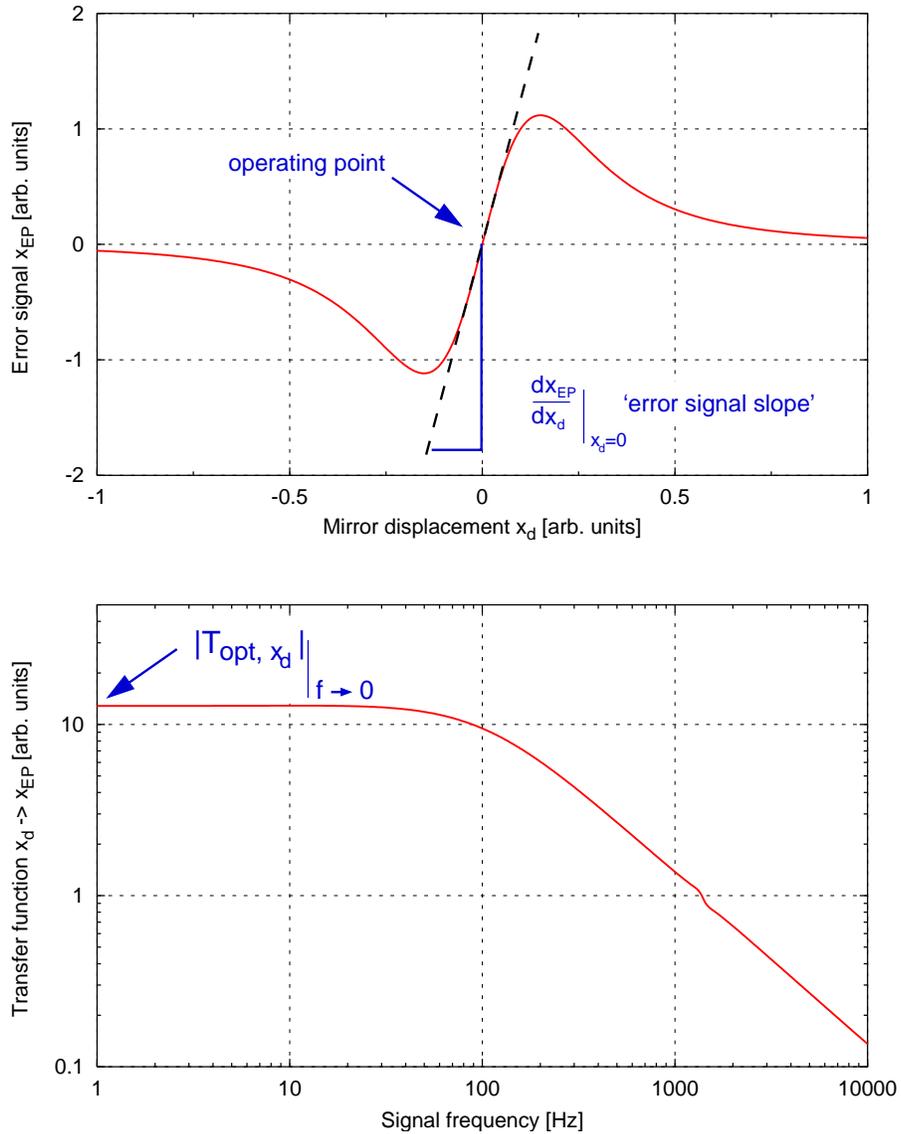


Figure 8.4: Example of an error signal: the top graph shows the electronic interferometer output signal as a function of mirror displacement. The operating point is given as the zero crossing, and the *error-signal slope* is defined as the slope at the operating point. The right graph shows the magnitude of the transfer function *mirror displacement* \rightarrow *error signal*. The slope of the error signal (left graph) is equal to the low frequency limit of the transfer function magnitude (see Equation (8.6)).

matter of convenience or familiarity. Since Bode plots provide a complete description of single-input single-output (SISO) LTI control loops we choose to describe that approach as an example.

Throughout this section, the system is described in continuous time, i.e. as an analogue model. When the technique is applied to digital control systems discrete-time models are needed as discussed in Section 8.3.

A Bode plot of a system shows its transfer function in the form of log-magnitude and linear-phase graphs against a logarithmic frequency axis – conventionally in vertically-stacked plots with matching, aligned frequency axes. In the context of the design of complete negative feedback loops, it is common, though not universal, to add π to the phase to represent the overall negative sign – this convention is assumed here. The standard procedure starts with consideration of the open-loop Bode plot. In this, the loop is broken (in the model) at a convenient point, and the transfer function from there back to just before the break is calculated and plotted. Remember that the total transfer function is computed as the product of individual transfer functions of parts of the loop that are connected in series. Particular attention is paid to the regions close to points where the transfer function magnitude crosses unity (i.e. zero on the log scale), called the unity gain point(s), and where the phase crosses $-\pi$ in absolute terms, *not* modulo 2π . The transfer function is then characterised by the phase margin and the gain margin. The phase margin is the phase of the transfer function plus π at the frequency where the gain is unity, and the gain margin is the inverse of the gain where the phase is $-\pi$ (or the negative of the log gain). If there are multiple unity gain points the smallest phase margin, and the smallest gain margin, dominate. If the smallest gain and phase margins are both positive, the system is stable. Note that if there are multiple paths or ‘loops’, these are dealt with by applying loop algebra to reduce the system to a single feedback loop without subsidiary loops.

Traditionally these methods were extended to reveal properties of the closed-loop system, i.e. of the original model without any break. This was done because, for transfer functions of low order (one, two or three poles), there are simple expressions that relate the phase margin to the ringing, or equivalently damping, of the closed-loop response. When computer models are employed for systems of greater complexity there is no need for these rules or guidelines and it is common to transform back to the time domain, calculate the impulse response of the closed loop system, and characterise its resonant frequencies and damping without reliance on rules.

As a concrete example of a Bode plot, we include one representing a system that approximates the transfer function shown in Figure 8.4). The system consists of a gain factor (12) and a single pole at 100 Hz (or $2\pi \times 100$ radian/s). The transfer function may be written

$$G(s) = \frac{12}{s + 200\pi}, \quad (8.7)$$

such that there is a single real pole at complex frequency $s = -200\pi$. Further explanation of the mathematics of transfer functions is given in Section 8.2, while Bode plots of higher order systems in both continuous and discrete time are found in Section 8.3.

The construction and utility of the Bode plot originates in part from the properties of a common subset of transfer functions that represents stable, causal systems. Such systems are called *minimum phase* as a consequence of the locations of their zeros in the s -plane. In a causal system the output lags the input. Stable, causal LTI systems are also invertible, i.e. the transfer function numerator and denominator can be swapped, or equivalently all the poles and zeros may be exchanged resulting in another stable, causal system. For this to work the zeros of the system must have negative real parts, so that when they become poles in the inverse system they are damped. It can be shown that in such a system there is a strict relationship between the phase and the slope of the log-magnitude, as shown on a Bode plot – one is a Hilbert transform of the other. In practice this is equivalent to writing that when the magnitude graph has a slope of f^{-n} , where f is the frequency, the phase approaches $-n\pi/2$. This method allows the loop to be designed to meet

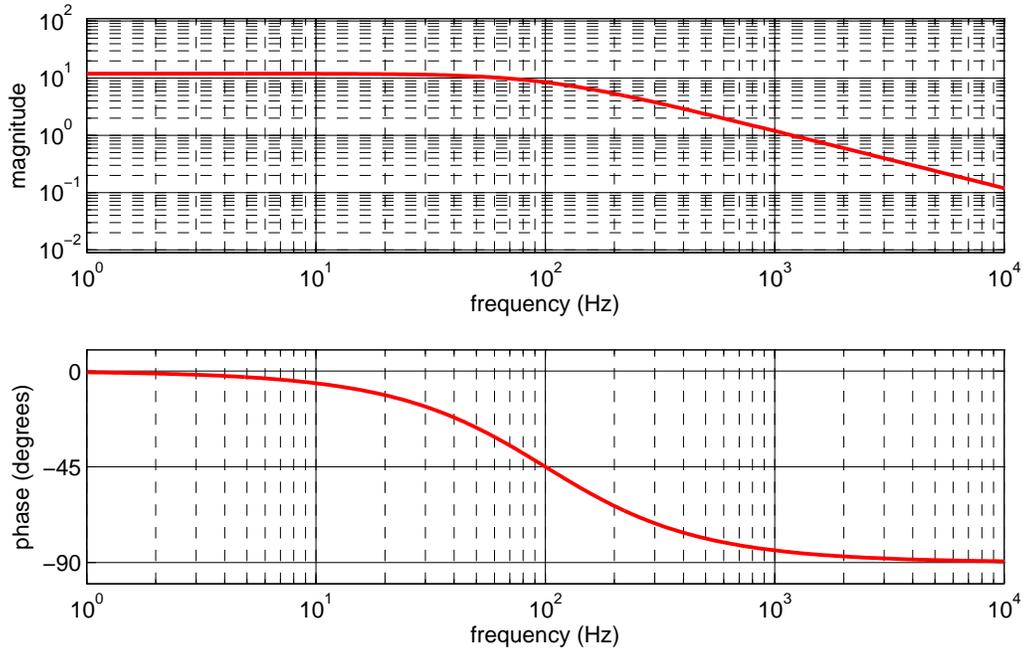


Figure 8.5: Example Bode plot for a simple first order low-pass transfer function with a gain of 12 at low-frequency and a single pole at 100 Hz. The upper panel shows the magnitude of the response, presented on a logarithmic scale, as a function of frequency (here in Hz, may also be radian/s). The lower panel shows the corresponding phase in degrees. As noted in the text, for minimum-phase systems such as this, the magnitude and phase are not independent, but both provide useful information in the design of control loops. Where the response is flat with frequency, the phase is asymptotically zero; where the response varies as $1/f$, there is a phase lag approaching 90° . As explained in the text, if this plot were to represent the open-loop transfer function of a negative feedback loop, important properties of the loop can be read-off by inspection. For example, stability can be assessed by checking the phase margin at the unity gain frequency (here the gain is unity at 1200 Hz). At this frequency the phase is about -85° and the phase margin is given by the difference of this from -180° , or 95° . This is far from zero, and so the closed-loop response is predicted to be stable.

various goals that are usually expressed in terms of gain (or attenuation) that must be achieved in one or more range of frequencies, with stability checked by reading off the phase and gain margins.

In interferometry the *optical transfer function* is usually a significant aspect of control loops. Such transfer functions may be measured or found by calculation (e.g. with FINESSE). The corresponding transfer functions can be found by applying the techniques described in Section 8.5.

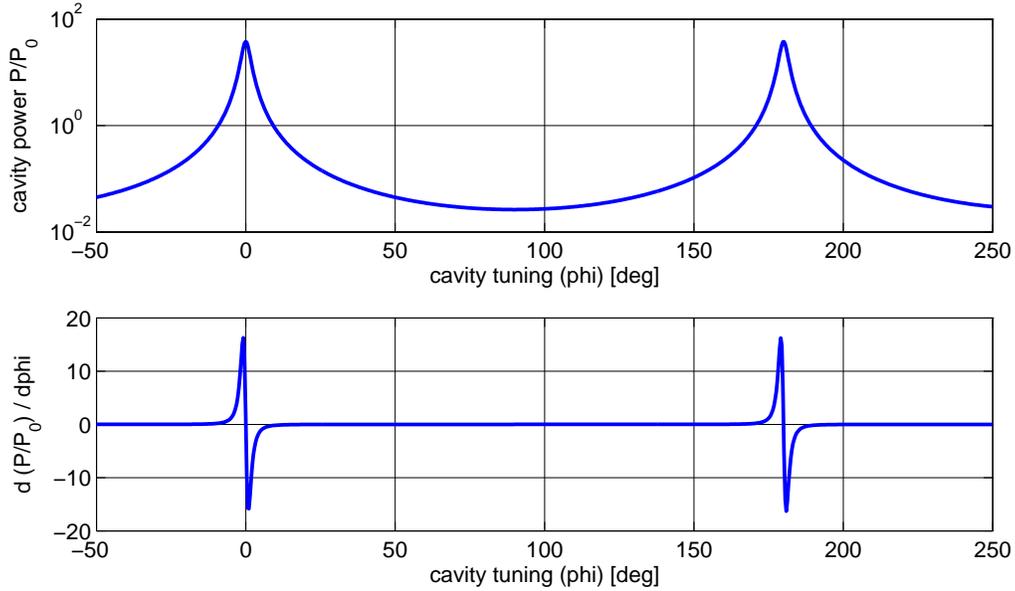


Figure 8.6: The top plot shows the cavity power as a function of the cavity tuning. A tuning of 360° refers to a change in the cavity length by one laser wavelength. The bottom plot shows the differentiation of the upper trace. This illustrates that near resonance the cavity power changes very rapidly when the cavity length changes. However, for most tunings the cavity seems not sensitive at all.

8.7 Fabry-Perot length sensing

In Figure 5.2 we have plotted the circulating power in a Fabry-Perot cavity as a function of the laser frequency. The steep features in this plot indicate that such a cavity can be used to measure changes in the laser frequency. From the equation for the circulating power (see Equation (5.1)),

$$P_1/P_0 = \frac{T_1}{1 + R_1 R_2 - 2r_1 r_2 \cos(2kL)} = \frac{T_1}{d}, \quad (8.8)$$

we can see that the actual frequency dependence is given by the $\cos(2kL)$ term. Writing this term as

$$\cos(2kL) = \cos\left(2\pi \frac{Lf}{c}\right), \quad (8.9)$$

we can highlight the fact that the cavity is in fact a reference for the laser frequency in relation to the cavity length. If we know the cavity length very well, a cavity should be a good instrument to measure the frequency of a laser beam. However, if we know the laser frequency very accurately, we can use an optical cavity to measure a length. In the following we will detail the optical setup and behaviour of a cavity used for a length measurement. The same reasoning applies for frequency

measurements. If we make use of the resonant power enhancement of the cavity to measure the cavity length, we can derive the sensitivity of the cavity from the differentiation of Equation (5.1), which gives the slope of the trace shown in Figure 5.2,

$$\frac{dP_1/P_0}{dL} = \frac{-4T_1r_1r_2k \sin(2kL)}{d^2}, \quad (8.10)$$

with d as defined in Equation (8.8). This is plotted in Figure 8.6 together with the cavity power as a function of the cavity tuning. From Figure 8.6 we can deduce a few key features of the cavity:

- The cavity must be held as near as possible to the resonance for maximum sensitivity. This is the reason that active servo control systems play an important role in modern laser interferometers.
- If we want to use the power directly as an error signal for the length, we cannot use the cavity directly on resonance because there the optical gain is zero. A suitable error signal (i.e. a bipolar signal) can be constructed by adding an offset to the light power signal. A control system utilising this method is often called *DC-lock* or *offset-lock*. However, we show below that more elegant alternative methods for generating error signals exist.
- The differentiation of the cavity power looks like a perfect error signal for holding the cavity on resonance. A signal proportional to such differentiation can be achieved with a modulation-demodulation technique.

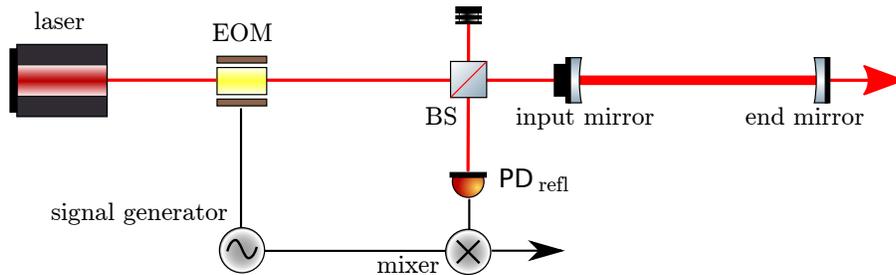


Figure 8.7: Typical setup for using the Pound–Drever–Hall scheme for length sensing and with a two-mirror cavity: the laser beam is phase modulated with an electro-optical modulator (EOM). The modulation frequency is often in the radio frequency range. The photodiode signal in reflection is then electrically demodulated at the same frequency.

8.8 The Pound–Drever–Hall length sensing scheme

This scheme for stabilising the frequency of a light field to the length of a cavity, or vice versa, is based on much older techniques for performing very similar actions with microwaves and microwave resonators [134]. Drever and Hall have adapted such techniques for use in the optical regime [61] and today what is now called the *Pound–Drever–Hall* technique can be found in a great number of different types of optical setups. An example layout of this scheme is shown in Figure 8.7, in this case for generating a length (or frequency) signal of a two-mirror cavity. The laser is passed through an electro-optical modulator, which applies a periodic phase modulation at a fixed frequency. In many cases the modulation frequency is chosen such that it resides in the radio frequency band for which low-cost, low-noise electronic components are available. The phase modulated light is then injected into the cavity. However, from the frequency domain analysis introduced in Section 5,

we know that in most cases not all the light can be injected into the cavity. Let's consider the example of an over-coupled cavity with the reflectivity of the end mirror $R_2 < 1$. Such a cavity would have a frequency response as shown in the top traces of Figure 5.3 (recall that the origin of the frequency axis refers to an arbitrarily chosen default frequency, which for this figure has been selected to be a resonance frequency of the cavity). If the cavity is held on resonance for the unmodulated carrier field, this field enters the cavity, gets resonantly enhanced and a substantial fraction is transmitted. If the frequency offset of the modulation sidebands is chosen such that it does not coincide with (or is near to) an integer multiple of the cavity's free spectral range, the modulation sidebands are mostly reflected by the cavity and will not be influenced as much by the resonance condition of the cavity as the carrier. The photodiode measuring the reflected light will see the optical beat between the carrier field and the modulation sidebands. This includes a component at the modulation frequency which is a measure of the phase difference between the carrier field and the sidebands (given the setup as described above). Any slight change of the cavity length would introduce a proportional change in the phase of the carrier field and no change in the sideband fields. Thus the photodiode signal can be used to measure the length changes of the cavity. One of the advantages of this method is the fact that the so-generated signal is bipolar with a zero crossing and steep slope exactly at the cavity's resonance, see Figure 8.8.

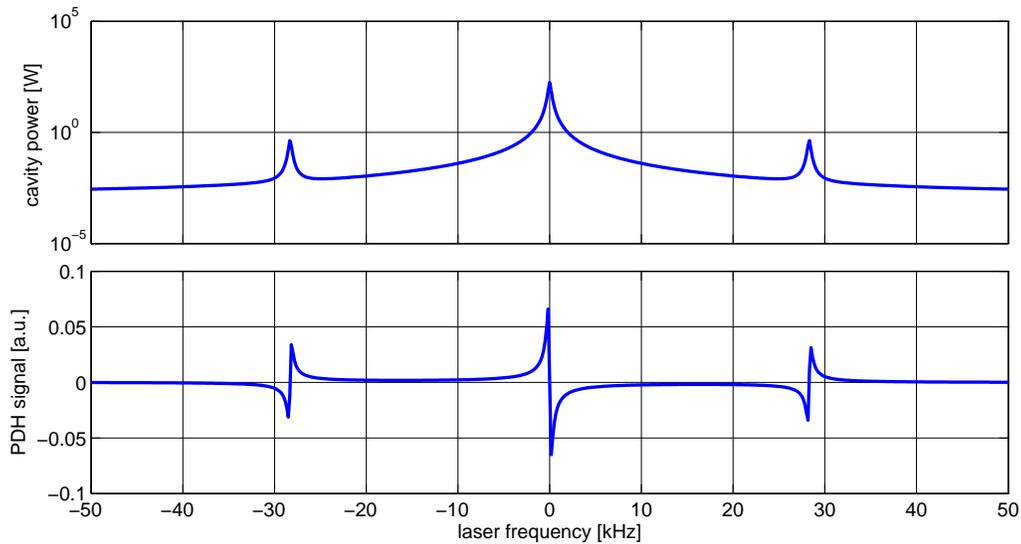


Figure 8.8: This figure shows an example of a Pound–Drever–Hall (PDH) signal of a two-mirror cavity. The plots refer to a setup in which the cavity mirrors are stationary and the frequency of the input laser is tuned linearly. The upper trace shows the light power circulating in the cavity. The three peaks correspond to the frequency tunings for which the carrier (main central peak) or the modulation sidebands (smaller side peaks) are resonant in the cavity. The lower trace shows the PDH signal for the same frequency tuning. Coincident with the peaks in the upper trace are bipolar structures in the lower trace. Each of the bipolar structures would be suitable as a length-sensing signal. In most cases the central structure is used, as experimentally it can be easily identified because its slope has a different sign compared to the sideband structures.

8.9 Michelson length sensing

Similarly to the two-mirror cavity, we can start to understand the length-sensing capabilities of the Michelson interferometer by looking at the output light power as a function of a mirror movement, as shown in Figure 5.6. The power changes as sine squared with the maximum slope at the point when the output power (in what we call the South port) is half the input power. The slope of the output power, which is the *optical gain* of the instrument for detecting a differential arm-length change ΔL with a photo detector in the South port can be written as

$$\frac{dS}{d\Delta L} = \frac{2\pi P_0}{\lambda} \sin\left(\frac{4\pi}{\lambda} \Delta L\right) \quad (8.11)$$

and is shown in Figure 8.9. The most notable difference of the optical gain of the Michelson interferometer with respect to the Fabry-Perot interferometer (see Figure 8.6) is the wider, more smooth distribution of the gain. This is due to the fact that the cavity example is based on a high-finesse cavity in which the optical resonance effect is dominant. In a basic Michelson interferometer such resonance enhancement is not present.

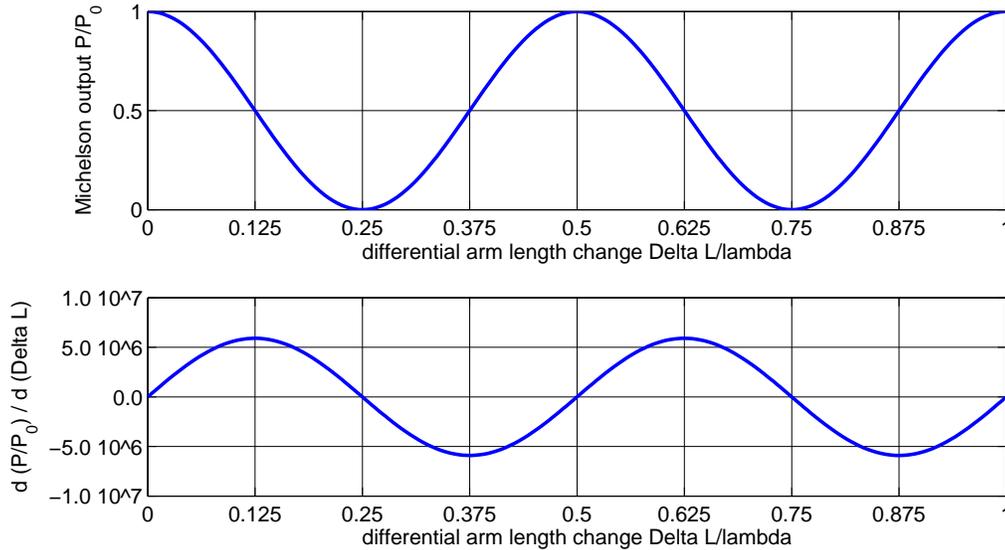


Figure 8.9: Power and slope of a Michelson interferometer. The upper plot shows the output power of a Michelson interferometer as detected in the South port (as already shown in Figure 5.6). The lower plot shows the optical gain of the instrument as given by the slope of the upper plot.

However, the main difference is that the measurement is made differentially by comparing two lengths. This allows one to separate a larger number of possible noise contributions, for example noise in the laser light source, such as amplitude or frequency noise. This is why the main instrument for gravitational-wave measurements is a Michelson interferometer. However, the resonant enhancement of light power can be added to the Michelson, for example, by using Fabry-Perot cavities within the Michelson as introduced in Section 7.2. This construction of new topologies by combining Michelson and Fabry-Perot interferometers has culminated in the dual-recycled Fabry-Perot Michelson configuration that is the subject of the following section.

The Michelson interferometer has two longitudinal degrees of freedom (setting aside the optical wavelength as a third degree of freedom). These can be represented by the positions (along the optical axes) of the end mirrors. However, it is more efficient to use proper linear combinations

of these and describe the Michelson interferometer length or position information by the *common* and *differential arm length*, as introduced in Equation (5.10):

$$\begin{aligned}\bar{L} &= \frac{L_N + L_E}{2} \\ \Delta L &= L_N - L_E.\end{aligned}$$

The Michelson interferometer is intrinsically insensitive to the common arm length \bar{L} .

8.10 NEW: Advanced LIGO: an example of a complex interferometer

In this section we present a simplified overview of the dual-recycled Fabry-Perot Michelson interferometer (**DRFPMI**) topology, as exemplified by the Advanced LIGO detectors [85]. At this level of detail, the description applies equally to Advanced Virgo [6].

Our description builds on the ideas presented in Section 7. The DRFPMI configuration is built around a Michelson interferometer, with 4 cavities added to modify the behaviour of the system. As shown in Figure 8.10, there are two Fabry-Perot arm cavities that extend the light path in the arms of the interferometer to enhance the signal due to gravitational waves. The Michelson is operated at, or very close to, a dark fringe so that, apart from losses, most of the light is reflected back in the direction towards laser and injection optics, hence this input port is also called the ‘bright’ port of the interferometer. A partially transmitting power-recycling mirror, placed at the bright port and adjusted to resonate the light, allows the power circulating within the interferometer to build up (ideally by a factor of 1/loss), reducing the requirement for input light power.

The final cavity is formed by placing a partially transmitting mirror between the output or ‘dark’ port of the Michelson and the detection optics (consisting of a photo-detector, and perhaps some other components). This mirror recycles light that carries signal information to the photo-detector, and is called the signal recycling mirror – see Section 7.3 for an introduction to this aspect of the interferometer configuration.

The idea of a bright fringe or port and dark fringe or port can be extended to form one of the central concepts in the control of complex interferometers. In the condition described, with the input or power recycling port maintained in the bright state, and the output or signal recycling port held in the dark state, there is a separation of light-field components to one or other port according to their relative state in the interferometer arms. Here ‘component’ means light at a single frequency, i.e. a carrier or a sideband, and in a single optical mode (for a discussion of spatial modes, see Section 9). Such light-field components, which have spatial and temporal coherence, can interfere. If they have the same phase in the two arms they interfere constructively at the bright port. If they have the opposite phase in the two arms they interfere destructively at the dark port. Note that this arises because of the choice of interference of the carrier light to create the bright and dark ports.

In the same way that the carrier light which has a common phase in the two arms appears at the bright port, any perturbation of the interferometer that is common to the two arms generates higher order modes and/or sidebands that have the same phase in the two arms and thus causes an effect on the optical field at the bright port. Examples of this would be in-phase arm-length changes, or the addition of the same amount of optical loss in the two arms. On the other hand, perturbations that are exactly out-of-phase between the two arms have an effect on the light field at the dark port. An example would be that gravitational waves produce differential phase modulation sidebands that have opposite phase in the two arms, and these interfere constructively at the output port.

The distinction between effects that are either in-phase or have opposing phases is frequently important in the control of interferometers. As noted in the previous section for the case of the simple Michelson, it has become standard to consider the two physical degrees of freedom associated with the arms of an interferometer in logical-combination as the *common mode* and the *differential*

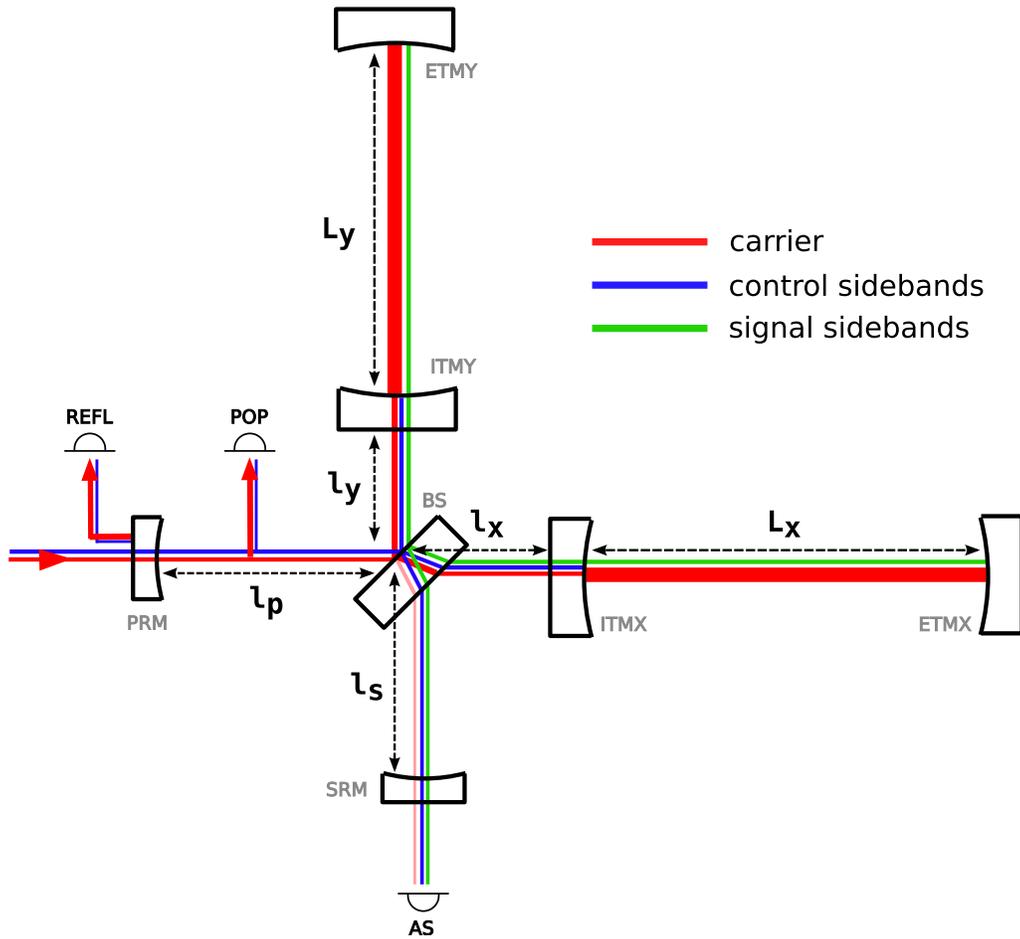


Figure 8.10: Schematic illustration of the dual-recycled Fabry-Perot Michelson configuration showing the main optical components (i.e. 6 mirrors and the beam-splitter), components of the light field in different regions of the interferometer, photo-detectors and one possible representation of the degrees of freedom. The system is controlled by signals obtained from three photo-detectors: REFL, short for reflected port, and POP, short for pick-off-port detect aspects of the light reflected by the Michelson, while the transmitted light is detected at the anti-symmetric port (AS). The degrees of freedom are indicated by the various lengths ‘L’ and ‘l’ with subscripts described in the text of the current section. Note that the lengths marked with capital ‘L’s involve the long arms of the interferometer, while the others involve the short distances from the beam-splitter to the nearby components. Further detail of the sensing and control is discussed in Appendix B.

mode. For the same reasons, the bright port is also called the *symmetric port* and the dark port is called the *anti-symmetric port*.

The advantage of the choice of common and differential modes may be seen in consideration of control loops to deal with laser-frequency fluctuations and to keep the interferometer locked at the dark fringe, to give but two examples. In a nearly-symmetrical interferometer a fluctuation of the frequency of the in-going light will lead to a primarily common-mode effect, and it makes sense to stabilise the laser frequency with respect to the common mode of the two arms. Similarly the gravitational wave signal may be read-out as part of the error signal of a control loop for the dark fringe. Such a loop should act on the differential mode, rather than on the length of one arm cavity, or the other.

Referring to Figure 8.10, the physical optical path-lengths shown on the diagram may be related to the logical degrees of freedom applied in interferometer control in the following way. The solution presented here is not unique, but is intended as an example of one way to approach the problem. We deal with the degrees of freedom in turn, take the beam-splitter as a point of reference for the small 'l' lengths (as suggested on the figure) and assume the laser frequency is fixed. This leaves 5 degrees of freedom to be controlled:

- **CARM** Common-mode arm length, $CARM = L_x + L_y$. This corresponds to the average length of the arm cavities and is adjusted to keep both arm-cavities on resonance.
- **DARM** Differential arm length, $DARM = L_x - L_y$. This corresponds to the difference in length of the two arm cavities and is used to maximise the constructive interference, at the output port, of sidebands resulting from differential arm-length changes (this degree of freedom is therefore the source of the gravitational wave channel).
- **MICH** Michelson arm length difference, $MICH = l_x - l_y$. MICH corresponds to the difference in length of the short arms of the Michelson, between the ITMs and the beam-splitter, and determines the state of interference at the output port. In Advanced LIGO, the Michelson is operated close to the dark fringe.
- **PRCL** Power recycling cavity length, $PRCL = L_p + \frac{l_x + l_y}{2}$. The power recycling cavity is operated on resonance to maximise the power coupled into the central interferometer.
- **SRCL** Signal recycling cavity length, $SRCL = L_s + \frac{l_x + l_y}{2}$. This corresponds to the resonance condition of the signal recycling cavity. The operating point of SRCL depends on the mode of operation of the interferometer. It can be tuned for a particular frequency of gravitational wave or for broadband operation.

As a reminder, we restate that in a gravitational wave detector, we are concerned with microscopic variations of path lengths that may be up to several km.

In the following sections we discuss, in general terms, how the error signals can be extracted from the optical system, combined and processed to provide signals representing the degrees of freedom to be controlled, and how the resulting signals can be fed-back to force the optical system into the desired condition.

8.11 NEW: Separating mixtures of the degrees of freedom: control matrices

In practice, each error signal intended to represent a particular degree of freedom of the optical arrangement also contains some information about other degrees of freedom. To give a simple example of the mixing that may occur, any motion that leads to a change in the circulating light

power in a cavity is likely to couple, at some level, to every signal that depends on the intra-cavity light, unless the signal is precisely zero.

In most cases such mixing is undesirable as it is easier to design control systems to deal with one degree of freedom in isolation. In the worst case, if the mixing, or cross-coupling is strong, it can lead to the formation of unintended feedback paths. If the transfer function of such loops has a magnitude exceeding unity, there is a chance that the loop may be unstable. A common cause of such instability is a resonance in the unintended or ‘parasitic’ loop. At such a resonance high gain is typically accompanied by a phase lag of $-\pi$ which will tend to be unstable unless some compensation is included, e.g. in the form of a notch filter to cancel the resonance.

Unwanted mixing of signals can also occur at the point of actuation. For example, a mirror may be common to two degrees of freedom of an interferometer. In an interferometer with arm cavities, the cavity mirrors closest to the beam-splitter behave in this way. Moving such a mirror must then affect at least two length degrees of freedom. This can be seen in Figure 7.3 where motion of either of the two mirrors labelled ITMX and ITMY affects the phase of the light in the respective arm cavity and also the interference condition of the Michelson interferometer. In contrast, the end mirrors (ETMX, ETMY) each affect only one longitudinal degree of freedom.

A further possible source of mixing between degrees of freedom arises at the point of actuation. Feedback to control a mirror is often carried out in practice using an array of actuators, such as coil-magnet pairs, that push on the mirror at various points on its surface. For example, it is common to employ a square-array of four magnets attached to the rear surface of the mirror, as these allow longitudinal, pitch and yaw adjustment. If they are mounted close to the perimeter of the rear surface they may be out of the way of a transmitted light beam. With such an arrangement, each individual actuator causes changes to a mixture of angular and longitudinal degrees of freedom. If the actuators are not of precisely uniform strength and alignment, this leads to unintended components in the resultant force produced by the array. An *actuation matrix*, with frequency-dependent elements where necessary, can be employed to orthogonalise the response of the system to commands from the controller, at least to some degree of precision.

The elements of actuation and sensing matrices are typically determined as a result of simulation and measurement. Modelling may yield a set of starting values that suffice to allow the interferometer to operate. When operational residual mixing is normally determined by carrying out all possible transfer function measurements. The measurements allow coupling matrices to be determined, and inverting the coupling matrix provides the appropriate matrix necessary to remove unwanted mixing. This process is somewhat involved and benefits from automation.

8.12 NEW: Modern control methods in gravitational wave detectors

During the past few decades new methods of designing sophisticated controllers based on digital signal processing have emerged. A major benefit of the resulting ‘digital controls’ is that the response of a control filter can be adjusted by changing filter coefficients, this can even be achieved while the controller is operating, if that is required.

Digital control facilitates the application of so-called modern control methods in which optimisation methods are employed. As an indication of the possible advantages that may arise from this, we briefly mention two approaches to modern control of application in interferometry. For a relevant description of these see, e.g. [68].

In the first approach, we consider the generation of an optimal filter with fixed coefficients (gain, poles and zeros). In such a case, the plant to be controlled is characterised by some means, and the results are used in the design of an optimal filter. For example, if it can be assumed that a measurement produces an estimate of the system contaminated by noise, and a model of the system with the correct number of degrees of freedom exists, a Wiener filter may be formed as a result of least-squares fitting the model to the data. If the result is to be inverted to provide a

compensating filter in a control system, then the fit must be constrained produce a causal filter (with all poles and zeros having negative real parts, in an analogue model). The are standard methods by which this may be accomplished.

The next step up in sophistication is to find a controller that remains optimal even if the underlying plant changes (or if its parameters cannot be measured accurately before the controller is put into operation). Such an *adaptive* controller, employs a Kalman filter – also called a Linear Quadratic Estimator. This is implemented as an algorithm that operates on a series of measurements taken over time. These measurements are assumed to be contaminated with noise. The algorithm operates recursively to produce an optimal estimate of the state of the physical system. During this process a model of the system, i.e. a representation of the equations of motion, with relevant coefficients available to be adjusted, is iteratively updated. The model is assumed to have errors either as a result of poor starting estimates or due to drifting of parameters over time. A weighting function, also called a *cost function*, is applied to the measured data to allow less noisy or otherwise more important aspects of the data to have a stronger influence on the outcome. At each iteration the model is employed to predict the current state, this is then compared with the actual state and the results of the comparison are used to refine and update the model. When this method is made to operate, the model of the underlying system converges to an optimal solution for the given weighting function.

8.13 The Schnupp modulation scheme

In this and the following three sections (8.14, 8.15, 8.16), we introduce techniques for reading out signals from interferometers. These approaches complement and extend the Pound-Drever-Hall method for readout from Fabry-Perot cavities presented in Section 8.8.

Similar to the Fabry-Perot cavity, the Michelson interferometer is also often used to set an operating point where the optical gain of a direct light power detection is zero. This operating point, given by $\Delta L/\lambda = (2N + 1) \cdot 0.25$ with N a non-negative integer, is called *dark fringe*. This operating point has several advantages, the most important being the low (ideally zero) light power on the diode. Highly efficient and low-noise photodiodes usually use a small detector area and thus are typically not able to detect large power levels. By using the dark fringe operating point, the Michelson interferometer can be used as a *null instrument* or *null measurement*, which generally is a good method to reduce systematic errors [142].

One approach to make use of the advantages of the dark fringe operating point is to use an operating point very close to the dark fringe at which the optical gain is not yet zero. In such a scenario a careful trade-off calculation can be done by computing the signal-to-noise with noises that must be suppressed, such as the laser amplitude noise. This type of operation is usually referred to as *DC control* or *offset control* and is very similar to the similarly-named mechanism used with Fabry-Perot cavities.

Another option is to employ phase modulated light, similar to the Pound–Drever–Hall scheme described in Section 8.8. The optical layout of such a scheme is depicted in Figure 8.11: an electro-optical modulator is used to apply a phase modulation at a fixed frequency, usually in the RF range, to the monochromatic laser light before it enters the interferometer. The photodiode signal from the interferometer output is then demodulated at the same frequency. This scheme allows one to operate the interferometer precisely on the dark fringe. The method originally proposed by Lise Schnupp is also sometimes referred to as *frontal modulation*.

The optical gain of a Michelson interferometer with Schnupp modulation is shown in Figure 8.16 in Section 8.17.

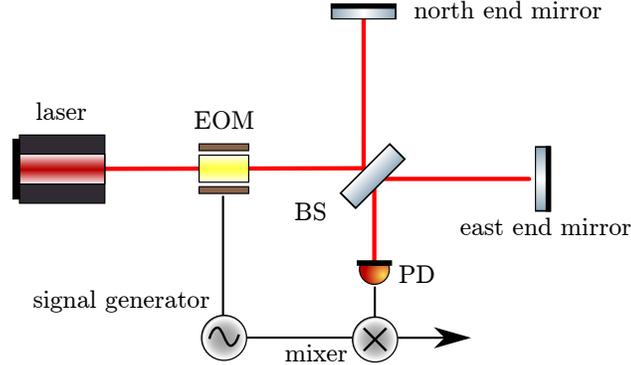


Figure 8.11: This length sensing scheme is often referred to as *frontal* or *Schnupp modulation*: an EOM is used to phase modulate the laser beam before entering the Michelson interferometer. The signal of the photodiode in the South port is then demodulated at the same frequency used for the modulation.

8.14 NEW: Extending the Pound-Drever-Hall technique to more complicated optical systems

To recap Section 8.8, in the Pound-Drever-Hall (PDH) or RF-reflection locking technique sinusoidal radio-frequency phase modulation is applied to the light to produce phase modulation sidebands. With phase modulation, higher order sidebands are imposed on the light, though the beats due to these are generally not employed in the normal implementation of the Pound-Drever-Hall technique. The light is then incident on the cavity that is to be controlled. The signal is obtained by detecting the reflected light on a photo-detector which has a square-law response to the light amplitude, and analysing the resulting beats. The important beats are between the carrier and the first order RF sidebands. The electronic signal from the photodiode is filtered to pass the beats in a frequency range around the modulation frequency, and multiplied or ‘mixed’ with an electronic signal at the modulation frequency: an electronic local oscillator. The output from the mixer is then low-pass filtered to remove oscillations at harmonics of the modulation frequency. The useful signal is in one quadrature of the output from the photo-detector at the modulation frequency. The phase of the local oscillator is chosen to select the required quadrature.

During the 1980s and 1990s, the question arose of how to obtain control signals for systems of coupled cavities and systems with combination of cavities in a Michelson interferometer. A good example is the power-recycled Fabry-Perot Michelson interferometer configuration as employed in initial LIGO and Virgo. In such a system, one possibility is to add pick-offs (low-reflectivity beam-splitters) to remove some of the light reflected from each arm cavity for detection. This approach introduces a conflict between efficient power recycling that requires low loss, and the generation of a low-noise control signal, which argues for more highly reflecting beam-splitters. It is of interest to identify other approaches that do not require additional detection ports. With this restriction, the problem becomes one of sensing all internal degrees of freedom by analysing light fields reflected from or transmitted by the entire interferometer. This has been accomplished for the dual-recycled Michelson topology of GEO 600 [83], for the dual-recycled Fabry-Perot Michelson configuration, e.g. Advanced LIGO – see Appendix B for a short description of the sensing scheme.

The scope of this section permits discussion only of design principles. It is worth noting, however, some practical matters that constrain the acceptable solutions. For example, the choice of modulation frequencies is usually restricted. One limit is the speed of photo-detectors, and in particular quadrant photo-detectors, for alignment sensing. This restriction makes the use of mod-

ulation frequencies above of order 100 MHz highly challenging. Another limitation results from the presence of mode-cleaning cavities in the path from the laser to the interferometer. Due to practical difficulties in the design of in-vacuum modulators, modulation is usually applied prior to the light passing the mode-cleaner. In this case the only available modulation frequencies are whole-multiples of the free-spectral-range of the mode-cleaner. Note however that in-vacuum modulation is possible, and has been applied in GEO 600 allowing a relatively free choice of modulation frequency which is important for the method of locking the dual recycled system [83].

The essence of the Pound-Drever-Hall method is that the light field is divided, according to frequency, into a component that suffers a phase change in response to variation of the target degree of freedom for measurement, and a component that does not. Therefore, a starting point in the discovery of alternatives is to create circumstances in which different light components, distinguished by frequency, resonate in different locations. Secondly, to produce a useful error signal, the output from the detection process should contain a dominant linear component in terms of its magnitude as a function of the target degree of freedom. Although it is desirable that the signal crosses zero at the operating point, it may be necessary and acceptable to subtract a (hopefully steady) offset to obtain the required result. These aspects are dealt with in turn.

First we consider how zero-crossing signals may be obtained from beats. The desired zero-crossing linear slope is achieved most directly if the components of the light are in quadrature, as is the case in Pound-Drever-Hall sensing: see sections 3.2 and 8.8. This ensures that the measurement depends on the relative phase of the optical field components, rather than their amplitudes. As an example of an alternative, quadrature is also achieved in the case of beating amplitude modulation sidebands against phase modulation sidebands.

In cases like this, where beats are obtained between various sidebands, rather than by beating with the carrier, the demodulated signal may either be obtained directly by mixing the electronic signal with a local oscillator at the beat frequency, or by employing double demodulation. A description of this process is shown in Section 4.2.

The condition for quadrature requires pairs of sidebands to be symmetrical so that they represent either pure phase modulation or pure amplitude modulation. In either of these cases, their resultant sum maintains a constant phase over time. If there is an imbalance of the amplitude of the lower and upper sidebands, the phase of the resultant must oscillate. This is equivalent to saying that the sidebands represent a mixture of amplitude and phase modulation, or equivalently, that there is an unbalanced single-sideband component. Extraction of useful error signals is still possible, but it is to be expected that there will be an offset in the demodulated signal, rather than a zero-crossing at the desired resonance condition.

Such sideband imbalance arises naturally in interferometers with detuned signal recycling, see Section 7.3. In these interferometers, the resonance of the signal recycling cavity is not centred on the carrier and so the response to upper and lower modulation sidebands can be expected to be asymmetrical. The beats produced on detection of the unbalanced sidebands may still produce a useful linear component, corresponding to the part of the amplitude that is in the appropriate quadrature.

As an example of obtaining signals from beats between sidebands, we cite the important method called *third-harmonic demodulation*, introduced and explained in detail in [11]. In brief summary, this technique exploits the natural presence of higher harmonics in phase modulation for moderate to large modulation indices, e.g. 0.8 rad in the cited work. As noted above, such harmonics are passed by a mode-cleaner that is resonant at the first harmonic, and depending on the design of the interferometer, at least some can be expected to be resonant in the power recycling cavity (the odd members of the series in the scheme described by Arai *et al.* in [11]). By combining this method of demodulation with the introduction of asymmetry in the geometry of the interferometer, as described in the following section, it is possible to construct a sensing system that provides well separated readout of the various degrees of freedom. In the cited scheme, neither the first or third

order sidebands are strongly affected by the phase of the arm cavities (when the carrier is on resonance), and the method allows relatively independent control of the other degrees of freedom.

The third harmonic demodulation approach has been extended, with results proven in a series of investigations on prototype interferometers, including a 4 m interferometer with resonant sideband enhancement [95], and experiments on the CalTech 40 m apparatus [120] as part of the development of control systems for Advanced LIGO, in which third-harmonic demodulation is employed – see Appendix B.

Next we return to the question of how sideband fields may be separated by breaking the symmetry of the interferometer. To reduce noise couplings, interferometers are usually designed and built to be as symmetrical as possible. For instance, an interferometer with perfectly matched arms is insensitive to the frequency of the light. In the design process it is usually assumed that the long arms of the interferometer must be kept as symmetrical as can be arranged in practice, but that controlled amounts of asymmetry can be introduced in the paths from the beam-splitter to the arm cavities or recycling mirrors as appropriate to facilitate the design of sensing schemes.

The methods discussed in this section stem from the Schnupp modulation technique described in Section 8.13. In the unmodified Michelson interferometer, shown in Figure 8.11, the asymmetry required to maximise the strength of the sidebands at the output, with modulation frequencies in the usual range (typically 10 to 100 MHz) is one quarter of the RF wavelength. The addition of power-recycling lowers the required asymmetry because in this case optimum transfer of sideband power occurs when the asymmetry leads to an out-coupling of equal strength to the transmission of the power recycling mirror. This is in direct analogy with the transmission of light through an equal-mirror Fabry-Perot cavity.

An example of this ‘classical’ application of Schnupp modulation is found in GEO 600. Here the approximately 1200 m (optical path) arms are adjusted to differ in length by about 10 cm, and this provides efficient transfer of ≈ 15 MHz sidebands to the output port. The approach is described in [83].

The idea of Schnupp modulation influenced the development of Advanced LIGO see, for example, [153]. It had been decided that phase modulation would be applied prior to the in-vacuum mode-cleaner, thus constraining the modulation sidebands to fall in a harmonic series. A detailed description of these methods is beyond the scope of this review, but some important features are described below.

The objective is always to cause distinct modulation sidebands to resonate in different physical regions within the interferometer. In a dual-recycling Fabry-Perot Michelson configuration, it is necessary to control the (inner) Michelson, the power recycling cavity and the signal recycling cavity. Controlling the arm cavities may be achieved by beating the carrier with suitable sidebands, the hard part of the problem is to remove the influence of arm cavities on signals for the other degrees of freedom. For control of the signal recycling cavity, for example, at least one sideband must be directed towards the signal recycling mirror. This can be accomplished by choosing a difference in the lengths of the two arms of the Michelson to arrange that one sideband is on a bright fringe, and therefore strongly directed towards the signal recycling mirror. For further detail of this aspect of interferometer sensing, see [153] and Appendix B.

One last design ingredient is that, in a ‘closed’ configuration like the dual-recycling Fabry-Perot Michelson, light travelling back from one of the arms ‘sees’ another (effective) Michelson interferometer formed by the beam-splitter and the two recycling mirrors. A variation of the Schnupp technique can also be applied in that case, by adjusting the optical paths from the beam-splitter to the recycling mirrors to be unequal. This provides further control over sideband resonance conditions in the various parts of the interferometer.

It can be appreciated that the design problem rapidly becomes too complex for a full description in this review, but all of the main principles are included, and numerical calculation allows these principles to be developed into a complete sensing scheme.

8.15 NEW: Complementary techniques: internal modulation, external modulation and dithering

For completeness we review a range of methods that have been applied in interferometry for gravitational wave detection. The ideas follow on from the basic RF heterodyne methods introduced in Section 5.4. The first RF-modulation based signal readout scheme for a Michelson interferometer involved generating the RF sidebands in phase modulators placed into the arms of the interferometer, as shown in Figure 8.12.

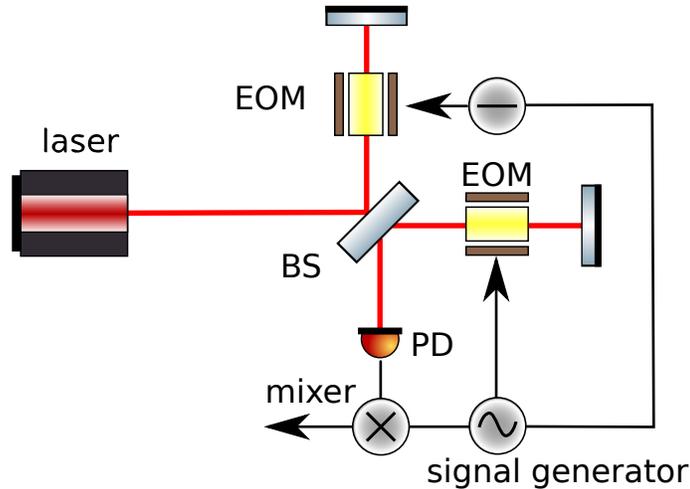


Figure 8.12: Michelson interferometer with internal modulation. Phase modulators are placed in the arms of the interferometer and driven sinusoidally in opposing phase at a radio-frequency. The strength of the modulation is chosen such that the light field at the output of the interferometer, at the dark fringe is strongly dominated by the modulation sidebands. Since the sidebands are applied differentially, they appear predominantly at the anti-symmetric port when the interferometer output is at the dark fringe for the carrier light. If, as shown here, the light passes the modulators in both directions, the position of the modulators and the frequency chosen must be taken into account to avoid unwanted cancellation or enhancement of the effect.

Although this technique, called *internal modulation* was shown to be successful in interferometry up to the late 1980s [145], it has not been possible to devise an implementation that operates with the low noise levels required for modern detectors. A related concept, dithering of interferometer mirrors to phase modulate the light within the interferometer, is described below. See also Section 3.8.2.

In the technique of *external modulation* [110], a phase modulated field is derived from the common mode light within the interferometer as shown in Figure 8.13. Light picked-off from a convenient location, usually close to the beam-splitter or even at its imperfectly anti-reflection coated rear surface, is phase modulated and recombined with the main output field, by means of a second beam-splitter. This Mach-Zehnder interferometer geometry is distinguished from general heterodyne methods in that, when power recycling is present, the modulated field is obtained from within the power recycling cavity, where the light field may be more stable than the ingoing light, due to the passive filtering provided by the power recycling cavity. External modulation adds significant complexity to the output optics of an interferometer, and is disfavoured in advanced interferometers where the application of squeezed light is considered.

Another approach to the generation of suitable signals is *dithering*, this is, effectively, the

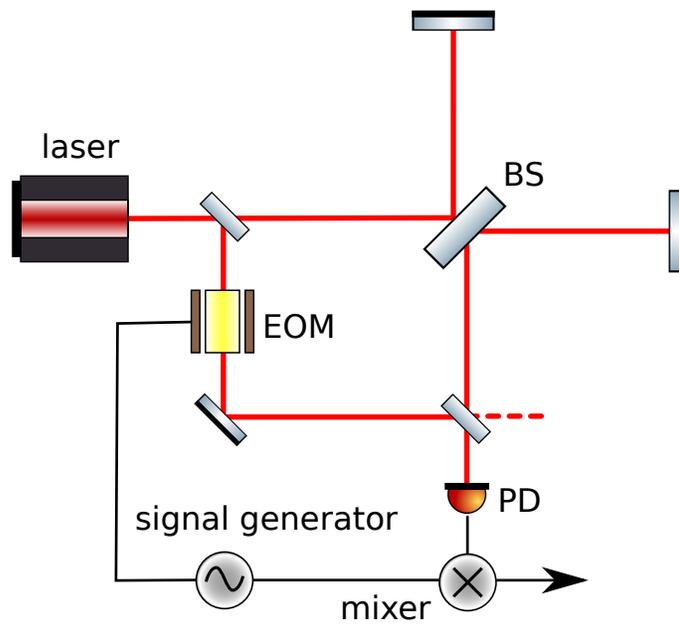


Figure 8.13: Michelson interferometer with external modulation. In this version of external modulation, a sample of the in-going light is picked off, phase modulated and recombined with the light emerging from the anti-symmetric port in a Mach-Zehnder arrangement. In an interferometer with power recycling, the light to be modulated may be extracted from within the power-recycling cavity, where the filtering action of the cavity may render it more stable. As with internal modulation, the sidebands should dominate the detected light. In that case to improve efficiency and minimise the amount of light that is extracted from the power recycling cavity, detectors may be placed at both ports of the Mach-Zehnder interferometer, and the resulting signals subtracted prior to demodulation. In the case of external modulation, the path-lengths involved are normally small compared to the RF wavelength.

application of phase modulation sidebands by modulating parameters of the system, usually the positions or angles of mirrors, rather than modulating the ingoing light. In principle, dithering could be applied at distinct frequencies to as many components of the system as there are degrees of freedom requiring to be controlled.

There are practical limitations that restrict the application of dithering, and it is normally applied to lock auxiliary degrees of freedom where the signal to noise requirements are less severe. The limitations arise because dithering is commonly applied by mechanical means, resulting in restricted actuation force (to avoid either causing damage or adding noise due from powerful actuators). This imposes a limit to the product of imposed displacement and (dither-) frequency-squared, resulting in typical dither frequencies that do not exceed a few kHz. Dithering is, therefore, typically employed to monitor and control slowly varying aspects of the interferometer. A relatively recent application of dithering is in locking an output mode-cleaner for use with DC readout. This is discussed in the following section and in [166].

8.16 NEW: Circumstances in which offset locking is favoured over modulation-based techniques

As mentioned in Sections 5.4 and 8.13, the idea of offset-locking of Michelson interferometers to produce a zero-crossing error signal for the differential displacement arises naturally. There are, however, disadvantages associated with this method of readout, and it has only become favoured over heterodyne methods due to particular circumstances that associated with recently developed interferometer designs, as explained below.

In a simple Michelson interferometer, the steepest gradient in the length to intensity transfer function occurs half-way-up the fringe. However, operating in this condition has two disadvantages: half of the light is directed back towards the laser and sensitivity to laser power fluctuations is maximised. The latter problem can be ameliorated by symmetrising the readout through the addition a photo-detector for the reflected light. On subtracting the signals from the detectors at the two ports of the interferometer, the displacement signals add while laser power fluctuations cancel, to the extent that balance is achieved. In this case, however, all the light is detected and there is no possibility to take advantage of low-loss optics by adding power recycling.

A further problem when a simple Michelson is offset-locked is that the optical local oscillator for the measurement is a relatively noisy component of the light field. Indeed this last concern led to the choice of radio frequency modulation in the Pound-Drever-Hall and other techniques described above. In those techniques modulation frequencies are chosen to fall at Fourier frequencies where technical laser noise is less than shot noise in the detected light power. This is typically true above about 10 MHz for detection of the tens of mW of light from the argon-ion or Nd:YAG lasers typically employed.

During the design of Enhanced and Advanced LIGO, Advanced Virgo and GEO-HF, three motivations emerged to prompt reconsideration of offset-locking methods. As noted in Section 3.1 it had been shown that modulation generally worsens shot-noise limited performance, and these arguments were extended to show that it is impractical to benefit from squeezed light in modulation based readout [44]. Secondly, it was realised that, for the interferometer to achieve the planned sensitivity, the light within the power recycling cavity in a system such as Advanced LIGO, must be more stable than the best available RF oscillators, at Fourier frequencies of interest, and so the arguments against employing this light for signal readout scheme become moot. Finally, whether the detected light amplitude is shot noise limited or not depends on the power that is detected, because the shot noise in the detection of small light power can make technical noise unimportant. It was realised that, by adding a mode-cleaner on the output of the interferometer, to pass the signal, which would predominantly be in the TEM₀₀ mode of the arms, but exclude other light resulting from imperfect interference, mainly in other modes, it would suffice to detect relatively

low light power, at which level the measurement should be shot noise limited. See Section 10 for a description of modes resulting from imperfect interference.

In modern detectors this scheme, where signals are read out directly in the base-band i.e. near zero frequency or ‘DC’, is often called *DC readout*. As an example of its application, the details of the DC readout scheme developed for Advanced LIGO are described in [166]. The technique has also been tested on GEO 600, where the method has been shown to be compatible with squeezing [155].

It should be noted that offset locking applies to the control of one length degree of freedom per interferometer, and the remaining degrees of freedom are typically sensed using the modulation methods described above.

8.17 Finesse examples

8.17.1 Michelson modulation

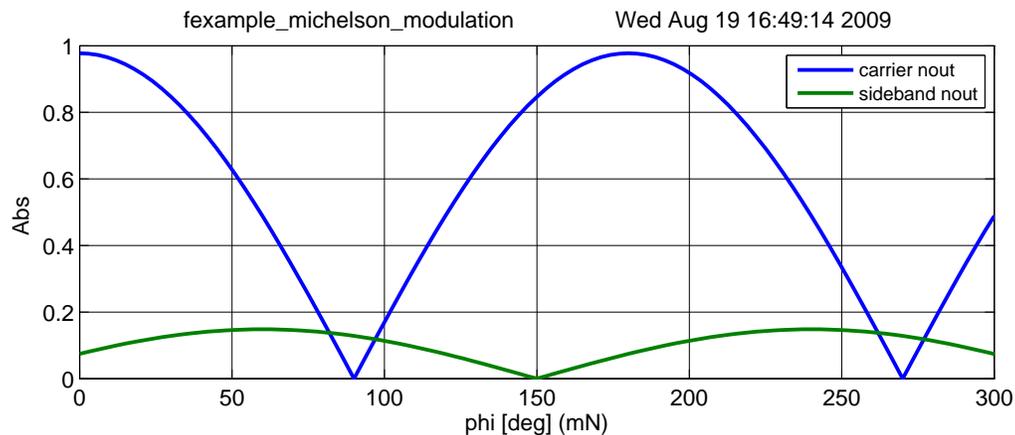


Figure 8.14: FINESSE example: Michelson modulation.

This example demonstrates how a macroscopic arm length difference can cause different ‘dark fringe’ tuning for injected fields with different frequencies. In this case, some of the 10 MHz modulation sidebands are transmitted when the interferometer is tuned to a dark fringe for the carrier light. This effect can be used to separate light fields of different frequencies. It is also the cause for transmission of laser noise (especially frequency noise) into the Michelson output port when the interferometer is not perfectly symmetric.

Finesse input file for ‘Michelson modulation’

```
laser l1 1 0 n1      % laser with P=1W at the default frequency
space s1 1 1 n1 n2  % space of 1m length
mod eom1 10M 0.3 1 pm n2 n3 % phase modulation at 10 MHz
space s2 1 1 n3 n4  % another space of 1m length
bs b1 0.5 0.5 0 0 n4 nN1 nE1 nS1 % 50:50 beam splitter
space LN 100 1 nN1 nN2 % north arm
space LE 110 1 nE1 nE2 % east arm
mirror mN 1 0 0 nN2 dump % north end mirror, lossless
mirror mE 1 0 0 nE2 dump % east end mirror, lossless
```

```

space s3 1 1 nS1 nout
ad carrier 0 nout      % amplitude detector for carrier field
ad sideband 10M nout  % amplitude detector for +10 MHz sideband
xaxis mN phi lin 0 300 100 % changing the microscopic position of mN

```

8.17.2 Cavity power and slope

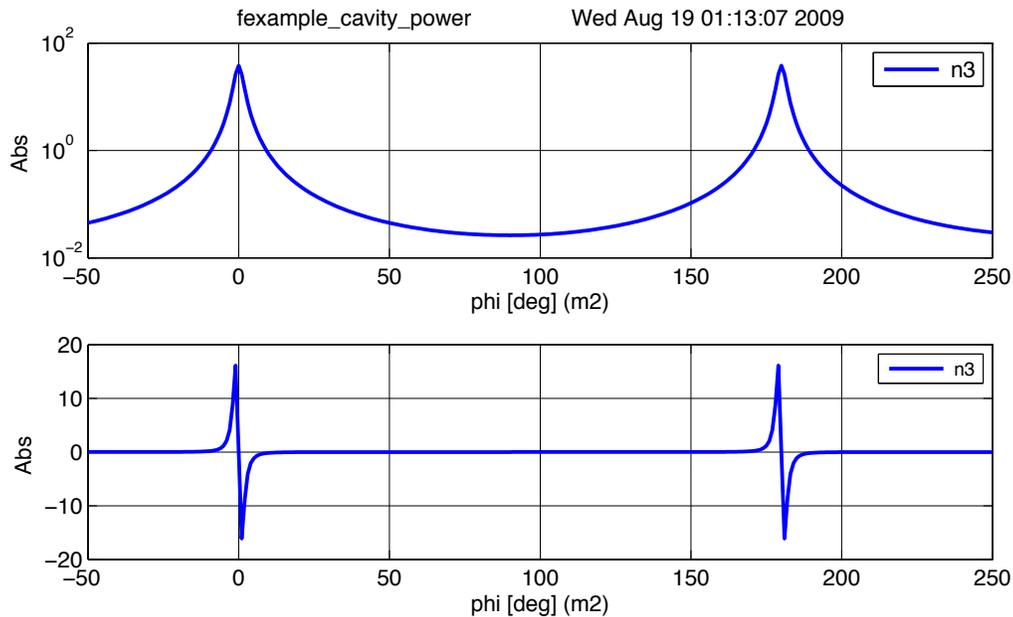


Figure 8.15: FINESSE example: Cavity power and slope.

Figure 8.15 (same as Figure 8.6) shows a plot of the analytical functions describing the power inside a cavity and its differentiation by the cavity tuning. This example recreates the plot using a numerical model in FINESSE.

Finesse input file for ‘Cavity power and slope’

```

laser l1 1 0 n1      % laser with P=1W at the default frequency
space s1 1 1 n1 n2  % space of 1m length
mirror m1 0.9 0.1 0 n2 n3 % cavity input mirror
space L 1200 1 n3 n4      % cavity length of 1200m
mirror m2 1.0 0.0 0 n4 dump % cavity output mirror
pd P n3              % photo diode measuring the intra-cavity power

% for the plot we perform two sequential runs of Finesse using ‘mkat’
% 1) first trace: plot the power (switching to log plot)
yaxis log abs
% 2) second trace: plot the differentiation
%diff m2 phi

```

```
xaxis m2 phi lin -50 250 300 % changing the microscopic tuning of mirror m2
```

8.17.3 Michelson with Schnupp modulation

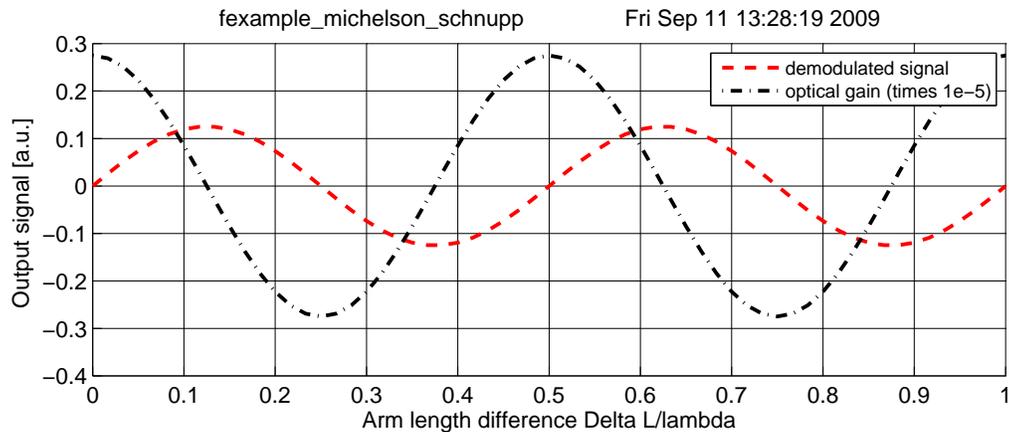


Figure 8.16: FINESSE example: Michelson with Schnupp modulation.

Figure 8.16 shows the demodulated photodiode signal of a Michelson interferometer with Schnupp modulation, as well as its differentiation, the latter being the optical gain of the system. Comparing this figure to Figure 8.9, it can be seen that with Schnupp modulation, the optical gain at the dark fringe operating points is maximised and a suitable error signal for these points is obtained.

Finesse input file for ‘Michelson with Schnupp modulation’

```
laser l1 1 0 n1 % laser with P=1W at the default frequency
space s1 1 1 n1 n2 % space of 1m length
mod eom1 10M 0.3 1 pm n2 n3 % phase modulation at 10 MHz
space s2 1 1 n3 n4 % another space of 1m length
bs b1 0.5 0.5 0 0 n4 nN1 nE1 nS1 % 50:50 beam splitter
space LN 100 1 nN1 nN2 % north arm
space LE 110 1 nE1 nE2 % east arm
mirror mN 1 0 22 nN2 dump % north end mirror, lossless
mirror mE 1 0 -22 nE2 dump % east end mirror, lossless
space s3 1 1 nS1 nout

pd1 South 10M -115 nout % demodulated output signal
% for the second (black) trace, we add differentiation
%diff mN phi % computing the slope of the signal

xaxis mN phi lin 0 300 100 % changing the microscopic position of mN
put mE phi $mx1 % moving mE as -mN to make a differential motion
```

9 Beam Shapes: Beyond the Plane Wave Approximation

In previous sections we have introduced a notation for describing the on-axis properties of electric fields. Specifically, we have described the electric fields along an optical axis as functions of frequency (or time) and the location z . Models of optical systems may often use this approach for a basic analysis even though the respective experiments will always include fields with distinct off-axis beam shapes. A more detailed description of such optical systems needs to take the geometrical shape of the light field into account. One method of treating the transverse beam geometry is to describe the spatial properties as a sum of ‘spatial components’ or ‘spatial modes’ so that the electric field can be written as a sum of the different frequency components and of the different spatial modes. Of course, the concept of modes is directly related to the use of a sort of oscillator, in this case the optical cavity. Most of the work presented here is based on the research on laser resonators reviewed originally by Kogelnik and Li [100]. Siegman has written a very interesting historic review of the development of Gaussian optics [149, 148] and we use whenever possible the same notation as used in his textbook ‘Lasers’ [147].

This section introduces the use of Gaussian modes for describing the spatial properties along the transverse orthogonal x and y directions of an optical beam. We can write

$$E(t, x, y, z) = \sum_j \sum_{n,m} a_{jnm} u_{nm}(x, y, z) \exp(i(\omega_j t - k_j z)), \quad (9.1)$$

with u_{nm} as special functions describing the spatial properties of the beam and a_{jnm} as complex amplitude factors (ω_j is again the angular frequency and $k_j = \omega_j/c$). For simplicity we restrict the following description to a single frequency component at one moment in time ($t = 0$), so

$$E(x, y, z) = \exp(-i k z) \sum_{n,m} a_{nm} u_{nm}(x, y, z). \quad (9.2)$$

In general, different types of spatial modes u_{nm} can be used in this context. Of particular interest are the *Gaussian modes*, which will be used throughout this document. Many lasers emit light that closely resembles a *Gaussian beam*: the light mainly propagates along one axis, is well collimated around that axis and the cross section of the intensity perpendicular to the optical axis shows a Gaussian distribution. The following sections provide the basic mathematical framework for using Gaussian modes for analysing optical systems.

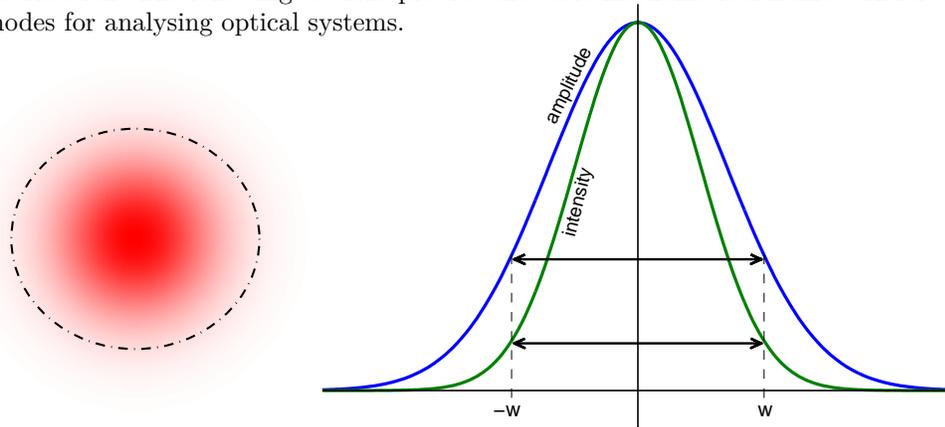


Figure 9.1: A typical laser beam intensity pattern (left) and the intensity and amplitude distributions of a normalised Gaussian beam (right). A Gaussian beam is characterised by its spot size, w , the radius at which the intensity falls to $\frac{1}{e^2}$ ($\sim 14\%$) of the peak intensity.

9.1 NEW: A typical laser beam: the fundamental Gaussian mode

The beam produced from a real laser is not a plane wave, but has some intensity distribution. This is typically a roughly circular beam with a peak brightness near the centre. The intensity pattern of a beam generated by an ideal laser based on a stable optical cavity with spherical mirrors would resemble a Gaussian beam. Figure 9.1 shows the intensity and amplitude distribution of a typical Gaussian beam, often characterised by the beam spot size, w , the radius within which $\sim 86\%$ ($\frac{1}{e^2}$) of the light power is contained. As the beam propagates the beam spot size changes slowly, which allows producing a narrow beam of light with a small diffraction angle.

The use of cavities in interferometry provides the basis for the mathematical description of laser beam shapes as Gaussian modes. A well designed cavity is a perfect optical resonator for a particular Gaussian mode. As discussed above, the intensity distribution can be characterised by the beam spot size, which determines the width of the beam. In the case of Gaussian modes the wavefront, or phase, of the light field is curved and can be expressed with a radius of curvature, R_C . As the beam propagates the curvature of the wavefront changes. To achieve perfect resonance in an optical cavity the curvature of the wavefront must match the curvature of the mirrors at their positions on the optical axis. The Gaussian beam whose curvatures match the mirrors of a cavity is known as the cavity eigenmode, see Figure 9.2.

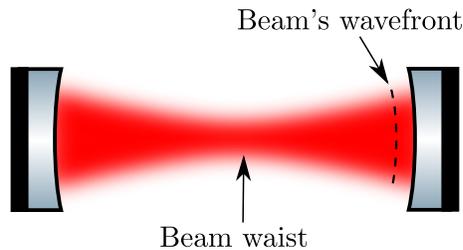


Figure 9.2: Simple depiction of a cavity eigenmode. The length and curvature of the mirrors determine the cavity eigenmode which is defined by the beam waist size and position relative to the mirrors.

9.2 NEW: Describing beam distortions with higher-order modes

In an ideal interferometer the laser beam would be a perfect Gaussian beam, with wavefronts exactly matched to the shape of the mirrors. However, in a real interferometer mismatches between the beam and mirror curvatures, misalignments from the optical axis and deviations of the mirror surfaces from a perfect sphere all contribute to distort the beam from the ideal Gaussian beam.

Small distortions of the fundamental beam can be described by the addition of *higher-order modes*. Higher-order modes have the same basic properties of the fundamental Gaussian beam, with two exceptions: higher-order modes have different intensity patterns from the simple spot of the fundamental mode and modes of different order pick up an extra phase upon propagation (the Gouy phase, see Section 9.10).

One simple example is a misaligned beam, whose centre has been shifted from the optical axis. This can be described by the addition of an order '1' Hermite-Gauss mode, HG_{10} (Section 9.7), as illustrated in the left panel of Figure 9.3. Such a distortion is a first order effect and, as long as the misalignment is small, can be described with just this one additional mode. In a similar way the second order effect such as a mismatch in beam size can be described by the addition of a single order '2' mode, in this case the Laguerre-Gauss mode LG_{10} (Section 9.11). A mismatch in beam size is illustrated in the right panel of Figure 9.3.

The following sections describe details of Gaussian modes and how any paraxial laser beam with distortions can be described by a sum of Gaussian modes.

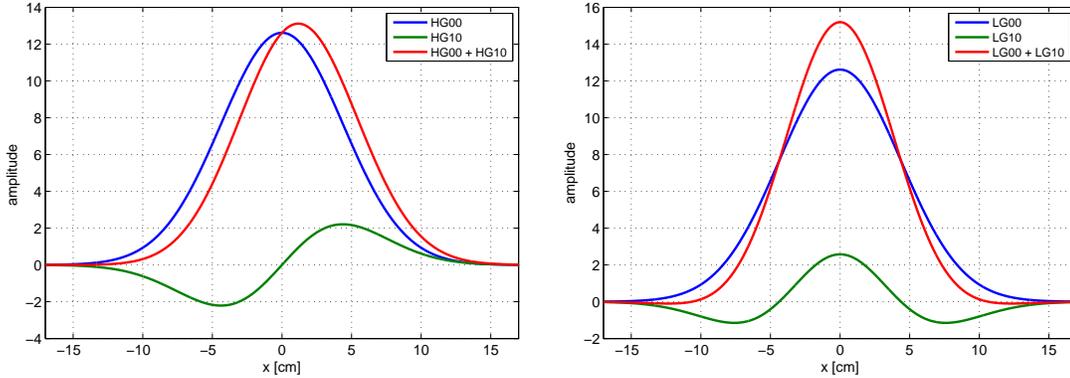


Figure 9.3: **Left:** Amplitude distributions of a fundamental gaussian beam (HG₀₀), order 1 Hermite-Gauss beam (HG₁₀) and the sum of the two modes. The resulting sum is a good description of a misaligned fundamental beam. The total power is 1 W with 4% power in the order 1 mode. **Right:** Amplitude distributions of a fundamental gaussian beam (LG₀₀), order 2 Laguerre-Gauss beam (LG₁₀) and the sum of the two modes. The resulting sum is a good description of a fundamental gaussian beam with a smaller beam spot size. The power in the order 2 mode is 4% of the total 1 W power.

9.3 The paraxial approximation

All electromagnetic waves are solutions to the general wave equation (Helmholtz equation), which in vacuum can be given as:

$$\Delta \vec{E} - \frac{1}{c^2} \ddot{\vec{E}} = 0. \quad (9.3)$$

Mathematically, Gaussian modes represent solutions to the *paraxial approximation* of this equation. Laser light fields are special class of electromagnetic waves. A laser beam will have a characteristic size w describing the ‘width’ (the dimension of the field transverse to the main propagation axis), and a characteristic length l defining some local length along the propagation over which the beam characteristics do not vary much. By definition, for what we call a *beam* w is typically small and l large in comparison, so that w/l can be considered small. In fact, the paraxial wave equation (and its solutions) can be derived as the first-order terms of a series expansion of Equation (9.3) into orders of w/l [103].

A simpler approach to the paraxial-wave equation goes as follows: A particular beam shape shall be described by a function $u(x, y, z)$ so that we can write the electric field as

$$E(x, y, z) = u(x, y, z) \exp(-ikz). \quad (9.4)$$

Substituting this into the standard wave equation yields a differential equation for u :

$$(\partial_x^2 + \partial_y^2 + \partial_z^2) u(x, y, z) - 2ik\partial_z u(x, y, z) = 0. \quad (9.5)$$

Now we put the fact that $u(x, y, z)$ should be slowly varying with z in mathematical terms. The variation of $u(x, y, z)$ with z should be small compared to its variation with x or y . Also the second partial derivative in z should be small. This can be expressed as

$$|\partial_z^2 u(x, y, z)| \ll |2k\partial_z u(x, y, z)|, |\partial_x^2 u(x, y, z)|, |\partial_y^2 u(x, y, z)|. \quad (9.6)$$

With this approximation, Equation (9.5) can be simplified to the *paraxial wave equation*,

$$(\partial_x^2 + \partial_y^2) u(x, y, z) - 2i k \partial_z u(x, y, z) = 0. \quad (9.7)$$

Any field u that solves this equation represents a paraxial beam shape when used in the form given in Equation (9.4).

9.4 Transverse electromagnetic modes

In general, any solution $u(x, y, z)$ of the paraxial wave equation, Equation (9.7), can be employed to represent the transverse properties of a scalar electric field representing a beam-like electromagnetic wave. Especially useful in this respect are special *families* or *sets* of functions that are solutions of the paraxial wave equation. When such a set of functions is complete and countable, it's called a set of *transverse electromagnetic modes* (TEM). For instance, the set of *Hermite–Gauss modes* are exact solutions of the paraxial wave equation. These modes are represented by an infinite, countable and complete set of functions. The term *complete* means they can be understood as a base system of the function space defined by *all* solutions of the paraxial wave equation. In other words, we can describe any solution of the paraxial wave equation u' by a linear superposition of Hermite–Gauss modes:

$$u'(x, y, z) = \sum_{n,m} a_{jnm} u_{nm}(x, y, z), \quad (9.8)$$

which in turn allows us to describe any laser beam using a sum of these modes:

$$E(t, x, y, z) = \sum_j \sum_{n,m} a_{jnm} u_{nm}(x, y, z) \exp(i(\omega_j t - k_j z)). \quad (9.9)$$

The Hermite–Gauss modes as given in this document (see Section 9.7) are orthonormal so that

$$\iint dx dy u_{nm} u_{n'm'}^* = \delta_{nn'} \delta_{mm'} = \begin{cases} 1 & \text{if } n = n' \text{ and } m = m' \\ 0 & \text{otherwise} \end{cases}. \quad (9.10)$$

This means that, in the function space defined by the paraxial wave equation, the Hermite–Gauss functions can be understood as a complete set of *unit-length* basis vectors. This fact can be utilised for the computation of coupling factors, as shown in Section 11.3. Furthermore, the power of a beam, as given by Equation (9.2), being detected on a single-element photodetector (provided that the area of the detector is large with respect to the beam) can be computed as

$$EE^* = \sum_{n,m} a_{nm} a_{nm}^*, \quad (9.11)$$

or for a beam with several frequency components (compare with Equation (4.9)) as

$$EE^* = \sum_{n,m} \sum_i \sum_j a_{inm} a_{jnm}^* \quad \text{with } \{i, j \mid i, j \in \{0, \dots, N\} \wedge \omega_i = \omega_j\}. \quad (9.12)$$

9.5 Properties of Gaussian beams

The basic or ‘lowest-order’ Hermite–Gauss mode is equivalent to what is usually called a *Gaussian beam* and is given by

$$u(x, y, z) = \sqrt{\frac{2}{\pi}} \frac{1}{w(z)} \exp(i\Psi(z)) \exp\left(-ik \frac{x^2 + y^2}{2R_C(z)} - \frac{x^2 + y^2}{w^2(z)}\right). \quad (9.13)$$

The parameters of this equation are explained in detail below. The shape of a Gaussian beam is quite simple: the beam has a circular cross section, and the radial intensity profile of a beam with total power P is given by

$$I(r) = \frac{2P}{\pi w^2(z)} \exp(-2r^2/w^2), \quad (9.14)$$

with w the *spot size*, defined as the *radius* at which the intensity is $1/e^2$ times the maximum intensity $I(0)$. This is a Gaussian distribution, see Figure 9.4, hence the name *Gaussian beam*.

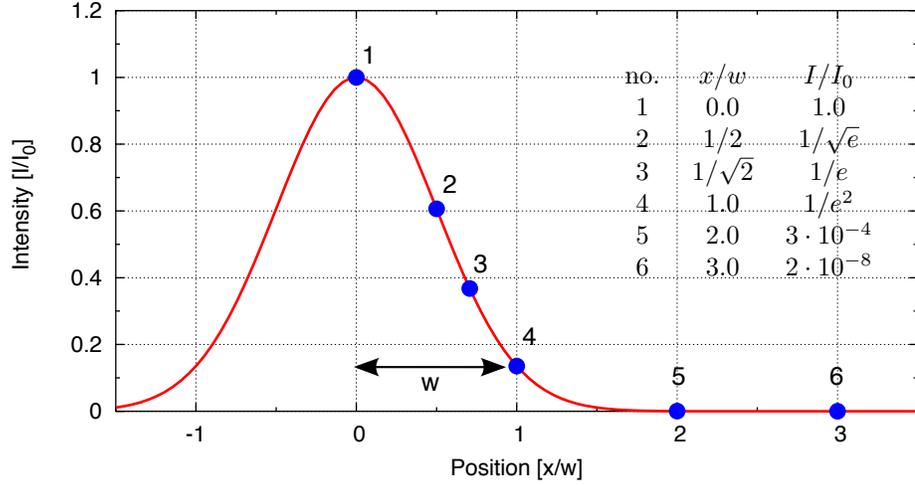


Figure 9.4: One dimensional cross-section of a Gaussian beam. The width of the beam is given by the radius w at which the intensity is $1/e^2$ of the maximum intensity.

Figure 9.5 shows a different cross section through a Gaussian beam: it plots the beam size as a function of the position on the optical axis. Such a beam profile (for a beam with a given wavelength λ) can be completely determined by two parameters: the size of the minimum spot size w_0 (called *beam waist*) and the position z_0 of the beam waist along the z -axis.

To characterise a Gaussian beam, some useful parameters can be derived from w_0 and z_0 . A Gaussian beam can be divided into two different sections along the z -axis: a *near field* – a region around the beam waist, and a *far field* – far away from the waist. The length of the near-field region is approximately given by the *Rayleigh range* z_R . The Rayleigh range and the spot size are related by

$$z_R = \frac{\pi w_0^2}{\lambda}. \quad (9.15)$$

With the Rayleigh range and the location of the beam waist, we can usefully write

$$w(z) = w_0 \sqrt{1 + \left(\frac{z - z_0}{z_R} \right)^2}. \quad (9.16)$$

This equation gives the size of the beam along the z -axis. In the far-field regime ($z \gg z_R, z_0$), it can be approximated by a linear equation, when

$$w(z) \approx w_0 \frac{z}{z_R} = \frac{z\lambda}{\pi w_0}. \quad (9.17)$$

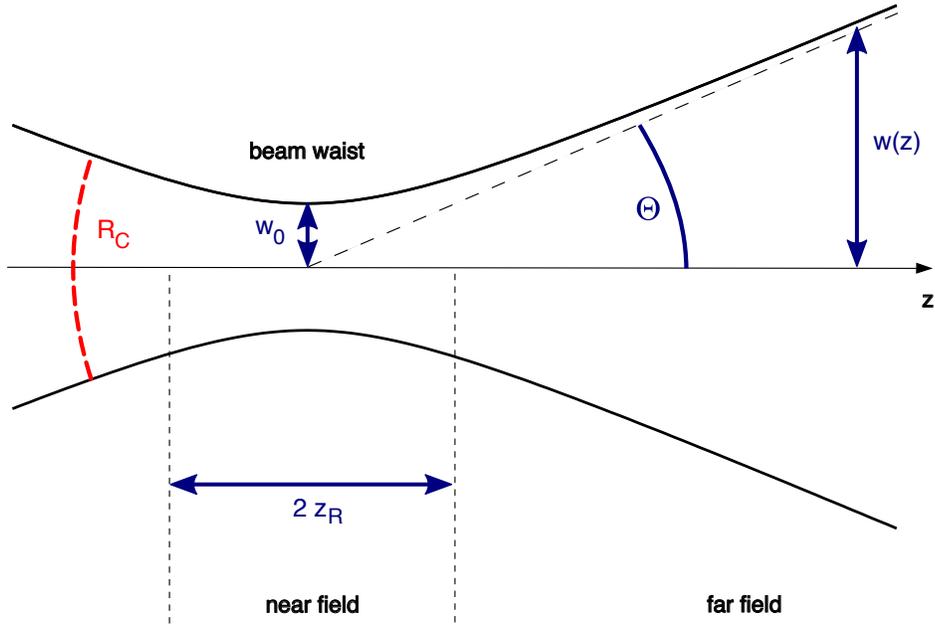


Figure 9.5: Gaussian beam profile along z : this cross section along the x - z -plane illustrates how the beam size $w(z)$ of the Gaussian beam changes along the optical axis. The position of minimum beam size w_0 is called *beam waist*. See text for a description of the parameters Θ , z_R and R_c .

The angle Θ between the z -axis and $w(z)$ in the far field is called the *diffraction angle*¹² and is defined by

$$\Theta = \arctan\left(\frac{w_0}{z_R}\right) = \arctan\left(\frac{\lambda}{\pi w_0}\right) \approx \frac{w_0}{z_R}. \quad (9.18)$$

Another useful parameter is the *radius of curvature* of the wavefront at a given point z . The radius of curvature describes the curvature of the ‘phase front’ of the electromagnetic wave – a surface across the beam with equal phase – intersecting the optical axis at the position z . We obtain the radius of curvature as a function of z :

$$R_C(z) = z - z_0 + \frac{z_R^2}{z - z_0}. \quad (9.19)$$

We also find:

$$\begin{aligned} R_C &\approx \infty, & z - z_0 &\ll z_R & \text{(beam waist)} \\ R_C &\approx z, & z &\gg z_R, z_0 & \text{(far field)} \\ R_C &= 2z_R, & z - z_0 &= z_R & \text{(maximum curvature)}. \end{aligned} \quad (9.20)$$

9.6 Astigmatic beams: the tangential and sagittal plane

If the interferometer is confined to a plane (here the x - z plane), it is convenient to use projections of the three-dimensional description into two planes [137]: the *tangential plane*, defined as the x - z plane and the *sagittal plane* as given by y and z .

¹² Also known as the *far-field angle* or the *divergence* of the beam.

The beam parameters can then be split into two respective parameters: $z_{0,s}, w_{0,s}$ for the sagittal plane and $z_{0,t}$ and $w_{0,t}$ for the tangential plane so that the Hermite–Gauss modes can be written as

$$u_{nm}(x, y) = u_n(x, z_{0,t}, w_{0,t}) u_m(y, z_{0,s}, w_{0,s}). \quad (9.21)$$

Beams with different beam waist parameters for the sagittal and tangential plane are *astigmatic*.

Remember that these Hermite–Gauss modes form a base system. This means one can use the separation into sagittal and tangential planes even if the actual optical system does not show this special type of symmetry. This separation is very useful in simplifying the mathematics. In the following, the term *beam parameter* generally refers to a simple case where $w_{0,x} = w_{0,y}$ and $z_{0,x} = z_{0,y}$ but all the results can also be applied directly to a pair of parameters.

9.7 Higher-order Hermite–Gauss modes

The complete set of Hermite–Gauss modes is given by an infinite discrete set of modes $u_{nm}(x, y, z)$ with the indices n and m as *mode numbers*. The sum $n+m$ is called the *order* of the mode. The term *higher-order modes* usually refers to modes with an order $n + m > 0$. The general expression for Hermite–Gauss modes can be given as [100]

$$u_{nm}(x, y, z) = u_n(x, z)u_m(y, z), \quad (9.22)$$

with

$$u_n(x, z) = \left(\frac{2}{\pi}\right)^{1/4} \left(\frac{\exp(i(2n+1)\Psi(z))}{2^n n! w(z)}\right)^{1/2} \times H_n\left(\frac{\sqrt{2}x}{w(z)}\right) \exp\left(-i\frac{kx^2}{2R_C(z)} - \frac{x^2}{w^2(z)}\right), \quad (9.23)$$

and $H_n(x)$ the Hermite polynomials of order n . The first Hermite polynomials, without normalisation, can be written

$$\begin{aligned} H_0(x) &= 1 & H_1(x) &= 2x \\ H_2(x) &= 4x^2 - 2 & H_3(x) &= 8x^3 - 12x. \end{aligned} \quad (9.24)$$

Further orders can be computed recursively since

$$H_{n+1}(x) = 2xH_n(x) - 2nH_{n-1}(x). \quad (9.25)$$

For both transverse directions we can also rewrite the above to

$$u_{nm}(x, y, z) = \left(2^{n+m-1} n! m! \pi\right)^{-1/2} \frac{1}{w(z)} \exp(i(n+m+1)\Psi(z)) \times H_n\left(\frac{\sqrt{2}x}{w(z)}\right) H_m\left(\frac{\sqrt{2}y}{w(z)}\right) \exp\left(-i\frac{k(x^2+y^2)}{2R_C(z)} - \frac{x^2+y^2}{w^2(z)}\right). \quad (9.26)$$

The latter form has the advantage of clearly showing the extra phase shift along the z -axis of $(n+m+1)\Psi(z)$, called the *Gouy phase*; see Section 9.10.

9.8 The Gaussian beam parameter

For a more compact description of the interaction of Gaussian modes with optical components we will make use of the *Gaussian beam parameter* q [99]. The beam parameter is a complex quantity defined as

$$\frac{1}{q(z)} = \frac{1}{R_C(z)} - i\frac{\lambda}{\pi w^2(z)}. \quad (9.27)$$

It can also be written as

$$q(z) = iz_R + z - z_0 = q_0 + z - z_0 \quad \text{and} \quad q_0 = iz_R. \quad (9.28)$$

Using this parameter, Equation (9.13) can be rewritten as

$$u(x, y, z) = \sqrt{\frac{2}{\pi}} \frac{q_0}{w_0 q(z)} \exp\left(-i k \frac{x^2 + y^2}{2q(z)}\right). \quad (9.29)$$

Other parameters, like the beam size and radius of curvature, can also be written in terms of the beam parameter q :

$$w^2(z) = \frac{\lambda}{\pi} \frac{|q|^2}{\Im\{q\}}, \quad (9.30)$$

$$w_0^2 = \frac{\Im\{q\} \lambda}{\pi}, \quad (9.31)$$

$$z_R = \Im\{q\} \quad (9.32)$$

and

$$R_C(z) = \frac{|q|^2}{\Re\{q\}}. \quad (9.33)$$

The Hermite–Gauss modes can also be written using the Gaussian beam parameter as¹³

$$u_{nm}(x, y, z) = u_n(x, z)u_m(y, z) \quad \text{with} \quad (9.34)$$

$$u_n(x, z) = \left(\frac{2}{\pi}\right)^{1/4} \left(\frac{1}{2^n n! w_0}\right)^{1/2} \left(\frac{q_0}{q(z)}\right)^{1/2} \left(\frac{q_0 q^*(z)}{q_0^* q(z)}\right)^{n/2} H_n\left(\frac{\sqrt{2}x}{w(z)}\right) \exp\left(-i \frac{kx^2}{2q(z)}\right).$$

9.9 Properties of higher-order Hermite–Gauss modes

Some of the properties of Hermite–Gauss modes can easily be described using cross sections of the field intensity or field amplitude. Figure 9.6 shows such cross sections, i.e. the intensity in the x - y plane, for a number of higher-order modes. This shows a x - y symmetry for mode indices n and m . We can also see how the size of the intensity distribution increases with the mode index, while the peak intensity decreases. Similarly, Figure 9.8 shows the amplitude and phase distribution of several higher-order Hermite–Gauss modes. Some further features of Hermite–Gauss modes:

- The size of the intensity profile of any sum of Hermite–Gauss modes depends on z while its shape remains constant over propagation along the optical axis.
- The phase distribution of Hermite–Gauss modes shows the curvature (or radius of curvature) of the beam. The curvature depends on z but is equal for all higher-order modes.

Note that these are special features of Gaussian beams and not generally true for arbitrary beam shapes. Figure 9.7, for example, shows the amplitude and phase distribution of a triangular beam at the point where it is (mathematically) created and after a 10 m propagation. Neither the shape is preserved nor does it show a spherical phase distribution.

¹³ Please note that this formula from [147] is very compact. Since the parameter q is a complex number, the expression contains at least two complex square roots. The complex square root requires a different algebra than the standard square root for real numbers. Especially the third and fourth factors can *not* be simplified in any obvious way: $\left(\frac{q_0}{q(z)}\right)^{1/2} \left(\frac{q_0 q^*(z)}{q_0^* q(z)}\right)^{n/2} \neq \left(\frac{q_0^{n+1} q^{*n}(z)}{q^{n+1}(z) q_0^{*n}}\right)^{1/2}$!

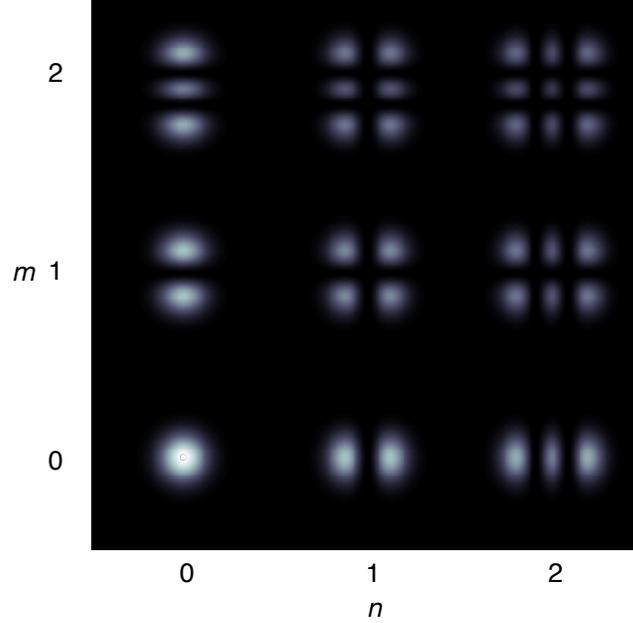


Figure 9.6: This plot shows the intensity distribution of Hermite–Gauss modes u_{nm} . One can see that the intensity distribution becomes wider for larger mode indices and the peak intensity decreases. The mode index defines the number of dark stripes in the respective direction.

9.10 Gouy phase

The equation for Hermite–Gauss modes shows an extra longitudinal phase lag. This *Gouy phase* [34, 79, 78] describes the fact that, compared to a plane wave, the Hermite–Gauss modes have a slightly slower phase velocity, especially close to the waist. The Gouy phase can be written as

$$\Psi(z) = \arctan\left(\frac{z - z_0}{z_R}\right), \quad (9.35)$$

or, using the Gaussian beam parameter,

$$\Psi(z) = \arctan\left(\frac{\Re\{q\}}{\Im\{q\}}\right). \quad (9.36)$$

Compared to a plane wave, the phase lag φ of a Hermite–Gauss mode is

$$\varphi = (n + m + 1)\Psi(z). \quad (9.37)$$

With an astigmatic beam, i.e. different beam parameters in the tangential and sagittal planes, this becomes

$$\varphi = \left(n + \frac{1}{2}\right)\Psi_t(z) + \left(m + \frac{1}{2}\right)\Psi_s(z), \quad (9.38)$$

with

$$\Psi_t(z) = \arctan\left(\frac{\Re\{q_t\}}{\Im\{q_t\}}\right), \quad (9.39)$$

as the Gouy phase in the tangential plane (and Ψ_s is similarly defined in the sagittal plane).

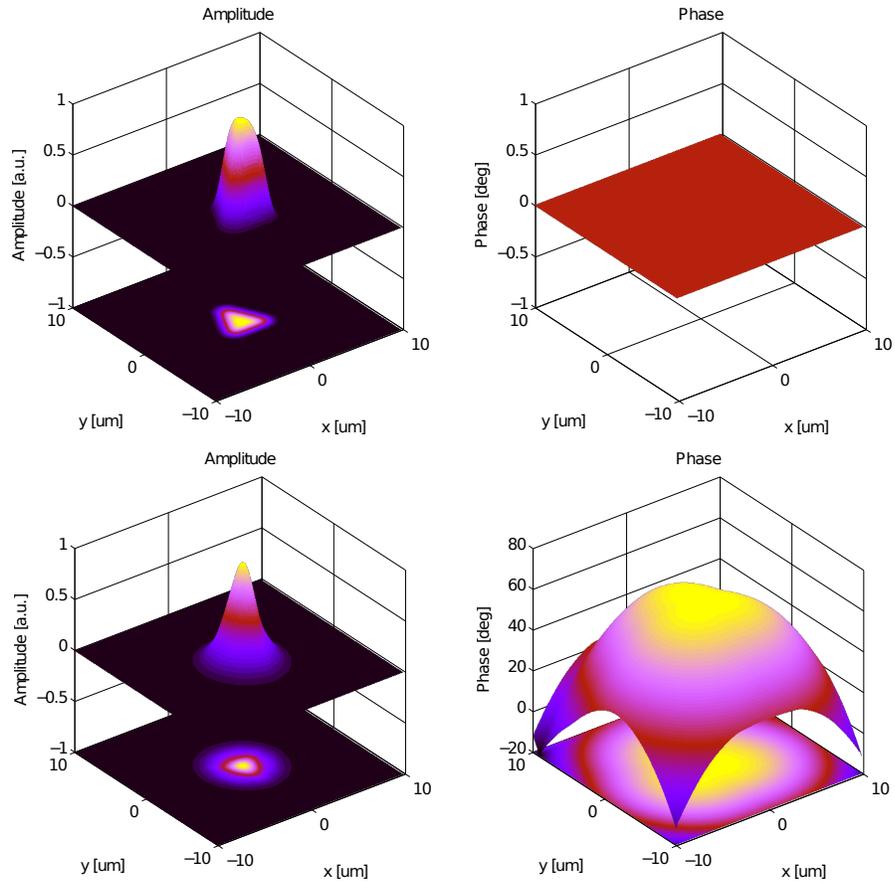


Figure 9.7: These top plots show a triangular beam shape and phase distribution and the bottom plots the diffraction pattern of this beam after a propagation of $z = 5$ m. It can be seen that the shape of the triangular beam is not conserved and that the phase front is not spherical.

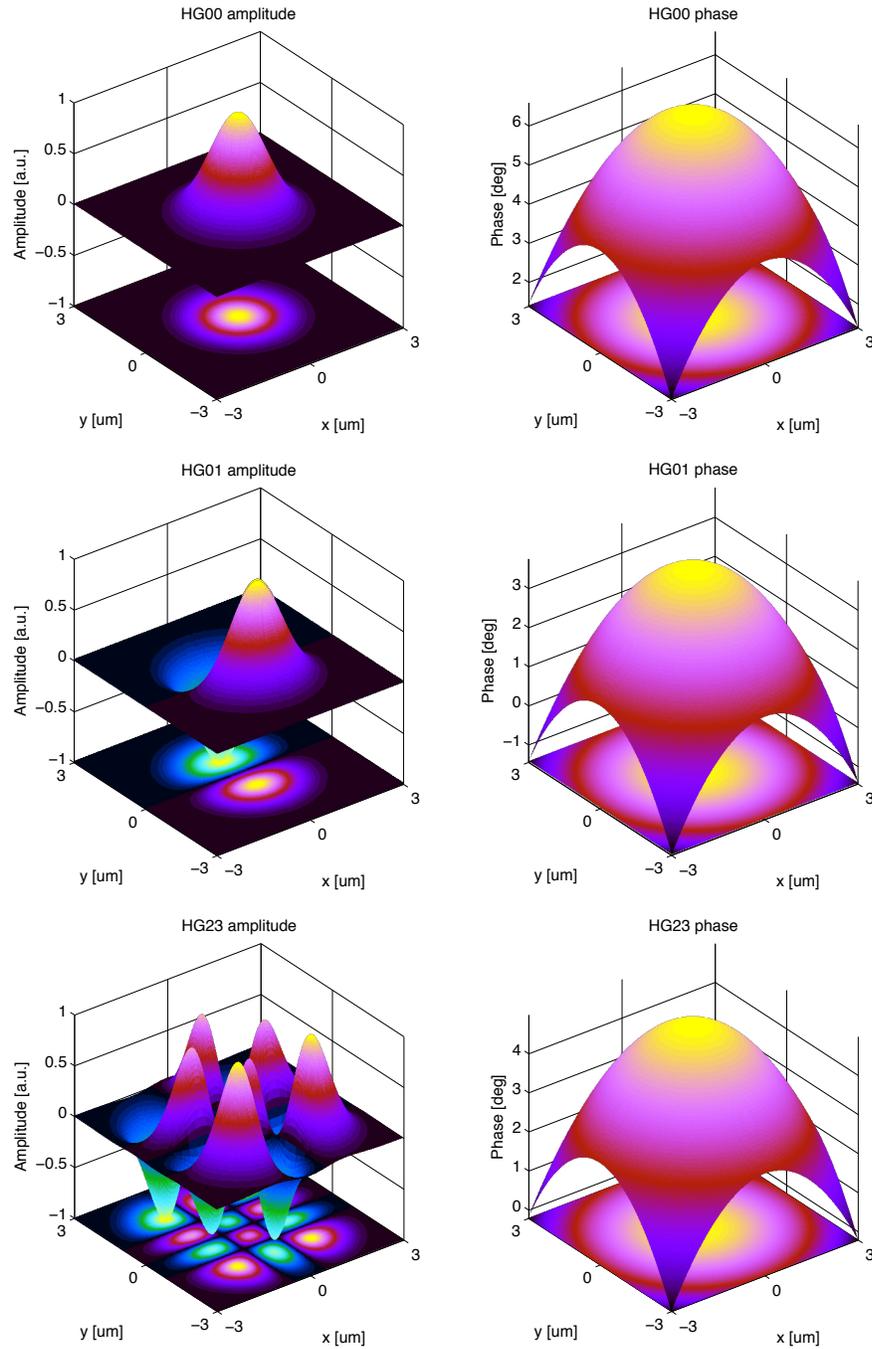


Figure 9.8: These plots show the amplitude distribution and wave front (phase distribution) of Hermite–Gaussian modes u_{nm} (labeled as HG nm in the plot). All plots refer to a beam with $\lambda = 1 \mu\text{m}$, $w = 1 \text{ mm}$ and distance to waist $z = 1 \text{ m}$. The mode index (in one direction) defines the number of zero crossings (along that axis) in the amplitude distribution. One can also see that the phase distribution is the same spherical distribution, regardless of the mode indices.

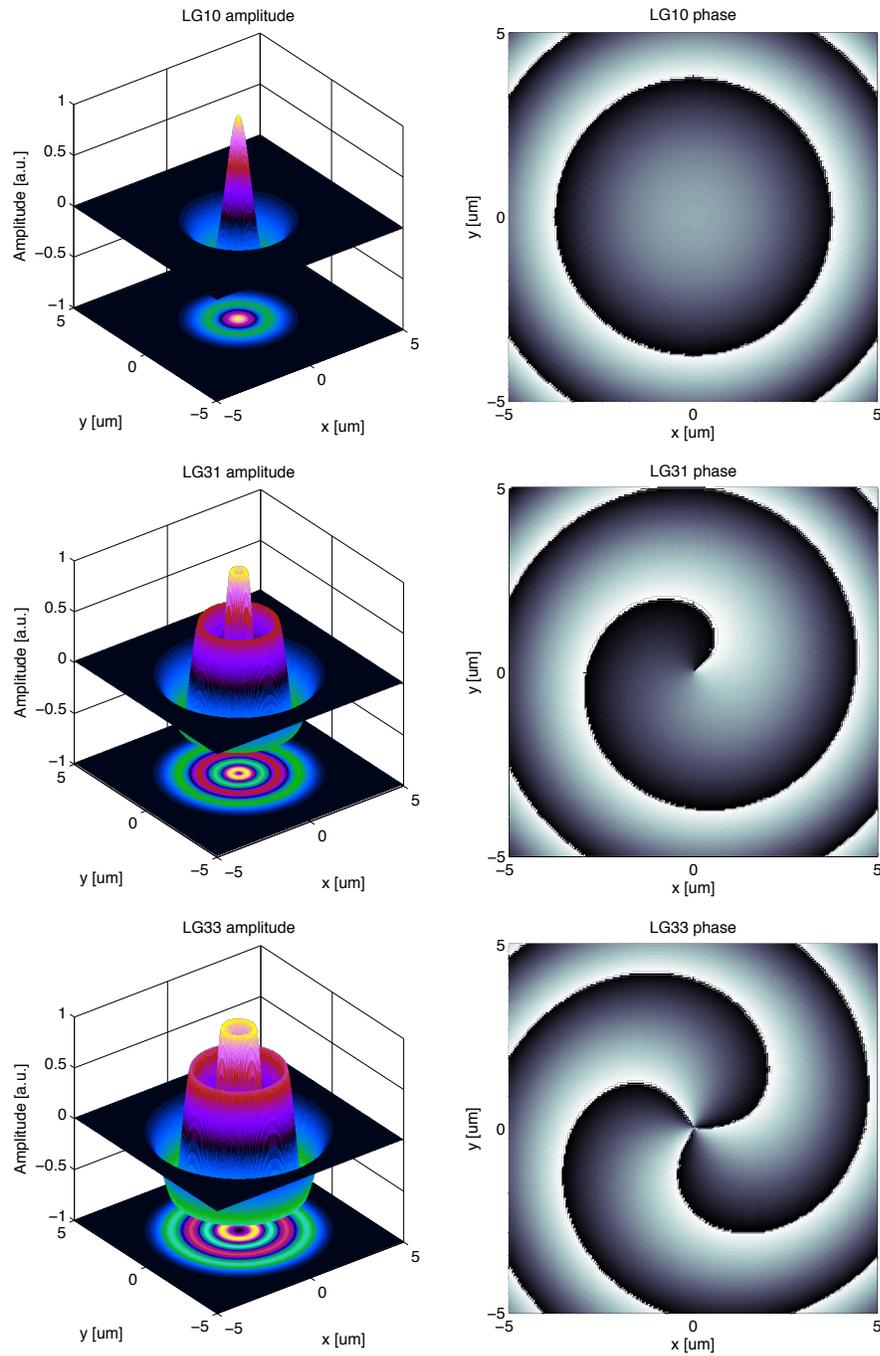


Figure 9.9: These plots show the amplitude distribution and wave front (phase distribution) of helical Laguerre-Gauss modes u_{pl} . All plots refer to a beam with $\lambda = 1 \mu\text{m}$, $w = 1 \text{ mm}$ and distance to waist $z = 1 \text{ m}$.

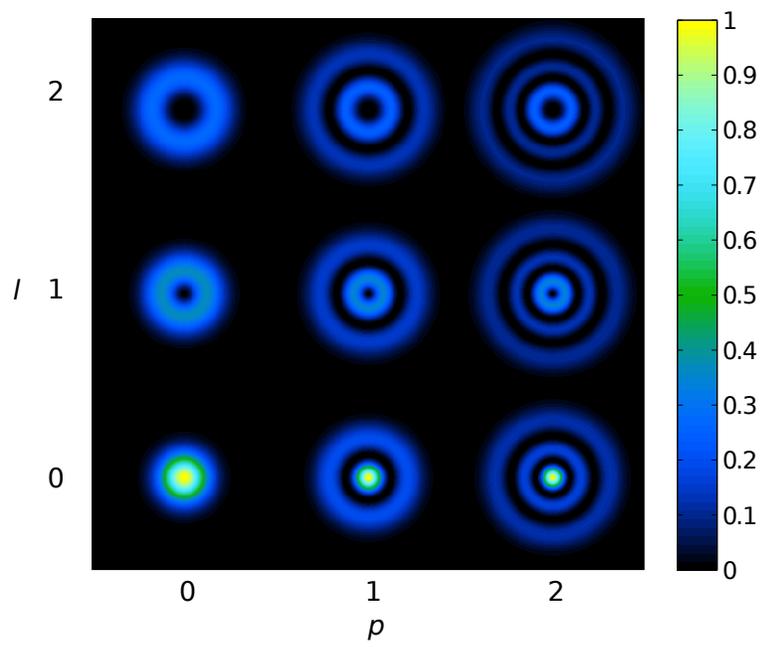


Figure 9.10: Intensity profiles for helical Laguerre-Gauss modes u_{pl} . The u_{00} mode is identical to the Hermite-Gauss mode of order 0. Higher-order modes show a widening of the intensity and decreasing peak intensity. The number of concentric dark rings is given by the radial mode index p .

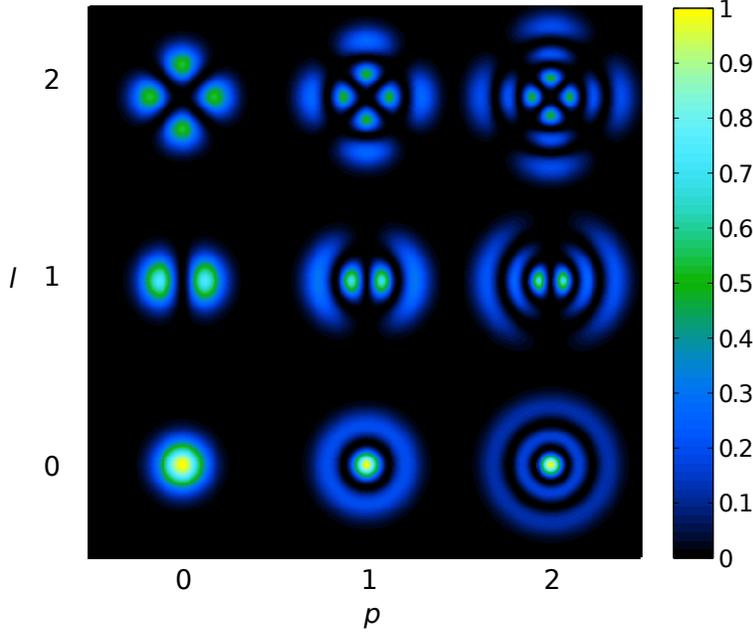


Figure 9.11: Intensity profiles for sinusoidal Laguerre–Gauss modes u_{pl}^{alt} . The u_{p0} modes are identical to the helical modes. However, for azimuthal mode indices $l > 0$ the pattern shows l dark radial lines in addition to the p dark concentric rings.

9.11 Laguerre–Gauss modes

Laguerre–Gauss modes are another complete set of functions, which solve the paraxial wave equation. They are defined in cylindrical coordinates and can have advantages over Hermite–Gauss modes in the presence of cylindrical symmetry. More recently, Laguerre–Gauss modes are being investigated in a different context: using a pure higher-order Laguerre–Gauss mode instead of the fundamental Gaussian beam can significantly reduce the impact of mirror thermal noise on the sensitivity of gravitational wave detectors [159, 49]. Laguerre–Gauss modes are commonly given as [147]

$$u_{p,l}(r, \phi, z) = \frac{1}{w(z)} \sqrt{\frac{2p!}{\pi(|l|+p)!}} \exp(i(2p + |l| + 1)\Psi(z)) \times \left(\frac{\sqrt{2}r}{w(z)}\right)^{|l|} L_p^{|l|}\left(\frac{2r^2}{w(z)^2}\right) \exp\left(-ik\frac{r^2}{2q(z)} + il\phi\right), \quad (9.40)$$

with r , ϕ and z as the cylindrical coordinates around the optical axis. The letter p is the radial mode index, l the azimuthal mode index¹⁴ and $L_p^{|l|}(x)$ are the associated Laguerre polynomials:

$$L_p^{|l|}(x) = \frac{1}{p!} \sum_{j=0}^p \frac{p!}{j!} \binom{|l|+p}{p-j} (-x)^j. \quad (9.41)$$

All other parameters ($w(z), q(z), \dots$) are defined as above for the Hermite–Gauss modes.

The dependence of the Laguerre modes on ϕ as given in Equation (9.40) results in a spiralling phase front, while the intensity pattern will always show unbroken concentric rings; see Figure 9.9.

¹⁴ [147] states that the indices must obey the following relations: $0 \leq |l| \leq p$. However, that is not the case.

These modes are also called *helical* Laguerre–Gauss modes because of their special phase structure.

The reader might be more familiar with a slightly different type of Laguerre modes (compare Figure 9.10 and Figure 9.11) that features dark radial lines as well as dark concentric rings. Mathematically, these can be described simply by replacing the phase factor $\exp(i l \phi)$ in Equation (9.40) by a sine or cosine function. For example, an alternative set of Laguerre–Gauss modes is given by [162]

$$u_{p,l}^{\text{alt}}(r, \phi, z) = \frac{2}{w(z)} \sqrt{\frac{p!}{(1+\delta_{0l}\pi(|l|+p))!}} \exp(i(2p+|l|+1)\Psi(z)) \times \left(\frac{\sqrt{2}r}{w(z)}\right)^{|l|} L_p^{|l|}\left(\frac{2r^2}{w(z)^2}\right) \exp\left(-i k \frac{r^2}{2q(z)}\right) \cos(l\phi). \quad (9.42)$$

This type of mode has a spherical phase front, just as the Hermite–Gauss modes. We will refer to this set as *sinusoidal* Laguerre–Gauss modes throughout this document.

For the purposes of simulation it can be sometimes useful to decompose Laguerre–Gauss modes into Hermite–Gauss modes. The mathematical conversion for helical modes is given as [24, 2]

$$u_{p,l}^{LG}(x, y, z) = \sum_{k=0}^N (-1)^p (\mp i)^k b(|l|+p, p, k) u_{N-k,k}^{HG}(x, y, z), \quad (9.43)$$

where \mp is negative for positive l and positive for negative l and with real coefficients

$$b(n, m, k) = \sqrt{\frac{(N-k)!k!}{2^N n!m!}} \frac{1}{k!} (\partial_t)^k [(1-t)^n (1+t)^m]_{t=0}, \quad (9.44)$$

if $N = 2p + |l|$. The coefficients $b(n, m, k)$ can be computed numerically by using Jacobi polynomials. Jacobi polynomials can be written in various forms:

$$P_n^{\alpha,\beta}(x) = \frac{(-1)^n}{2^n n!} (1-x)^{-\alpha} (1+x)^{-\beta} (\partial_x)^n (1-x)^{\alpha+n} (1+x)^{\beta+n}, \quad (9.45)$$

or

$$P_n^{\alpha,\beta}(x) = \frac{1}{2^n} \sum_{j=0}^n \binom{n+\alpha}{j} \binom{n+\beta}{n-j} (x-1)^{n-j} (x+1)^j, \quad (9.46)$$

which leads to

$$b(n, m, k) = \sqrt{\frac{(N-k)!k!}{2^N n!m!}} (-2)^k P_k^{n-k, m-k}(0). \quad (9.47)$$

9.12 Tracing a Gaussian beam through an optical system

Whenever Gauss modes are used to analyse an optical system, the Gaussian beam parameters (or equivalent waist sizes and locations) must be defined for each location at which field amplitudes are to be computed (or at which coupling equations are to be defined). In our experience the quality of a computation or simulation and the correctness of the results depend critically on the choice of these beam parameters. One might argue that the choice of a basis should not alter the result. This is correct, but there is a practical limitation: the number of modes having non-negligible power might become very large if the beam parameters are not optimised, so that in practice a good set of beam parameters is usually required.

In general, the Gaussian beam parameter of a mode is changed at every optical surface in a well-defined way (see Section 9.13). Thus, a possible method of finding reasonable beam parameters for every location in the interferometer is to first set only some specific beam parameters at selected locations and then to derive the remaining beam parameters from these initial ones: usually it is

sensible to assume that the beam at the laser source can be properly described by the (hopefully known) beam parameter of the laser's output mode. In addition, in most stable cavities the light fields should be described by using the respective cavity eigenmodes. Then, the remaining beam parameters can be computed by *tracing* the beam through the optical system. 'Trace' in this context means that a beam starting at a location with an already-known beam parameter is propagated mathematically through the optical system. At every optical element along the path the beam parameter is transformed according to the ABCD matrix of the element (see below).

9.13 ABCD matrices

The transformation of the beam parameter can be performed by the ABCD matrix-formalism [99, 147]. When a beam passes an optical element or freely propagates through space, the initial beam parameter q_1 is transformed into q_2 . This transformation can be described by four real coefficients as follows:

$$\frac{q_2}{n_2} = \frac{A \frac{q_1}{n_1} + B}{C \frac{q_1}{n_1} + D}, \quad (9.48)$$

with the coefficient matrix

$$M = \begin{pmatrix} A & B \\ C & D \end{pmatrix}, \quad (9.49)$$

n_1 being the index of refraction at the beam segment defined by q_1 , and n_2 the index of refraction at the beam segment described by q_2 . ABCD matrices for some common optical components are given below, for the sagittal and tangential plane.

Transmission through a mirror:

A mirror in this context is a single, partly-reflecting surface with an angle of incidence of 90° . The transmission is described by

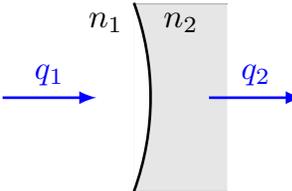
$$M = \begin{pmatrix} 1 & 0 \\ \frac{n_2 - n_1}{R_C} & 1 \end{pmatrix}$$


Figure 9.12

with R_C being the radius of curvature of the spherical surface. The sign of the radius is defined such that R_C is negative if the centre of the sphere is located in the direction of propagation. The curvature shown above (in Figure 9.12), for example, is described by a positive radius. The matrix for the transmission in the opposite direction of propagation is identical.

Reflection at a mirror:

The matrix for reflection is given by

The reflection at the back surface can be described by the same type of matrix by setting $C = 2n_2/R_C$.

$$M = \begin{pmatrix} 1 & 0 \\ -\frac{2n_1}{R_C} & 1 \end{pmatrix}$$

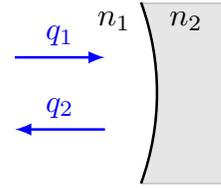


Figure 9.13

Transmission through a beam splitter:

A beam splitter is understood as a single surface with an arbitrary angle of incidence α_1 . The matrices for transmission and reflection are different for the sagittal and tangential planes (M_s and M_t):

$$M_t = \begin{pmatrix} \frac{\cos \alpha_2}{\cos \alpha_1} & 0 \\ \frac{\Delta n}{R_C} & \frac{\cos \alpha_1}{\cos \alpha_2} \end{pmatrix}$$

$$M_s = \begin{pmatrix} 1 & 0 \\ \frac{\Delta n}{R_C} & 1 \end{pmatrix}$$

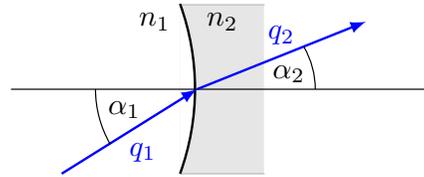


Figure 9.14

with α_2 given by Snell's law:

$$n_1 \sin(\alpha_1) = n_2 \sin(\alpha_2), \quad (9.50)$$

and Δn by

$$\Delta n = \frac{n_2 \cos(\alpha_2) - n_1 \cos(\alpha_1)}{\cos(\alpha_1) \cos(\alpha_2)}. \quad (9.51)$$

If the direction of propagation is reversed, the matrix for the sagittal plane is identical and the matrix for the tangential plane can be obtained by changing the coefficients A and D as follows:

$$\begin{aligned} A &\rightarrow 1/A, \\ D &\rightarrow 1/D. \end{aligned} \quad (9.52)$$

Reflection at a beam splitter:

The reflection at the front surface of a beam splitter is given by:

$$M_t = \begin{pmatrix} 1 & 0 \\ -\frac{2n_1}{R_C \cos \alpha_1} & 1 \end{pmatrix}$$

$$M_s = \begin{pmatrix} 1 & 0 \\ -\frac{2n_1 \cos \alpha_1}{R_C} & 1 \end{pmatrix}$$

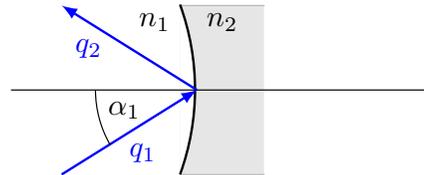


Figure 9.15

To describe a reflection at the back surface the matrices have to be changed as follows:

$$\begin{aligned} R_C &\longrightarrow -R_C, \\ n_1 &\longrightarrow n_2, \\ \alpha_1 &\longrightarrow -\alpha_2. \end{aligned} \tag{9.53}$$

Transmission through a thin lens:

A thin lens transforms the beam parameter as follows:

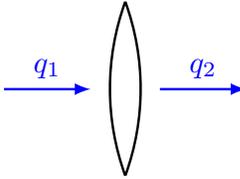
$$M = \begin{pmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{pmatrix}$$


Figure 9.16

where f is the focal length. The matrix for the opposite direction of propagation is identical. Here it is assumed that the thin lens is surrounded by ‘spaces’ with index of refraction $n = 1$.

Transmission through a free space:

As mentioned above, the beam in free space can be described by one base parameter q_0 . In some cases it is convenient to use a matrix similar to that used for the other components to describe the z -dependency of $q(z) = q_0 + z$. On propagation through a free space of the length L and index of refraction n , the beam parameter is transformed as follows.

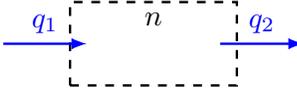
$$M = \begin{pmatrix} 1 & \frac{L}{n} \\ 0 & 1 \end{pmatrix}$$


Figure 9.17

The matrix for the opposite direction of propagation is identical.

9.14 NEW: Computing a cavity eigenmode and stability

We refer to cavity eigenmodes and stable resonators elsewhere in this article. Chapter 21 of [147] provides a comprehensive description of optical resonators including a derivation and discussion of stability criteria. Here we provide a brief introduction focussing on the specific case of the closed and stable resonators with spherical mirrors.

A cavity eigenmode is defined as the optical field whose spatial properties are such that the field after one round-trip through the cavity will be exactly the same as the injected field. In the case of resonators with spherical mirrors, the eigenmode will be a Gaussian mode, defined by the Gaussian beam parameter q_{cav} . For any generic cavity (an arbitrary number of spherical mirrors or lenses) a round-trip ABCD matrix M_{rt} can be defined. The change of the q parameter upon one round trip through the cavity is given by:

$$\frac{Aq_1 + B}{Cq_1 + D} = q_2 = q_1 \tag{9.54}$$

If $q_1 = q_2$ then the spatial profile of the beam is recreated after each round-trip and we have identified the cavity eigenmode. We can compute the parameter q_{cav} by solving:

$$Cq_{\text{cav}}^2 + (D - A)q_{\text{cav}} - B = 0, \quad (9.55)$$

For example, in the case of the two-mirror cavity shown in Figure 9.18 the matrix is given by:

$$M_{\text{rt}} = M_{\text{space}}(L) \times M_{\text{refl}}(R_2) \times M_{\text{space}}(L) \times M_{\text{refl}}(R_1), \quad (9.56)$$

with L the length of the cavity, and $R_{1/2}$ the radii of curvature of the mirrors. Now we can compute the A, B, C and D coefficients for the round-trip matrix M_{rt} to solve Equation 9.55. This quadratic equation generally has two solutions, one being the complex conjugate of the other.

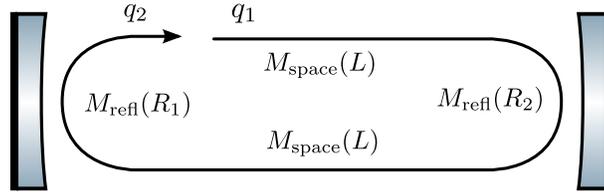


Figure 9.18: Cavity round trip ABCD matrices for a 2-mirror cavity

When the polynomial above has a suitable solution the optical resonator is said to be ‘stable’. The stability requirement can be formulated using the Gaussian beam parameter: a cavity is stable only when the cavity’s eigenmode, q_{cav} , has a real waist size. The value for the beam waist is a real number whenever q_{cav} has a positive non-zero imaginary part, as this defines the Rayleigh range of the beam and therefore the beam waist, $\text{Im}(q_{\text{cav}}) = \pi w_0^2/\lambda$. A complex q_{cav} is ensured if the determinant of equation 9.55 is negative. This requirement can be formulated in a compact way by defining the parameter m as:

$$m \equiv \frac{A + D}{2}, \quad (9.57)$$

where A and D are the coefficients of the round-trip matrix M_{rt} . The stability criterion then simply becomes:

$$m^2 < 1. \quad (9.58)$$

The stability of simple cavities are often described using g -factors. These factors are simply rescaled versions of the more generic m value:

$$g \equiv \frac{m + 1}{2} = \frac{A + D + 2}{4}, \quad (9.59)$$

For the cavity to be stable the g -factor must fulfil the requirement:

$$0 \leq g \leq 1 \quad (9.60)$$

The closer g is to the 0 or 1, the smaller the tolerances are for any change in the geometry before the cavity becomes unstable.

For a simple two-mirror cavity of length L and mirror radii of curvature $R_{1,2}$, its g -factor is

$$g_1 = 1 - \frac{L}{R_1}, \quad (9.61)$$

$$g_2 = 1 - \frac{L}{R_2}, \quad (9.62)$$

$$g = g_1 g_2. \quad (9.63)$$

Where $g_{1,2}$ are the individual g -factors of the cavity mirrors and g is the g -factor of the entire cavity.

9.15 NEW: Round-trip Gouy phase and higher-order-mode separation

As discussed in section 9.10, as a higher order optical mode propagates it accumulates an additional phase, the Gouy phase, proportional to its mode order. To determine how such a mode resonates within an optical cavity the accumulated Gouy phase on one round-trip through the cavity must be included. The round-trip Gouy phase will determine which order of optical modes are resonant within a cavity. As the resonance condition of a mode is dependent on its order, this allows an optical setup to select particular orders of optical modes from an incident field. This behaviour is the basis of *mode-cleaner* cavities; such as those used for the input and output light of gravitational wave detectors.

To compute the round-trip Gouy phase the evolution of the beam shape through the cavity must first be computed. This involves computing the round-trip ABCD matrix, M_{RT} , as outlined in section 9.14. With this matrix the round-trip Gouy phase is computed using its elements [10]:

$$\psi_{\text{RT}} = 2\arccos\left(\text{sign}(\text{B})\sqrt{\frac{\text{A} + \text{D} + 2}{4}}\right), \quad (9.64)$$

$$\psi_{\text{RT}}(g) = 2\arccos(\text{sign}(\text{B})\sqrt{g}). \quad (9.65)$$

As can be seen, the round-trip Gouy phase is linked to the cavity's g -factor, (9.59). As the cavity approaches instability, $g \rightarrow 0$ or 1 , the phase accumulated by a mode TEM_{nm} is then $(n+m)\psi_{\text{RT}}(0) = (n+m)\pi/2$ or $(n+m)\psi_{\text{RT}}(1) = 0$. In the later case all higher order optical modes—regardless of their mode order—are resonant in the cavity at the same time. In the former case either the odd or even mode orders are resonant at once.

The effect of the round-trip Gouy phase has is often referred to *higher order mode separation frequency*. This states how far the resonance of the next optical order is in frequency:

$$\delta f = \frac{\psi_{\text{RT}}}{2\pi} \text{FSR}. \quad (9.66)$$

For example, the Advanced LIGO arm cavity's have $\delta f \approx 5$ kHz.

9.16 NEW: Coupling of higher-order-modes

Now that we are able to compute the eigenmode of a particular cavity, what happens if a beam with a slightly different eigenmode is injected into it? The aim of this section is to outline the problem. In reality producing a perfect Gaussian laser which matches exactly the eigenmode of a cavity is essentially impossible, there will always be a minor difference. However we are still able to inject lasers into a cavity and produce a resonance. This is because as long as the eigenmode of the incoming laser is nearly the same, the majority of the laser light will 'fit' into the cavity and resonate, the rest will be reflected from it.

Let us consider a cavity whose eigenmode is given by q_2 and the eigenmode of a Gaussian beam that is incident on it, q_1 . The incident beam has all of its power in the fundamental 00 mode. For a cavity with perfectly spherical mirrors there are two possible 'misconfigurations' that can take place:

- If the optical axes of the beam and the cavity do not overlap perfectly, the setup is called *misaligned*,

- If the beam size or shape at cavity input does not match the beam shape and size of the (resonant) fundamental eigenmode ($q_1(z_{\text{cav}}) \neq q_2(z_{\text{cav}})$), the beam is then not *mode-matched* to the second cavity, i.e. there is a *mode mismatch*.

The coupling of a mode refers to how a spatial mode in one basis is represented in another; e.g. which sum of modes in the cavity basis q_2 produces the HG_{00} mode in the q_1 basis. Hermite–Gauss modes are coupled whenever a beam is not matched or aligned to a cavity or beam segment. This coupling is sometimes referred to as *scattering* into higher-order modes because in most cases the laser beam is considered as a pure HG_{00} mode and any mode coupling would transfer power from the fundamental into higher-order modes. However, in general every mode with non-zero power will transfer energy into other modes whenever mismatch or misalignment occur, and this effect also includes the transfer from higher orders into a low order.

To compute the amount of coupling the beam must be projected into the base system of the cavity or beam segment it is being injected into. This is always possible, provided that the paraxial approximation holds, because each set of Hermite–Gauss modes, defined by the beam parameter at a position z , forms a complete set. Such a change of the basis system results in a different distribution of light power in the new Hermite–Gauss modes and can be expressed by coupling coefficients that yield the change in the light amplitude and phase with respect to mode number.

Let us assume that a beam described by the beam parameter q_1 is injected into a segment described by the parameter q_2 . Let the optical axis of the beam be misaligned: the coordinate system of the beam is given by (x, y, z) and the beam travels along the z -axis. The beam segment is parallel to the z' -axis and the coordinate system (x', y', z') is given by rotating the (x, y, z) system around the y -axis by the *misalignment angle* γ . The amplitude of a particular mode TEM_{nm} in the beam segment is then defined as:

$$u_{nm}(x, y; q_2) \exp(i(\omega t - kz)) = \sum_{n', m'} k_{n, m, n', m'} u_{n' m'}(x, y; q_1) \exp(i(\omega t - kz')), \quad (9.67)$$

where $u_{n' m'}(x, y; q_1)$ are the Hermite–Gauss modes used to describe the injected beam, $u_{nm}(x, y; q_2)$ are the ‘new’ modes that are used to describe the light in the beam segment and $k_{n, m, n', m'}$ is the *coupling coefficient* from each $\text{TEM}_{n' m'}$ into TEM_{nm} . Note that including the plane wave phase propagation within the definition of coupling coefficients is important because it results in coupling coefficients that are independent of the position on the optical axis for which the coupling coefficients are computed.

Using the fact that the Hermite–Gauss modes u_{nm} are orthonormal, we can compute the coupling coefficients by the overlap integral [23]:

$$k_{n, m, n', m'} = \exp\left(i 2kz' \sin^2\left(\frac{\gamma}{2}\right)\right) \iint dx' dy' u_{n' m'} \exp(ikx' \sin \gamma) u_{nm}^*. \quad (9.68)$$

Since the Hermite–Gauss modes can be separated with respect to x and y , the coupling coefficients can also be split into $k_{nmn' m'} = k_{nn'} k_{mm'}$. These equations are very useful in the paraxial approximation as the coupling coefficients decrease with large mode numbers. In order to be described as paraxial, the angle γ must not be larger than the diffraction angle. In addition, to obtain correct results with a finite number of modes the beam parameters q_1 and q_2 must not differ too much.

The integral 9.68 can be computed directly using numerical integration methods. However, this can potentially be computationally very expensive depending on how difficult the integrand is to evaluate and complex it is. The following part of this section is based on the work of Bayer-Helms [23] and provides an analytic solution to the integral. Another description of coupling coefficients and their derivation can be found in the work of Vinet [162]. In [23] the above integral

is partly solved and the coupling coefficients are given by multiple sums as functions of γ and the mode mismatch parameter K , which is defined by

$$K = \frac{1}{2}(K_0 + i K_2), \quad (9.69)$$

where $K_0 = (z_R - z'_R)/z'_R$ and $K_2 = ((z - z_0) - (z' - z'_0))/z'_R$. This can also be written using $q = i z_R + z - z_0$, as

$$K = \frac{i(q - q')^*}{2\Im\{q'\}}. \quad (9.70)$$

The coupling coefficients for misalignment and mismatch (but no lateral displacement) can then be written as

$$k_{nn'} = (-1)^{n'} E^{(x)} (n!n'!)^{1/2} (1 + K_0)^{n/2+1/4} (1 + K^*)^{-(n+n'+1)/2} \{S_g - S_u\}, \quad (9.71)$$

where

$$S_g = \sum_{\mu=0}^{[n/2]} \sum_{\mu'=0}^{[n'/2]} \frac{(-1)^\mu \bar{X}^{n-2\mu} X^{n'-2\mu'}}{(n-2\mu)!(n'-2\mu')!} \sum_{\sigma=0}^{\min(\mu, \mu')} \frac{(-1)^\sigma \bar{F}^{\mu-\sigma} F^{\mu'-\sigma}}{(2\sigma)!(\mu-\sigma)!(\mu'-\sigma)!}, \quad (9.72)$$

$$S_u = \sum_{\mu=0}^{[(n-1)/2]} \sum_{\mu'=0}^{[(n'-1)/2]} \frac{(-1)^\mu \bar{X}^{n-2\mu-1} X^{n'-2\mu'-1}}{(n-2\mu-1)!(n'-2\mu'-1)!} \sum_{\sigma=0}^{\min(\mu, \mu')} \frac{(-1)^\sigma \bar{F}^{\mu-\sigma} F^{\mu'-\sigma}}{(2\sigma+1)!(\mu-\sigma)!(\mu'-\sigma)!}.$$

The corresponding formula for $k_{mm'}$ can be obtained by replacing the following parameters: $n \rightarrow m$, $n' \rightarrow m'$, $X, \bar{X} \rightarrow 0$ and $E^{(x)} \rightarrow 1$ (see below). The notation $[n/2]$ means

$$\left[\frac{m}{2} \right] = \begin{cases} m/2 & \text{if } m \text{ is even,} \\ (m-1)/2 & \text{if } m \text{ is odd.} \end{cases} \quad (9.73)$$

The other abbreviations used in the above definition are

$$\begin{aligned} \bar{X} &= (i z'_R - z') \sin(\gamma) / (\sqrt{1 + K^*} w_0), \\ X &= (i z_R + z') \sin(\gamma) / (\sqrt{1 + K^*} w_0), \\ F &= K / (2(1 + K_0)), \\ \bar{F} &= K^* / 2, \\ E^{(x)} &= \exp\left(-\frac{X\bar{X}}{2}\right). \end{aligned} \quad (9.74)$$

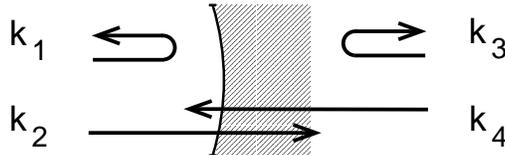


Figure 9.19: Coupling coefficients for Hermite–Gauss modes: for each optical element and each direction of propagation complex coefficients k for transmission and reflection have to be computed. In this figure k_1, k_2, k_3, k_4 each represent a matrix of coefficients $k_{nmm'n'}$ describing the coupling of $u_{n,m}$ into $u_{n',m'}$.

In general, the Gaussian beam parameter might be different for the sagittal and tangential planes and a misalignment can be given for both possible axes (around the y -axis and around the x -axis), in this case the coupling coefficients are given by

$$k_{nmm'n'} = k_{nn'}k_{mm'}, \quad (9.75)$$

where $k_{nn'}$ is given above with

$$\begin{aligned} q &\rightarrow q_t \\ \text{and} & \\ w_0 &\rightarrow w_{t,0}, \text{ etc.} \end{aligned} \quad (9.76)$$

and $\gamma \rightarrow \gamma_y$ is a rotation about the y -axis. The $k_{mm'}$ can be obtained with the same formula, with the following substitutions:

$$\begin{aligned} n &\rightarrow m, \\ n' &\rightarrow m', \\ q &\rightarrow q_s, \\ \text{thus} & \\ w_0 &\rightarrow w_{s,0}, \text{ etc.} \end{aligned} \quad (9.77)$$

and $\gamma \rightarrow \gamma_x$ is a rotation about the x -axis. At each component a matrix of coupling coefficients has to be computed for every time a beam transfers from one eigenmode to another for transmission and reflection as depicted in Figure 9.19.

In this section we have outlined how an incoming higher-order-mode will be coupled into an outgoing beam basis when taking into account a difference in the eigenmode of two sections of the interferometer or misalignments. This coupling of higher-order-modes is a very powerful tool that is used throughout this article, as it allows us to model interferometers with realistic defects; like imperfect mirror surfaces or misaligned optics. This enables us to better understand the reasons why complex interferometers behave in certain ways and provide solutions to combat particular problems that might arise. The next section details how misalignments and mode-mismatching affect the dual-recycled Fabry-Perot Michelson interferometers that were described in Section 7. Then Section 11 lays out the theory behind a more general form of scattering HOMs undergo when they interact with surface defects present on mirrors or beamsplitters.

9.17 Finesse examples

9.17.1 Beam parameter tracing

This example illustrates a possible use of the beam parameter detector ‘bp’: the beam radius of the laser beam is plotted as a function of distance to the laser. For this simulation, the interferometer matrix does not need to be solved. ‘bp’ merely returns the results from the beam tracing algorithm of FINESSE.

Finesse input file for ‘Beam parameter tracing’

```
laser i1 1 0 n1          % laser with P=1W
gauss g1 i1 n1 1m -2    % a dummy beam parameter
maxtem 0                % we need only the u_00 mode
s s1 1 n1 n2           % a space of 1m length
bp width x w n2        % detecting the beam width (horizontal)
xaxis s1 L lin 0.1 8 200 % tuning the length of s1
```

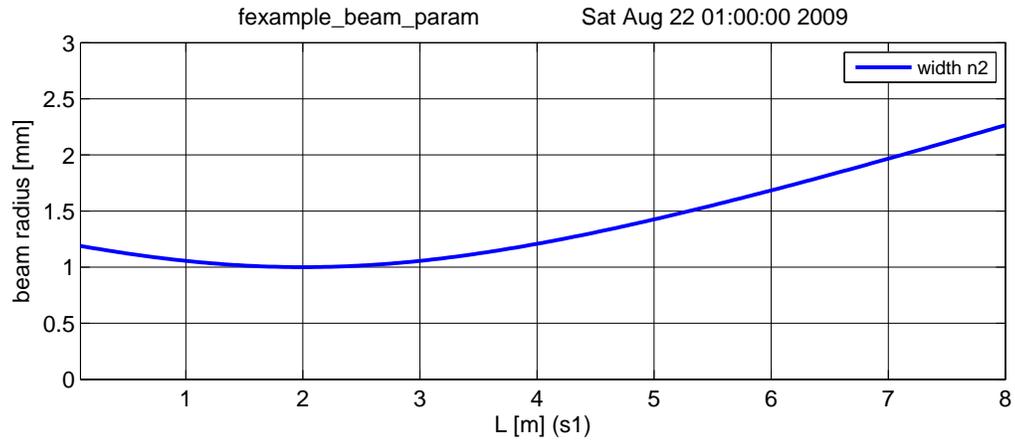


Figure 9.20: FINESSE example: Beam parameter tracing

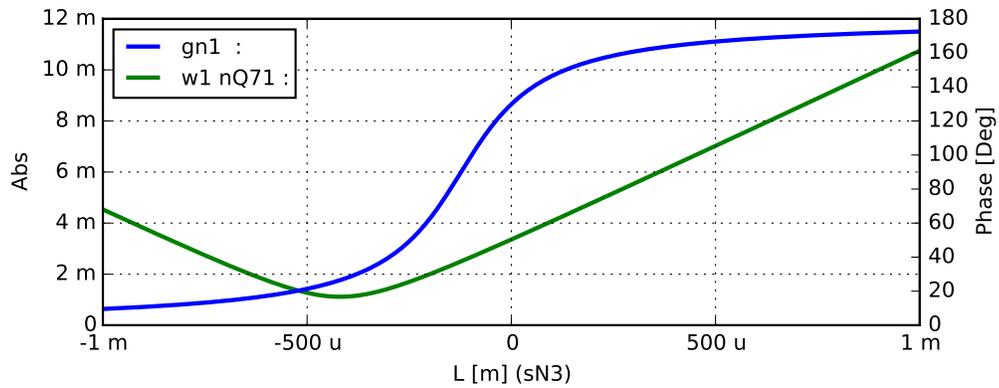


Figure 9.21: FINESSE example: Telescope and Gouy phase. The blue trace shows the Gouy phase accumulated in the telescope, the green trace the beam spot size at the end of the telescope. The change on the x axis represents a position tuning of the lens 'L2'.

9.17.2 NEW: Telescope and Gouy phase

This example shows the fine tuning of a telescope. The optical setup is similar to the optical layout on the Virgo north end detection bench, resembling the telescope for the beam transmitted by the end mirror of one arm. The purpose of the telescope is to reduce the beam size and provide a user defined Gouy phase for a split photo detector which is used for the alignment sensing system.

Finesse input file for ‘Telescope and Gouy phase’

```
l i1 6 0 0 nin
gauss g1 i1 nin 0.014852735 -2.2462888k
# multi-lens telescope, similar to the Virgo north end detction
s sN2 1.77 nin nL1
lens L1 1.02 nL1 nL2
s sN3 .8996 nL2 nL3
lens L2 -.2 nL3 nL4
s sN4 .2146 nL4 nL5
lens L3 -.1 nL5 nL6
s sN5 .608 nL6 nL12
lens L4a -.1 nL12 nL13
s sN8 .759 nL13 nQ71
# Plot Gouy phase from through the entire telescope
gouy gn1 x sN2 sN3 sN4 sN5
# Plot beam size at end of telescope
bp w1 x w nQ71
# Tuning the position of lens L2 by chaning the lengths of
# the spaces in front and behind the lens.
xaxis* sN3 L lin -1m 1m 400
func sN4L = 1.1142 - $x1
noplots sN4L
put sN4 L $sN4L
```

9.17.3 LG33 mode

FINESSE uses the Hermite–Gauss modes as a base system for describing the spatial properties of laser beams. However, Laguerre–Gauss modes can be created using the coefficients given in Equation (9.43). This example demonstrates this and the use of a ‘beam’ detector to plot amplitude and phase of a beam cross section.

Finesse input file for ‘LG33 mode’

```
laser i1 1 0 n1 % laser with P=1W
gauss g1 i1 n1 1m 0 % a dummy beam parameter
maxtem 9 % we need modes up to n+m=9
tem i1 0 0 0 0 % HG coefficients to create LG33 mode
tem i1 9 0 0.164063 0
tem i1 8 1 0.164063 -90
tem i1 7 2 0 0
tem i1 6 3 0.125 -90
tem i1 5 4 0.046875 180
tem i1 4 5 0.046875 -90
```

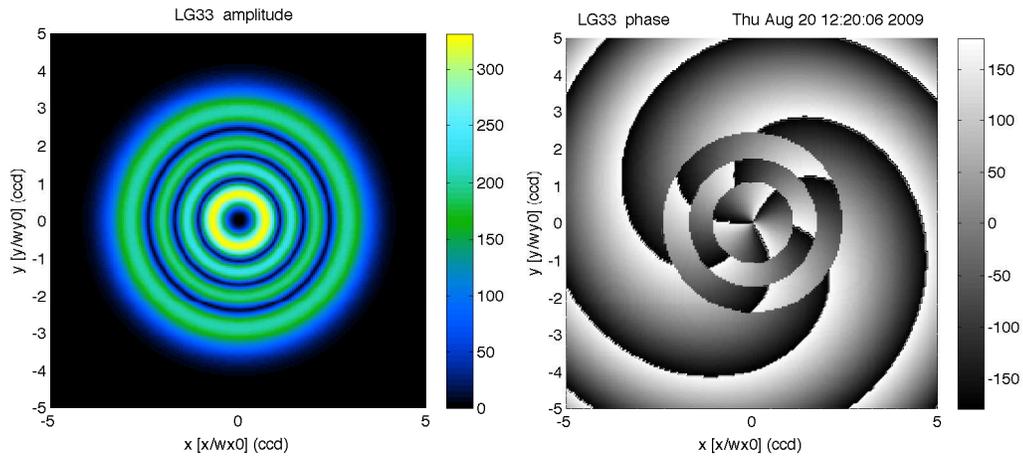


Figure 9.22: FINESSE example: LG33 mode. The ring structure in the phase plot is due to phase jumps, which could be removed by applying a phase ‘unwrap’.

```

tem i1 3 6 0.125 180
tem i1 2 7 0 0
tem i1 1 8 0.164063 180
tem i1 0 9 0.164063 90
s s1 1 n1 n2          % space of 1m lentgh

beam ccd 0 n2 % beam detector for carrier light
xaxis ccd x lin -5 5 200 % tune x position of beam detector
x2axis ccd y lin -5 5 200 % tune y position of beam detector
yaxis abs:deg % plot amplitude and phase
multi

```

10 NEW: Imperfect interferometers

Imperfections in a Michelson interferometer can refer to any of the differences between a real interferometer and the perfect design. These include, but are not limited to: deviations of the optical properties of the mirrors from the design; the limits of longitudinal and alignment control of the mirrors; additional noise sources not included in our models (i.e. electronic noise); and effects which distort the shape of the beam. To estimate the impact of such imperfections on the Michelson's performance is complicated and requires substantial modelling. The greatest impact on the sensitivity arises from asymmetries between the two arms. For accurate differential measurements, such as those made in gravitational wave interferometers, the mirrors are very carefully manufactured to make the arms as similar as possible. Differences between the two arms, for example, imbalances in the finesse of the two arm cavities, will couple extra light into the anti-symmetric port of the interferometer where it adds additional noise to the detection photodiode.

It is important to understand how imperfections in an interferometer affect the resonating beams and impact the sensitivity of the instrument. For this we need accurate models which can simulate complex interferometers in the presence of such imperfections. This is crucial for the design of interferometers, such as gravitational wave detectors, and the commissioning process, in which deviations of the interferometer behaviour from the expected design must be diagnosed. In this review we will consider imperfections in the form of distortions of the beam and we discuss these effects for gravitational wave interferometers; firstly in terms of the behaviour of distorted optics and how this effects the performance of different optical configurations; and secondly in terms of solutions to these distortion problems and implications for the design process.

10.1 Spatial modes in optical cavities

In the previous chapter the idea of representing distortions of a beam as higher-order Gaussian modes was introduced. Here we use this description to investigate the behaviour of interferometers with distorted beams.

A well designed optical cavity can act as a resonator for a particular order of Gaussian modes, depending on its longitudinal tuning. In modern interferometers such cavities are operated as resonators for the fundamental mode, filtering out unwanted spatial components of the beam. This is achieved as each Gauss mode is subject to an additional phase term as it propagates. This additional phase depends on the mode order:

$$\varphi(z) = (n + m + 1)\psi(z) = (n + m + 1) \tan^{-1} \left(\frac{z}{z_R} \right) \quad (10.1)$$

where $n + m$ is the mode order, ψ is the Gouy phase and z_R is the Rayleigh range (see Section 9.5). This additional phase ensures different modes are resonant in a cavity at different longitudinal tunings. The Gouy phase accumulated in one round trip of a cavity is

$$\Psi = 2(\psi_2 - \psi_1) = 2 \left(\tan^{-1} \left(\frac{z_2}{z_R} \right) - \tan^{-1} \left(\frac{z_1}{z_R} \right) \right) \quad (10.2)$$

where $\psi_{1/2}$ is the Gouy phase at the input/end mirror, $z_{1/2}$ is the distance from the waist of the input/end mirror and z_R is the Rayleigh range, all in terms of the cavity eigenmode. The different resonant tunings for various HOM in a cavity is illustrated in figure 10.1, where an Advanced LIGO cavity is simulated with an input beam made up of equal parts of 6 different order modes, orders 0 to 5. Each of the higher-order modes is resonant at a different microscopic tuning; a cavity operated on resonance for the fundamental mode (order 0) will suppress the power in the higher-order modes circulating in the cavity and transmitted by the cavity, as these are not resonant at the same tuning. In consequence the higher-order modes are reflected by the cavity.

$R_{C,1}$ [m]	$R_{C,2}$ [m]	w_0 [cm]	w_1 [cm]	w_2 [cm]	z_1 [m]	z_2	z_R [m]	$\frac{\Psi}{2}$ [°]
1934	2245	1.2	5.3	6.2	-1834	2160	425	24.3

Table 1: Summary of the parameters defining the Gaussian eigenmode of an Advanced LIGO arm cavity. This includes the radius of curvature, R_C , at the input (1) and end (2) mirrors; the beam spot size, w , at the input mirror, end mirror and at the beam waist (0); the distance from the waist, z , of the input and end mirrors; the Rayleigh range, z_R ; and half the round-trip Gouy phase, $\frac{\Psi}{2}$.

The parameters for the Gaussian eigenmode of an Advanced LIGO arm cavity are summarised in table 1. This includes half the round-trip Gouy phase, in this case 24.3° , which gives the spacing between subsequent resonance peaks in terms of cavity tuning (as seen in figure 10.1).

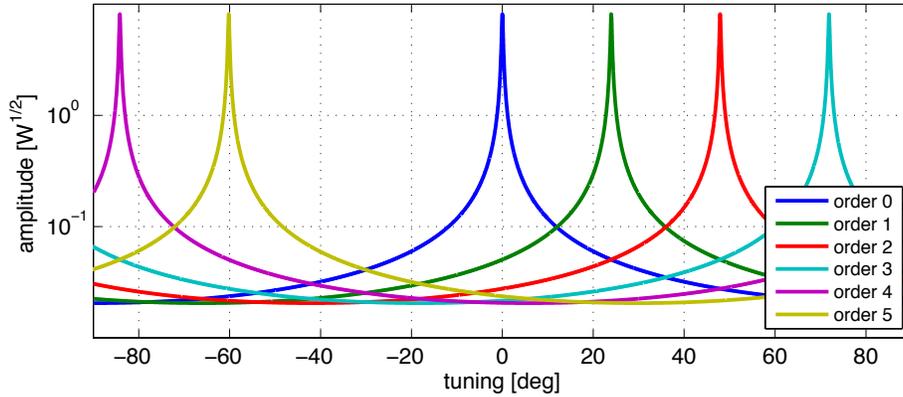


Figure 10.1: Amplitude of 6 higher-order modes (orders 0 to 5) circulating in an optical cavity as the microscopic length is tuned. The fundamental mode (order 0) is resonant at 0° tuning and the mode separation tuning, 24° is defined by the length of the cavity and the mirror curvatures.

This property of an optical cavity to act as a filter of spatial modes is utilised in gravitational wave detectors. Firstly, the input laser beam is ‘cleaned’ of spatial modes by passing through an *input mode cleaner*, an optical cavity carefully designed to transmit the fundamental mode and filter out most higher-order modes before the beam enters the main interferometer. Within the multiple cavities of the central interferometer careful design can take advantage of these resonant properties to suppress distortions of the beam. Finally, the output beam containing the gravitational wave signal is cleaned of spatial modes and control sidebands using an *output mode cleaner*. These design features are discussed in greater detail in section 10.7.

10.2 Cavity alignment in the mode picture

In the previous example the injected beam contains several different order modes. This is an exaggeration of the effect of a mode cleaner, where a distorted beam is cleaned of unwanted spatial modes. After the mode cleaner the input beam is well described by the fundamental mode and higher-order modes present in interferometers can be the result of defects in the optics and mismatches between the incoming beam and eigenmode of the interferometer. The simplest example of this is a misaligned 2-mirror cavity, where the optical axis of the incoming beam is not aligned to the optical axis of the cavity.



Figure 10.2: Different possible misalignments of an optical cavity. **a)** Constant x displacement of the input beam optical axis with respect to the cavity axis. **b)** Relative tilt between the input optical axis and the cavity axis.

As discussed by Anderson [9] and illustrated in Figure 10.2 we can consider different possible misalignments. Any misalignment can be split into a displacement in x (or y) of the input beam axis with respect to the cavity axis (a) and a relative tilt between the input beam and cavity axes (b). For mathematical simplicity we consider a fundamental Gaussian beam at the waist. As the Hermite-Gauss modes are separable in x and y we just consider the x component. The results are equivalent for a displacement in y . The fundamental mode ($n = 0$) and first order mode ($n = 1$) of the cavity can be written

$$u_0(x) = \left(\frac{2}{\pi w_0^2}\right)^{1/4} \exp\left(-\frac{x^2}{w_0^2}\right) \quad u_1(x) = \left(\frac{2}{\pi w_0^2}\right)^{1/4} \frac{2x}{w_0} \exp\left(-\frac{x^2}{w_0^2}\right) \quad (10.3)$$

where w_0 is the beam waist size. Assuming the input beam matches the cavity eigenmode, with the exception of the misalignment, a displacement of the input beam (a) is translated onto the cavity axis as

$$u_{\text{disp.}}(x) = u_0(x - x_0) = \left(\frac{2}{\pi w_0^2}\right)^{1/4} \exp\left(-\frac{(x - x_0)^2}{w_0^2}\right) \quad (10.4)$$

As long as the displacement, x_0 , is small compared to the beam size ($\frac{x_0}{w_0} \ll 1$) any second order terms and higher in $\frac{x_0}{w_0}$ can be ignored and the input field is approximated as

$$u_{\text{disp.}}(x) \approx \left(\frac{2}{\pi w_0^2}\right)^{1/4} \left(1 + \frac{2xx_0}{w_0^2}\right) \exp\left(-\frac{x^2}{w_0^2}\right) = u_0(x) + \frac{x_0}{w_0} u_1(x) \quad (10.5)$$

Thus this displacement of the input beam, with respect to the cavity, is equivalent to the addition of a first order Hermite-Gauss mode.

Similarly a misalignment in terms of a tilt of the input axis with respect to the cavity axis (b) can be described by the addition of a first order mode [9]. In this case the amplitude of the input field as projected onto the cavity axis is un-altered, for small tilts, and the relative misalignment only effects the phase of the beam

$$u_{\text{tilt.}}(x) = u_0(x) \exp(i k \sin(\alpha)x) \approx u_0(x) \exp(i k \alpha x) \quad (10.6)$$

For a small misalignment the higher-order terms of the exponential are ignored

$$u_{\text{tilt.}}(x) \approx u_0(x) (1 + i k \alpha x) = u_0(x) + i \frac{k \alpha w_0}{2} u_1(x) \quad (10.7)$$

The relative tilt of the input beam is expressed with the addition of an order 1 mode, 90° out of phase with the fundamental mode. This 90° phase factor is a useful feature which can be used to separate the order 1 modes caused by a displacement of the optical axis and those caused by a tilt

of the optical axis. A combination of these two types of misalignment can describe any misaligned cavity.

The consequence of a misalignment of an optical cavity is the creation of first order modes. If we chose to describe the problem using the Gaussian beam parameters and axis of the incoming beam as our basis, then the incoming beam is a pure fundamental beam and a first order modes is created when the light enters (and leaves) the cavity. Alternatively we can using the cavity eigenmode and cavity axis as our basis. In this case the higher-order modes are already present in the incoming beam. Either of these approaches is valid for such a simple distortion.

In more realistic cases the circulating field in a cavity is not completely described by a fundamental Gaussian beam, due to deviations of real mirrors from an ideal sphere. This can be modelled using the closest Gaussian eigenmode (from now on refereed to as the eigenmode of the cavity) superimposed with higher-order modes. On can say that the higher-order modes are created when the fundamental mode interacts with the distorted mirrors.

To describe the input-output relations of a cavity for higher-order modes it is important to know at which location they have been created, in other words where they enter the cavity. For higher-order modes present in the input beam (not created inside the cavity) the amplitude of these modes in the circulating field is given by:

$$a_{n,m}^{\text{circ.}} = \frac{i r_2 t_1 \exp(-i 2kL + i(1+n+m)\Psi)}{1 - r_1 r_2 \exp(-i 2kL + i(1+n+m)\Psi)} a_{n,m}^{\text{in}} \quad (10.8)$$

where $a_{n,m}^{\text{in}}$ is the amplitude of the HOM in the incoming field. The equation is very similar to that for a plane wave (equation 2.3) with the addition of the Gouy phase picked up for different modes. On the usual operating point of resonance for the fundamental mode this simplifies to:

$$a_{n,m}^{\text{circ.}} = \frac{i r_2 t_1 \exp(i(n+m)\Psi)}{1 - r_1 r_2 \exp(i(n+m)\Psi)} a_{n,m}^{\text{in}} \quad (10.9)$$

A well designed cavity will have $(n+m)\Psi \neq N2\pi$ up to a high mode order to prevent other modes resonating. In the case, where we consider higher-order modes created at individual mirrors, the equations are different. If the modes are created at the end mirror, with no higher-order modes present in the input beam, the circulating field is approximated as:

$$a_{n,m}^{\text{circ.}} \approx \frac{i r_2 t_1 \exp(i(n+m)\frac{\Psi}{2})}{(1 - r_1 r_2)(1 - r_1 r_2 \exp(i(n+m)\Psi))} k_{0,0,n,m} a_{0,0}^{\text{in}} \quad (10.10)$$

where $k_{0,0,n,m}$ is a coupling coefficient describing the phase and amplitude of the mode HG_{nm} created at the end mirror, due to an incident HG_{00} mode. The approximation here assumes the coupling is small and so does not include the loss of power from the HG_{00} mode and coupling from the HG_{nm} mode back into HG_{00} . This approximation is valid for small distortions, but including distortions on all the optics will quickly become very complicated analytically, and it is for such problems that simulation tools such as FINESSE are valuable.

In Figure 10.3 the effects of misalignment on intra-cavity power is illustrated. In this example an Advanced LIGO cavity has been modelled with a misaligned end mirror. The circulating power exhibits several peaks, corresponding to the resonances of the different higher-order modes created due to the misalignment. Most of the power remains in the fundamental mode (peak at $\sim 0^\circ$). The misalignment of the cavity has induced higher-order modes, mostly the first order HG_{10} mode, whose resonance is observed at $\sim 24^\circ$. In this case the extent of the misalignment also results in the creation of the order 2 mode HG_{20} , resonant at $\sim 50^\circ$. During operation, where the cavity is on resonance for the HG_{00} mode, the relative power in higher-order modes is suppressed. There will still be some higher-order modes in the beam at this tuning, which degrade the purity of the beam transmitted and reflected from the cavity.

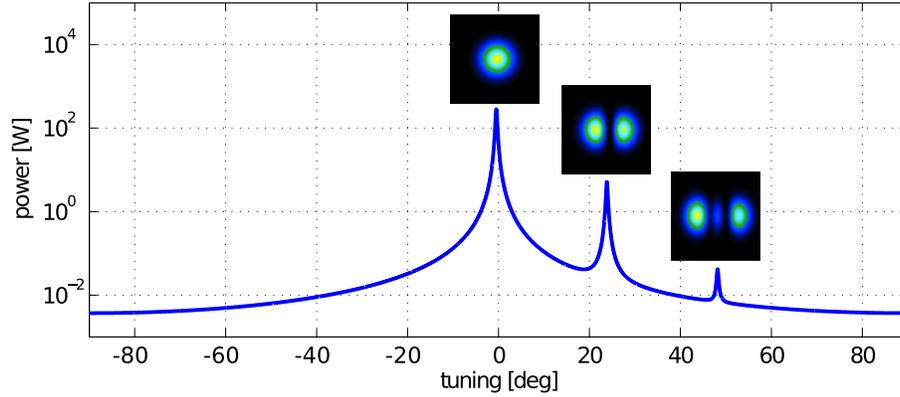


Figure 10.3: Circulating power in an Advanced LIGO cavity with a $0.3 \mu\text{rad}$ misalignment applied to the end mirror. The cavity is tuned and the circulating beam is detected for each peak in intra-cavity power. Most of the power remains in the fundamental mode, resonant at $\sim 0^\circ$, with some coupling into HG_{10} , resonant at $\sim 24^\circ$, and HG_{20} , resonant at $\sim 50^\circ$.

10.3 Mode mismatch

Another common defect of optical cavities with respect to an input laser beam is known as *mode mismatch* [126]. Whilst (a small) misalignment is a first order effect described by first order modes, a (small) mode mismatch is a second order effect, where the wavefront curvature or beam size of the incoming beam does not match that of the cavity eigenmode. Such effects are described primarily by second order modes. As with misalignment this defect can be split into two different effects: beam size mismatch and waist position mismatch.

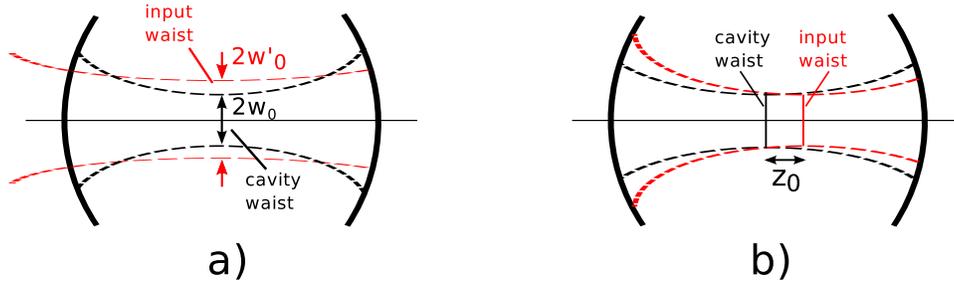


Figure 10.4: Different possible mode mismatch between an the eigenmode of an optical cavity and an injected laser beam. **a)** Beam size mismatch. **b)** Mismatch of the position of the beam waists.

In the case of a pure beam size mismatch, with the cavity and input beam waists located at the same point along the optical axis the input beam can be described in the cavity basis as [9]:

$$u_{\text{size.}}(r) = u_0(r) + \epsilon u_2(r) \quad (10.11)$$

where u_0 is the fundamental cavity mode, ϵ is the fractional difference in the input beam size to the beam size of the cavity eigenmode, $w'_0 = (1 + \epsilon)w_0$, and u_2 is the second order Laguerre-Gauss mode of the cavity, with no angular dependence (LG_{10})

$$u_2(r) = \sqrt{\frac{2}{\pi}} \frac{1}{w_0} \left(1 - \frac{2r^2}{w_0^2}\right) \exp\left(-\frac{r^2}{w_0^2}\right) \quad (10.12)$$

In this case the calculation is performed at the waist for simplicity. Similarly, for a purely waist position mismatch we have

$$u_{\text{posit.}}(r, z) = u_0(r, z) + i \frac{kz_0}{w_0^2} u_2(r, z) \quad (10.13)$$

where z_0 is the displacement of the input beam waist with respect to the cavity waist, and the fundamental and second order modes are now in their more general form, taking into account a finite radius of curvature. As with misalignment we find that the two types of mode mismatch result in the creation of the same mode, with one in phase (beam size) and one with a 90° phase shift (waist position) with respect to the fundamental mode.

In figure 10.5 the circulating power in a mismatched cavity is shown. In this case the mismatch is a 25% mismatch purely in beam size. Most of the power remains in the fundamental mode (resonant at 0°), with most of the mismatch described by the order 2 mode LG_{10} (resonant at $\sim 50^\circ$). Such a large mismatch results in additional modes with even mode orders: the order 4 mode LG_{20} and order 6 mode LG_{30} .

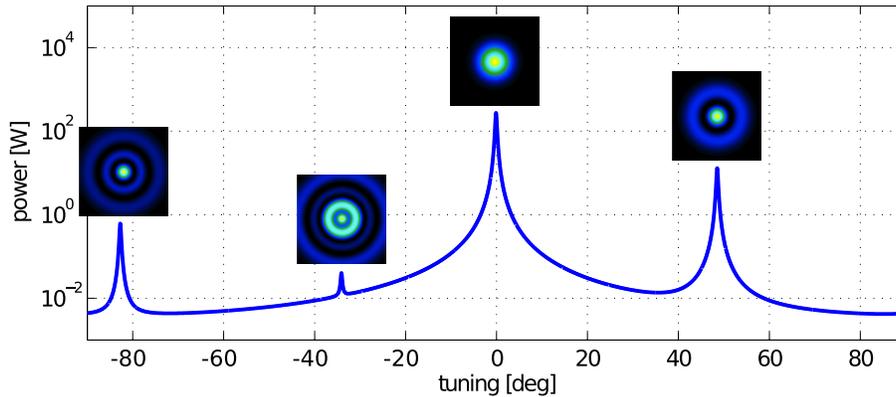


Figure 10.5: Circulating power in a Advanced LIGO cavity with a 25% mismatch in beam size between the injected beam and the cavity eigenmode. The intra-cavity power is detected as the longitudinal length is scanned, with the beam detected at each local resonance. Most of the power is in the fundamental mode, resonant at $\sim 0^\circ$, with the mismatch represented by power in the order 2 mode LG_{10} ($\sim 50^\circ$), the order 4 mode LG_{20} ($\sim -80^\circ$) and the order 6 mode LG_{30} ($\sim -35^\circ$).

10.4 Spatial defects

Misalignment and mode mismatch are the lowest order distortions of the beam and are well described analytically. These low order distortions are carefully controlled in an interferometer, using alignment control schemes and using lenses and curved optics to mode match beams between different cavities. Higher-order distortions produced from more complex processes, i.e. interaction with distorted mirror surfaces or finite sized optics, cannot currently be controlled. There are many different spatial defects which are likely to be present in real interferometers.

For the design and commissioning of real detectors we want to represent these more arbitrary defects, in particular the deviation of the mirror surfaces from a perfect sphere. In the case of interferometer design this will help set requirements on the polishing and coating of the mirrors. For the commissioning process this will aid in identifying the output beam shape and other effects associated with distortions of the beam. In this article we will focus on mirror surface errors and thermal effects. The detailed mathematics of these higher-order effects will be discussed

in Chapter 11. For now we just consider that higher-order modes are created when beams are distorted. The advantage of describing distortions of the beam as higher-order modes is that these spatial modes are easy to trace through the interferometer, to predict the behaviour of a distorted interferometer.

10.5 Operating cavities at high power

Advanced gravitational wave detectors will operate with very high powers in the arm cavities, to increase the signal compared to the shot noise. In Advanced LIGO, for example, the power in the arms will be almost 1 MW [8]. Even the state of the art optics used in advanced gravitational wave detectors will absorb a proportion of the power incident on them. The mirrors produced for Advanced LIGO have requirements of < 0.5 parts-per-million (ppm) power absorption. With the expected power in the arms this means ~ 0.5 W will be absorbed in the mirror coatings and substrates. During operation this absorption of power will lead to a temperature gradient evolving in the optics, starting from a *cold state* defined by the temperature of the environment and gradually developing a temperature field across the optic, with a hot point at the centre where the beam is most intense. Finally the temperature field of the mirrors will reach a steady state, where the optic is in thermal equilibrium. The development of such temperature gradients in the mirrors will result in two types of mirror aberration:

1. A thermal lens forms within the mirror due to the temperature dependent nature of the index of refraction of the substrate material (fused silica). This distortion can be described mostly as a spherical lens, with some higher-order components.
2. The mirror expands thermally, with the expansion greatest where the mirror is hottest, giving a non-uniform expansion over the mirror surface and effectively distorting the surface from the cold case. This thermal distortion is primarily a change in the radius of curvature of the mirror.

Both these effects will impact the shape of the beam in the arms, the thermal lens in the input mirror distorting the beam injected into the cavities and the surface distortions of the cavity mirrors changing the shape of the beam resonating in the arms. These effects will be primarily second order effects, impacting the mode matching of the beam into the arm cavities and the resonating eigenmode. Crucially these effects are not constant: the temperature fields and thermal aberrations will evolve from the cold state to thermal equilibrium, where this equilibrium state, or *hot state*, is dependent on the interferometer input power. For example, Advanced LIGO is expected to operate within a range of input powers up to ~ 100 W. The transitory nature of these thermal aberrations will be one of the key challenges for advanced interferometers. Effectively the input mode and cavity eigenmodes are constantly developing and require additional systems to control the resonating mode of the interferometer. For a more detailed description of the evolution of these thermal effects please refer to the Living Reviews article [159]. Here we will attempt to quantify this problem and motivate the need for thermal compensation systems to correct the lensing and change in curvatures of the mirrors at high power.

Firstly we consider a single arm cavity of the second generation gravitational wave detector Advanced LIGO [14]. The two mirrors which make up this cavity, the input test mass (ITM) and end test mass (ETM) are separated by ~ 4 km. The radii of curvature and optical parameters are given in Table 2. These numbers refer to the curvature of the mirrors in the cold state, before heating of the mirror from the laser beam. During operation the mirrors will heat up as they absorb power from the laser beam, creating a thermal lens in the ITM and distorting the reflective surfaces of both mirrors. Advanced LIGO is expected to operate within a range of input powers. Here we will refer to the cold case (0 W input power), low power (12.5 W input power) and high

	R_C [m]	Transmittance	Loss [ppm]
ITM	1934	1.4%	37.5
ETM	2245	5 ppm	37.5

Table 2: The design geometric and optical parameters of an Advanced LIGO arm cavity. The radius of curvature (R_C), proportion of power transmitted and proportion of power lost for the input test mass (ITM) and end test mass (ETM) are given. ppm refer to parts-per-million [14].

power (125 W input power). This gives a maximum of 800 kW in the arm cavities at high power. The thermal lensing and distortions for each case are summarised in Table 3. The thermal lens is the dominant aberration and will have a large impact on the beam injected into the cavity. However, it will not impact the eigenmode of the cavity, this is determined purely by the curvature of the highly reflective mirror surfaces.

Consider an individual arm cavity with an incoming laser mode matched to the cold optics (the design curvatures). The size of the beam corresponding to this cold eigenmode is plotted in blue in Figure 10.6 along the length of the cavity. Next we consider the hot eigenmode of the cavity, in this case corresponding to the curvatures of the cavity during high power operation (125 W). This is plotted in red. The mirrors are less curved and the eigenmode differs slightly from the cold case, with a slightly smaller beam size at the input and end mirror and a larger waist. The mismatch between the two eigenmodes is relatively small. The incoming beam, however, is strongly mismatched between the possible cavity eigenmodes (shown plotted in orange). During high power operation the injected beam will experience a strong 5 km lens in the ITM, focussing the beam and shifting the waist closer to the ITM, resulting in a larger beam at the ETM.

In reality the hot eigenmode and input beam will develop over time as the mirrors heat up and the aberrations evolve. This takes us from the cold case, where the incoming beam is well matched to the cavity, to the hot case where there is a strong mode mismatch. This will have a strong impact on the power injected into the cavity. During operation the arm cavities are ‘locked’ to the resonance of the fundamental cavity mode. In this state the components of the injected beam which do not overlap with the cavity eigenmode will be reflected. As was discussed in section 10.3 these will be primarily order 2 modes.

Table 4 lists the beam parameters for the 3 different Gaussian beams: the cold and hot cavity eigenmodes, calculated from the radii of curvature of the hot and cold optics, and the hot input beam, calculated using an ABCD matrix for a 5 km lens (see Section 9.13). To estimate how much power will be injected into the hot cavity we calculate the overlap between the hot cavity eigenmode and hot input beam, i.e., we want to know how much power in the input beam is in

	f_{ITM} [km]	$\delta R_{C,ITM}$ [km]	$\delta R_{C,ETM}$ [km]
Cold case (0 W)	∞	∞	∞
Low power (12.5 W)	50	1100	1600
High power (125 W)	5	110	160

Table 3: The expected thermal aberration of the test masses in an Advanced LIGO arm cavity for 3 states of operation corresponding to different input powers. The aberrations are well described by second order effects: a spherical lens in the ITM characterised by focal length f_{ITM} and distortions of the reflective surfaces of the mirrors characterised by a change in curvature $\delta R_{C,ITM}/\delta R_{C,ETM}$. In these cases of relatively low power absorption the distortions scale linearly with power.

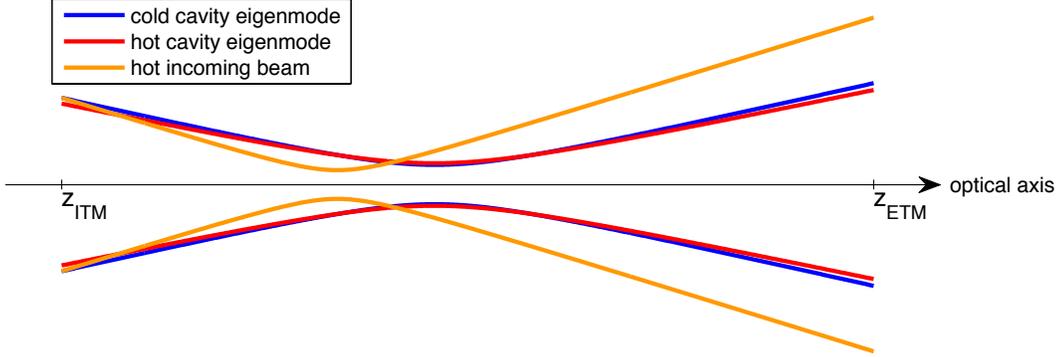


Figure 10.6: Plots of the predicted beam sizes for different states (hot and cold) of an Advanced LIGO arm cavity. In the cold case the cavity eigenmode (blue curve) is defined by the radius of curvature of the cold optics (0 W input power). We assume the incoming beam is mode matched to the cold cavity. The hot case refers to high power operation (125 W input power) where the mirrors absorb a proportion of the laser power. The hot cavity eigenmode (red curve) is determined by the curvature of the reflective surface of the hot optics: the mirror expands elastically, reducing the curvature. This changes the eigenmode of the cavity. In the hot case the input beam (orange curve) will no longer be matched to the cavity eigenmode, as it passes through the strong thermal lens ($f = 5$ km) in the ITM. During high power operation *thermal compensation systems* will be used to correct the curvatures of the mirrors back to their cold state and compensate the lens in the ITM, with the aim of keeping the interferometer modes well matched and consistent for a range of input powers.

	q [m]	w [cm]	R_C [m]	z [m]
Cold eigenmode	$-1834.2 + 427.8i$	5.30	-1934	-1834.2
Hot eigenmode	$-1832.7 + 499.0i$	4.95	-1968.6	-1832.7
Hot input beam	$-1356.2 + 228.1i$	5.30	-1394.6	-1356.2

Table 4: Beam parameter, q , beam size, w , wavefront curvature, R_C and distance from the wasit, z of 3 different Gaussian beams, the eigenmode of an Advanced LIGO cavity during cold operation (0 W input power) and during hot operation (125 W input power) and the input beam during hot operation.

the 00 mode of the cavity eigenmode. This takes the form

$$c = \int_S u_{\text{in}} u_{\text{cav}}^* dS \quad (10.14)$$

where u_{in} is the input field, u_{cav} is the cavity eigenmode, S is an infinite surface perpendicular to the optical axis and the percentage of input power in the cavity eigenmode is given by $|c|^2$. In this case both beams are cylindrically symmetric fundamental Gaussian beams (not astigmatic) and the overlap can be calculated as

$$c = \frac{2}{\pi} \frac{1}{w_{\text{in}} w_{\text{cav}}} \exp(i \Psi_{\text{in}} - i \Psi_{\text{cav}}) \int_0^{2\pi} \int_0^\infty \exp\left(-\frac{ikr^2}{2} \left(\frac{1}{q_{\text{in}}} - \frac{1}{q_{\text{cav}}^*}\right)\right) r d\phi dr \quad (10.15)$$

Integrating with respect to ϕ and changing variables to $R = r^2$ we have

$$c = \frac{2}{w_{\text{in}} w_{\text{cav}}} \exp(i\Psi_{\text{in}} - i\Psi_{\text{cav}}) \int_0^\infty \exp\left(-\frac{ikR}{2} \left(\frac{1}{q_{\text{in}}} - \frac{1}{q_{\text{cav}}^*}\right)\right) dR \quad (10.16)$$

As $\Re\left\{\frac{ik}{2} \left(\frac{1}{q_{\text{in}}} - \frac{1}{q_{\text{cav}}^*}\right)\right\} > 0$ the solution of this equation can be written as [80]

$$c = -\frac{4i}{w_{\text{in}} w_{\text{cav}} k} \exp(i\Psi_{\text{in}} - i\Psi_{\text{cav}}) \frac{1}{\frac{1}{q_{\text{in}}} - \frac{1}{q_{\text{cav}}^*}} \quad (10.17)$$

Using this formula we calculate the overlap between the hot cavity eigenmode and hot input beam as $|c|^2 = 52.5\%$. Such a large mismatch between the incoming beam and cavity would therefore result in around half the circulating power expected from a plane wave model or with a perfectly mode-matched beam. This is illustrated in figure 10.7, which shows the power circulating in a single arm cavity as the input power is increased from 0 to 125 W, taking into account the 50:50 beam-splitter and assuming a power recycling gain of 45 (in reality this will also be impacted by thermal effects). When no thermal effects are included the increase in circulating power is linear.

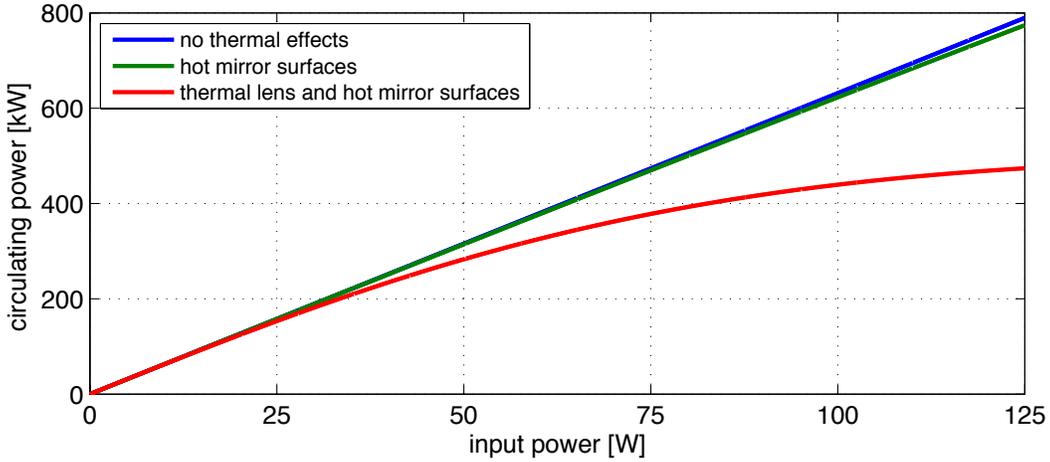


Figure 10.7: The simulated circulating power in an Advanced LIGO arm cavity vs. input laser power into the power recycled interferometer with linear arm cavities. Three cases are simulated: no thermal effects, where the response is linear; including the change in curvature of the mirror surfaces due to thermal effects; and including both the change in curvature of the mirrors and the thermal lens induced in the input mirror due to power absorbed in the mirrors. The addition of the thermal lens has the greatest impact, reducing the power coupled into the arm cavities.

Including the thermally induced reduction in curvature of the mirror surfaces, with the input beam remaining mode matched to the cold cavity, causes a small mismatch, which, at high powers can be noted in a reduction in the gain of the cavity. The largest effect of the internal heating is in the creation of the thermal lens in the ITM, which induces a large mismatch between the beam injected into the cavity and the cavity eigenmode. This is reflected in a large reduction in the circulating power at high input powers, around the 50% reduction predicted by the overlap between the hot input beam and cavity eigenmode. In this simple model we assume a linear scaling of the thermal distortions and lenses with input power. As these aberrations are determined by the circulating power, which no longer scales linearly with input power, this is a slight over estimation of the power loss. In reality this process is more complicated: as the mirrors heat and their aberrations evolve the

circulating power will decrease, but this will then reduce the thermal lensing and distortions. The expected stable cavity will therefore be slightly different to the cases shown here. However, these plots illustrate the magnitude of the problem: such extreme mode mismatches are unacceptably high. We require some method to compensate these effects, especially the thermal lensing. Such compensation will need to be adaptive, to be applicable for a range of input powers and for the transition from cold to hot, controlling the mode resonating in the interferometer as the power is increased and the mirrors reach thermal equilibrium. In reality the thermal aberrations will differ slightly from our models and more importantly the aberrations in each arm will differ from each other, due to differences in absorption for the individual mirrors. The *thermal compensation systems* need to act on individual mirrors, incorporating sensors which monitor the current state of the thermal aberrations in each arm and then feed back to systems which can correct the curvature of the mirror surfaces and the lenses in the ITMs. These compensation systems are discussed in more detail in Section 10.7 and in the comprehensive review article [159].

10.6 The Michelson: differential imperfections

Previously we motivated operating a Michelson interferometer on the dark fringe in order to maximise the differential gravitational wave signal and minimise the noise at the dark port (see Section 5.3). The differential degrees of freedom, the Michelson (MICH) and differential arm length (DARM), are carefully controlled to maintain the interferometer on the dark fringe, as discussed in Section 8.10. A well defined dark fringe relies on the fact that the two arms are very similar and essentially the carrier and any common mode effects cancel at the dark port. Simply we can express the field reflected back towards the laser at the symmetric port as

$$E_{\text{sym.}} = \frac{1}{\sqrt{2}} (E_x + E_y) \quad (10.18)$$

where E_x and E_y refer to the fields coming from the individual arms. The field in the asymmetric port, or output port is

$$E_{\text{asym.}} = \frac{1}{\sqrt{2}} (E_x - E_y) \quad (10.19)$$

In the case where each arm is identical the symmetric field is $E_{\text{sym.}} = \sqrt{2}E_{\text{arm}}$, where E_{arm} is the field reflected from an individual arm, and the asymmetric field is $E_{\text{asym.}} = 0$. For a generic interferometer any field components common to both arms cancel at the asymmetric port whilst any differential components cancel in the symmetric port: the field reflected from the interferometer is the common mode; the field exiting the interferometer is the differential mode. Previously we have considered the carrier and any noise coming from the laser to be common mode (reflected back towards the laser) whilst the asymmetric port is dominated by the differential gravitational wave signal, any differential noise and potentially a small proportion of leaked carrier light for DC readout, see Section 5.4. However, a complex realistic interferometer, such as gravitational wave detectors, contains imperfections and deviations from specifications that lead to additional fields at the asymmetric port. For example:

- Differences in the losses and finesse of each arm result in different carrier amplitudes in each arm, degrading the interference of the two beams at the dark fringe and leading to additional carrier light at the output port.
- Different resonant or interference conditions for the carrier and control sidebands. Advanced gravitational wave detectors such as Advanced LIGO employ a Schnupp modulation scheme, see Section 8.13, to control the interferometer, where by an asymmetric length applied to the short Michelson arms ensures that the dark fringe of the carrier is not equivalent to the dark

fringe of the control sidebands, resulting in a proportion of these radio frequency sideband fields at the dark port.

- Spatial differences between the beams coming from each arm. An imperfect overlap of the spatial distribution of these beams will degrade their interference and cause light in higher-order modes to leak into the dark port.

In the specific examples discussed here we will focus on the impact of higher-order modes at the detector output. These fields do not contain the gravitational wave signal but will carry noise to the output port. This will not only increase the contributions from expected differential mode noises but can couple common mode noise, such as laser noise, into the output channel. Such additional light fields can be referred to as excess light, defined as light fields exiting the interferometer which do not contribute to the signal readout. This should not be confused with the local oscillator fields, such as the leaked local carrier light in the DC readout scheme.

A figure of merit for the excess light leaving a Michelson interferometer is the *contrast defect*. This is the ratio of the excess light exiting through the dark port to the light circulating in the interferometer and is calculated as

$$C = \frac{\int_S E_x - E_y \, dS}{\int_S E_x + E_y \, dS} \quad (10.20)$$

In a Michelson with no differential spatial effects the contrast defect is determined by the differential losses in the arms and at the beam-splitter. In reality slight differences in mirror curvatures, distortions of the mirror surfaces and limits to alignment control will result in different spatial features in each arm, appearing as higher-order modes in the output port and increasing the contrast defect. The mirrors for each arm of the detector are manufactured to be very similar in terms of their optical properties, which will determine differential arm losses; and their geometric and thermal properties, which will determine the higher-order mode content in each arm. In Advanced LIGO the contrast defect should be lower than a few hundred ppm (10^{-6} W/W) [92]. In addition the higher-order modes can be suppressed using an output mode cleaner.

An example of the impact of higher order modes on contrast defect in a dual recycled Michelson have been observed at GEO 600, the German – British gravitational wave detector in Hannover [57, 19]. Unlike other gravitational wave detectors GEO 600 does not include arm cavities, but instead has folded arms to increase the effective arm length of the Michelson. As described in [106], during the operation of GEO 600 it was discovered that a difference in the radii of curvature of the folding mirrors in the x and y arms (687 m in the x arm, 666 m in the y arm) was causing a significant difference in the wavefront curvatures of the beams returning from each arm. This mismatch between the two beams resulted in a significant amount of power at the interferometer dark fringe: the degrade in overlap between the two beams reduced the effective destructive interference and consequently the output beam on the dark fringe was dominated by the order 2 mode typical of a mode mismatch, LG_{10} . The resulting loss of power into the anti symmetric port increased the effective loss in the power recycling cavity, limiting the power build up to ~ 200 W/W, a significant reduction from the 300 W/W predicted for this configuration. The mismatch of the two arms also had a negative impact on the longitudinal error signal of the Michelson, reducing the magnitude of the error signal and increasing the susceptibility to misalignments.

To reduce this mismatch and recover the power recycling gain the curvature of one of the folding mirrors required correcting, to match that of the other arm. In this case the thermal properties of the mirrors were exploited, namely the dependence of the radius of curvature of the mirrors to a temperature gradient, as was discussed in Section 10.5. In advanced detectors the temperature gradient which develops from high powered beams incident on the mirrors is an unwanted effect

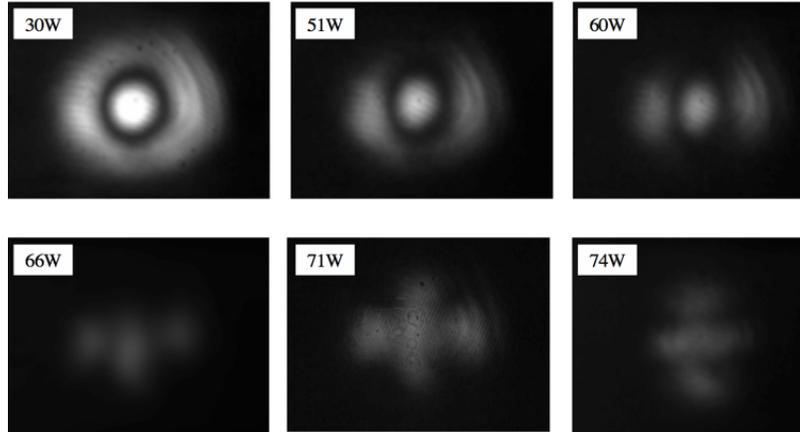


Figure 10.8: Interference pattern at the dark port of GEO 600, for different thermal compensation of the east arm folding mirrors, indicated by the different ring heater powers. The brightness of the beam images in the bottom row are slightly enhanced for better visibility (Figure reproduced from [106]).

which results in the distortions of the mirror surfaces (primarily a change in curvature) and thermal lensing. In GEO 600 this thermal behaviour was manipulated to alter the curvature of the folding mirror in the east arm (x arm) using a ring heater placed behind the mirror substrate to produce an appropriate temperature gradient in the east mirror. The extent of the change in mirror curvature is dependent on the ring heater power, which can be gradually altered to find the power which corresponds to the optimum curvature (i.e. ~ 666 m to match the north mirror).

In Figure 10.8 the interference pattern at the dark fringe is shown for different ring heater powers. For relatively low powers (30 W) the two arms are still not well matched and the dark port is dominated by the typical bullseye shape of the mismatch mode, LG_{10} . As the ring heater power is increased from 30 W to 66 W the mode matching between the two arms increases and the power at the dark fringe is reduced, improving the contrast defect by an order of magnitude. Increasing the ring heater power to 71 W further optimised the dark fringe, in terms of minimum power at the dark port. At this point the limitations of this curvature compensation are observed: the compensation is applied as a spherical curvature correction and does not take into account differences in curvature in the horizontal and vertical directions, i.e. astigmatism of the mirrors or beam-splitter. For ring heater powers of 66–74 W the output mode is still dominated by order two modes but in this case these are the Hermite-Gauss modes consistent with astigmatic mismatches. At 66 W the mismatch between the two arms is compensated in the vertical direction whereas optimum compensation in the horizontal direction requires a ring heater power of 74 W.

To fully diagnose and understand the nature of this problem these measurements were compared with FINESSE simulations of GEO 600. In Figure 10.9 the power circulating in the power recycling cavity is plotted against the power at the dark fringe, showing both simulation and experimental results. Two different experimental results are shown. The first result has the optimum curvature compensation applied with the powers measured as the interferometer passes through the dark fringe (solid red trace). The second result is the case where the interferometer is locked to the dark fringe and the curvature compensation is varied (black markers). The experimental and simulation results are sufficiently similar to suggest that that our understanding of this problem is correct and that the low intra cavity power/ high contrast defect is dominated by a differential mode mismatch. The slight differences between the experimental results and the simulation observed at

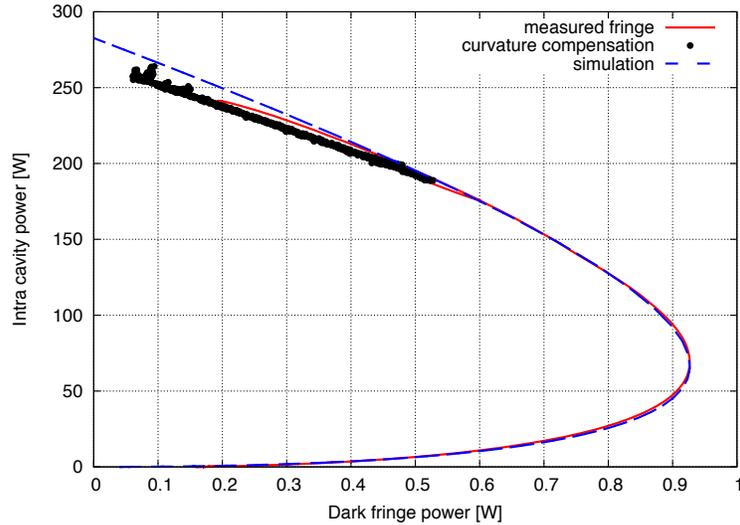


Figure 10.9: Comparison of measurements and simulations of the circulating power and dark fringe power in GEO 600. The measured fringe (red trace) and simulation (dashed blue trace) refer to the measured and simulated powers for GEO 600 as the interferometer is moved through the dark fringe with the optimal curvature compensation applied to the east folding mirror (that which best matches the two arms). The curvature compensation (black markers) refers to measurements made whilst the interferometer is locked to the dark fringe and the curvature compensation of the east mirror is varied (Figure reproduced from [106]).

high intra cavity power can be explained by the limits of the model: no astigmatic or higher-order spatial effects were included in this model and hence the model represents a more simplified system than reality. The experiment and simulation are well matched for low intra-cavity power where the effects of the spherical mode mismatch dominate.

This experience at GEO 600 illustrates the need to have well matched arms. This can be in terms of mode matching, as shown here, or in terms of mirror surface distortions and other defects. While low-order aberrations such as misalignment and mode mismatch can be corrected during operation by means of additional control systems, higher-order effects are typically not actively controlled. It is crucial that the impact of higher-order modes is considered during the design of an interferometer to avoid a large buildup of unwanted modes in the detector.

10.7 Advanced LIGO: implications for design and commissioning

The correct modelling of the impact of beam distortions in interferometers is crucial, not only to our understanding of the physics of real interferometers, but because it will have implications for real experiments, in particular during the design and commissioning of detectors. There are many defects in an interferometer which will effect the shape of the resonating beams. In complex advanced interferometers, such as Advanced LIGO, additional systems help control the shape of the beam, mitigating some higher-order mode effects. The main sources of higher-order modes are:

- **Misalignment.** Any tilt or lateral shift between the beam axis and a cavity axis, or between the axes of the multiple interdependent cavities in advanced interferometers, will produce higher-order modes, for small misalignments these are dominated by first-order modes. In modern gravitational wave detectors these effects are carefully controlled using alignment sys-

tems to maintain consistent optical axes within the interferometer and avoid a large amount of power in first order modes on the detection photodiode.

- **Mismatch.** Second-order modes arise from a mismatch in beam size or wavefront curvature between the cavity eigenmode and incoming beam, or the multiple cavity eigenmodes in complex interferometers. In gravitational wave detectors mismatches are the result of second-order mirror aberrations from the manufacturing process or environmental processes such as thermal lensing. In Advanced interferometers *thermal compensation systems* will be in place to correct the curvature of the arm cavity mirrors, to compensate any thermal lensing and to avoid large mode mismatches.
- **Surface distortions.** Higher-order distortions of the beam are generally the result of higher-order mirror distortions on the highly reflective mirror surfaces. These defects can arise during the manufacturing process (so called *mirror figure error*) or through environmental processes like the thermal distortion of the mirror surfaces. Whilst first and second order distortions of the beam can be corrected it is more difficult to actively correct modes of a higher order. A crucial part of the design process is to determine the tolerances and requirements for the polishing and coating of the interferometer mirrors, to ensure a low higher-order modes content. This is discussed in more detail in Section 11.
- **Apertures** Higher-order modes are also generated when the circulating beams encounter the effective aperture caused by the finite size of optical components. The ‘clipping’ of the beam results in a sharp cut-off, equivalent to the addition of high order modes. The design of a well behaved optical setup will ensure the size of the optics, compared to the beam, is sufficiently large such that these higher-order effects are small and we can simply consider the effect of the aperture as a small power loss.

In this section we consider the impact higher-order mode effects have on the final design of an advanced interferometer. The impact of beam distortions are carefully considered during the design process and here we review the choices motivated by beam shape and size for the particular case of Advanced LIGO.

The input mode cleaner

In a gravitational wave detector use an optical cavity, called the *input mode cleaner* (IMC), between the laser and the main interferometer. The purpose of the IMC is to produce a very pure fundamental TEM_{00} Gaussian beam for the detector input, filtering out higher-order spatial modes. It is also used as part of the laser frequency stabilisation system, producing a very stable carrier frequency. This is motivated by the desire to avoid injecting light fields into the interferometer which may couple additional noise to the output photodiode. The interferometer is tuned to the operating point of one specific mode, the carrier TEM_{00} mode. Any other fields will propagate differently through the interferometer, for example, most higher-order modes do not enter the arm cavities and therefore carry a different phase information than the TEM_{00} mode.

Another requirement of the IMC is to maximise transmission of the fundamental carrier mode, whilst also transmitting the radio frequency control sidebands applied to the beam. For the case of Advanced LIGO the corresponding modulation frequencies are 9 MHz and 45 MHz. The requirement of high transmission for the carrier and certain sidebands sets very specific specifications on the length of the IMC (see Section 5.1), whereas the suppression of higher-order spatial modes requires a choice of mirror curvatures which provide a round-trip Gouy phase sufficient to effectively separate the resonance of the spatial modes (see Section 10.1). The Advanced LIGO IMC is a 3 mirror impedance matched cavity, as shown in Figure 10.10. It consists of two identical flat mirrors (input and output mirrors) and one curved mirror with a very high reflectivity (the end

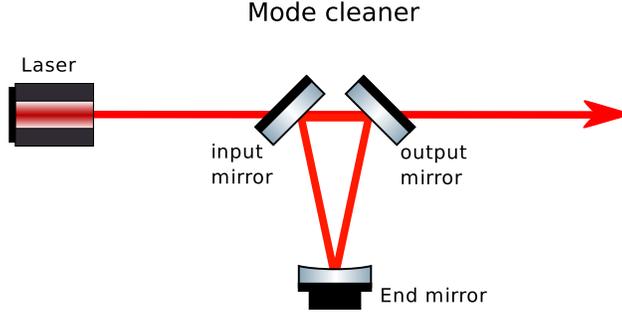


Figure 10.10: Diagram of a 3 mirror input mode cleaner, similar to that used in advanced interferometers. The cavity is impedance matched to ensure maximum transmission of the carrier.

mirror). The final design parameters of the IMC are described in [111], and table 5 summarises the key parameters. The free spectral range (FSR) is chosen to allow transmission of the two control sidebands at $f_1 = 1 \times \text{FSR}$ and $f_2 = 5 \times \text{FSR}$.

Parameter	Value
Length	16.473 m
Free spectral range	9,099,471 Hz
Input/end mirror R_C	>10000 m
Input/end mirror T	0.6%
Input/end mirror R	99.4%
Input/end mirror α	44.59°
Curved mirror R_C	27.24 ± 0.14 m
Curved mirror R	>0.9999
Curved mirror α	0.82°
Finesse	522

Table 5: Summary of key design parameters of an Advanced LIGO input mode cleaner [111]. The cavity length, radii of curvature (R_C), reflectance (R), transmittance (T) and angle of incidence (α) are all given, as well as derived parameters such as the free spectral range and finesse. The cavity consists of 3 mirrors of which the input and end mirrors are nominally flat.

Recycling cavities

As discussed in Sections 10.3 and 10.5, it is important that any beam injected into a cavity is well mode matched to ensure optimum coupling of the laser beam into the cavity. In a Michelson it is important that the two arms are well mode matched to avoid a large amount of power exiting the interferometer through the anti-symmetric port (see Section 10.6). Advanced interferometers are highly complex, incorporating a series of cavities within the general Michelson layout. The addition of a recycling mirror at the symmetric port (power recycling) and anti-symmetric port (signal recycling) form recycling cavities between these mirrors and the rest of the interferometer. The parameters of these cavities must be carefully chosen to ensure a good mode match between the eigenmodes of the recycling cavities and the arm cavities. The following discussion of the design of the recycling cavities refers to the most common design based on arguments presented

in [13]. Note that the Advanced Virgo project has chosen a different design approach [64].

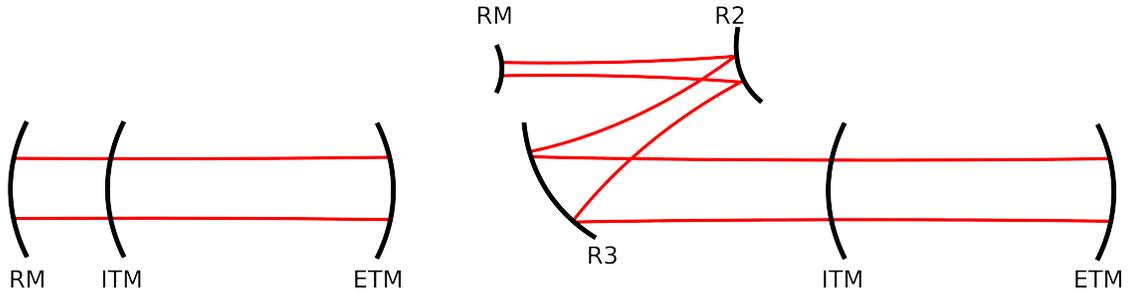


Figure 10.11: Two examples of a coupled cavity formed between a recycling mirror (RM) and an Advanced LIGO arm cavity, made of the input and end test masses (ITM and ETM). The diagram on the left has a single recycling mirror forming a cavity with the ITM. This is illustrative of the setup of Initial LIGO [7]. The diagram on the right illustrates a folded recycling cavity, where two additional mirrors in the recycling cavity reshape the beam between the recycling mirror and ITM. This is the setup used in Advanced LIGO [13]. Illustrations are not to scale and in the case of LIGO the distances between the recycling optics is much smaller (of the order 10 m) than the distance between the test masses (4 km).

For the design stage we first assume perfect matching of the arm cavities. We can then consider each recycling cavity acting with the arms as a simple coupled cavity. Two examples of a possible coupled cavity setup are shown in figure 10.11. The eigenmode of the arm cavities is selected to produce large beams at the ITM (5.3 cm) and ETM (6.2 cm) to reduce thermal noise, with slightly smaller beams at the ITM as the thermal noise is lower here (fewer coating layers) and to prevent scattering into the recycling cavities. The curvatures are also carefully selected for a specific Gouy phase to avoid higher-order modes easily ringing up in the arms: $R_C = 1934$ m (ITM) and $R_C = 2245$ m (ETM). The beam parameter of the arms is therefore a fixed parameter, and the properties of the recycling cavities should be chosen to mode match the recycling cavity to the arms.

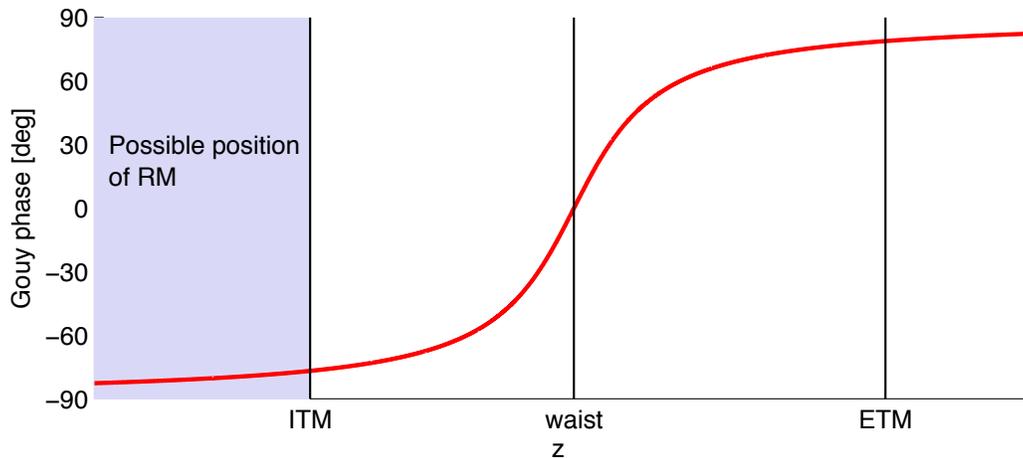


Figure 10.12: Gouy phase as a function of position on the optical axis for the Advanced LIGO arm cavity eigenmode. A single power/signal recycling mirror (RM) would be placed before the ITM in this representation [13].

The simplest design for the recycling cavities uses a single mirror coupled with the arm cavities, as shown in the left diagram of figure 10.11, where the curvature of the recycling mirror is matched to the wavefront curvature of the arm cavity eigenmode. This was the layout chosen for power recycling in Initial LIGO. In this layout the eigenmode of the arm and recycling cavity can be matched. However, there is another consideration for the design of the recycling cavities: the separation of higher-order mode resonances. This is determined by the Gouy phase accumulated in the recycling cavity (between RM and ITM). In figure 10.12 the Gouy phase of the eigenmode for the Advanced LIGO arms is shown at different positions along the optical axis. The ITM and ETM are both far from the waist but the difference in Gouy phase (155.7° , equivalent to -24.3°) is far outside the linewidth of the cavity. With a single recycling mirror the only possible positions do not allow for a large change in Gouy phase, as the ITM is already in the far field. In reality there are additional limitations on the position of the recycling mirror, such as the physical location of the vacuum chambers.

In Initial LIGO this configuration resulted in a power recycling cavity formed in the far field where the higher-order modes resonance were not sufficiently separated: they fell within the linewidth of the cavity. The individual recycling cavity (power recycling mirror and ITM) was only marginally stable in this setup. When operated as a coupled cavity the carrier TEM_{00} mode enters the arm cavity, whilst all higher-order modes are directly reflected, meaning the TEM_{00} mode acquires 180° of phase on reflection from the arm compared with the higher-order modes. This allowed stable operation of the power recycling cavity for the carrier in Initial LIGO, as in the coupled system the HOMs are effectively anti-resonant in the recycling cavity when the carrier is resonant. However, as observed in LIGO [7], this configuration is only marginally stable for the control sidebands, which do not enter the arm cavities and so share the resonance condition of all their spatial modes. HOMs of the sidebands are easily excited through misalignment and mode mismatch and it was only the use of thermal compensation systems which allowed the design sensitivity of LIGO to be achieved.

In Advanced LIGO unstable cavities would be even harder to implement, due to larger beam sizes, large thermal lensing effects and the addition of signal recycling. Unlike the power recycling cavity the signal recycling cavity coupled with the arm cavities will operate on anti-resonance for the carrier, for resonant sideband extraction. Any HOMs will be nearly resonant in an SRC designed with a single recycling mirror. These problems are not easily solved and so an alternative recycling geometry was designed. This is shown in the right diagram of figure 10.11, adding 2 folding mirrors to the recycling cavities to alter the beam parameter and gain significant Gouy phase between the ITM and recycling mirror. The curvatures of these mirrors are carefully chosen to gain this required Gouy phase, whilst maintaining a mode matched system. The design parameters for the power and signal recycling cavities for Advanced LIGO are summarised in Appendix B.

Such stable recycling cavities are now installed in Advanced LIGO. Each recycling cavity is characterised by 3 mirrors: the primary mirrors, PRM and SRM, and two additional folding mirrors which shape and direct the beam, PR2/3 and SR2/3. The greatest change in the beam occurs between PR2/3 (and SR2/3) where the beam size increases by around a factor of 10 over a short distance (~ 16 m). Any small changes in the curvatures of the folding mirrors or the distance between them can lead to substantially larger or smaller beams and degrade the mode matching to the arm cavities. This is illustrated in figure 10.13 where the mode matching between the power recycling cavity, arm cavity and input beam (input mode cleaner eigenmode) is plotted against the distance between PR2 and PR3¹⁵. Two sets of results are shown, those for the nominal values of recycling optics, and those for a slight error in the curvature of PR3. The mode matching between the arm and the recycling cavity is relatively insensitive to the PR2–PR3 distance over a 100 mm range, whilst the mode matching between the recycling mode and input beam falls more sharply

¹⁵This shows results which are slightly different than those reported in [13] because we have used the final design values for this plot, not the preliminary values used in [13].

away from the nominal value. An error in the curvature of the recycling optics can significantly degrade the mode matching, even pushing the recycling cavity to instability (regions of no data). However, the mode matching can be recovered from any such errors by adjusting the distance between the two folding mirrors, R2 and R3.

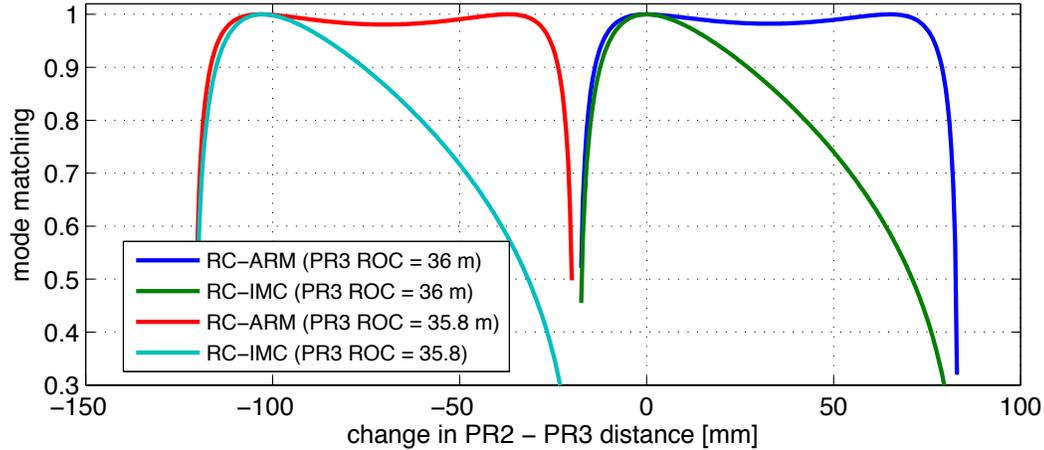


Figure 10.13: Plots showing the mode matching between the recycling cavity eigenmode, the arm cavity eigenmode and the incoming beam (input mode cleaner, IMC, eigenmode) for the Advanced LIGO design. The mode matching is shown for the power recycling cavity as the distance between the two telescope mirrors, PR2 and PR3 (see figure 10.11), is adjusted from the nominal design value. Two sets of results are shown, those for the design curvature of PR3 (36 m) and a small error on this curvature (35.8 m). Adjusting the PR2–PR3 distance recovers the mode matching from errors in the curvatures of the recycling optics [13].

Thermal distortions

The mode matching of the beams between the recycling cavities and arms is complicated by thermal effects, specifically thermal lensing and the change in mirror curvatures. Previously the need for some thermal compensation was motivated by the behaviour of a single cavity at high power (see Section 10.5). For Advanced LIGO the implications for the coupled systems of the arm and recycling cavities were considered during the design phase [14]. In figure 10.14 the mode matching between the recycling and arm cavities, and the recycling cavities and the input mode is shown, as the interferometer input power is increased. As the thermal lens in the ITM is by far the dominant effect (10.5) this is the only thermal aberration included, modelled as a simple spherical lens. The first two traces in figure 10.14 (0 W design) show the mode matching for the original design of the recycling cavities, where the parameters were chosen to match the cold optics of the arm cavities. A second design (18 W design) is also shown. In this case the mode matching between the recycling cavities, the arm cavities and the input mode was optimised for the expected thermal lensing of 34.5 km^{16} at 18 W input power. The advantages of this design is that it gives a larger range of input power at which the interferometer is well mode matched, without the need for thermal compensation systems.

The plots shown in figure 10.14 show that the mode matching between the recycling cavities and arm cavities is relatively independent of the expected thermal lensing. Whilst the eigenmode

¹⁶34.5 km is the focal length when modelled as an individual lens in a vacuum, the approach in this document. Sometimes quoted is 50 km corresponding to the lens when modelled inside the fused silica substrate of the ITM.

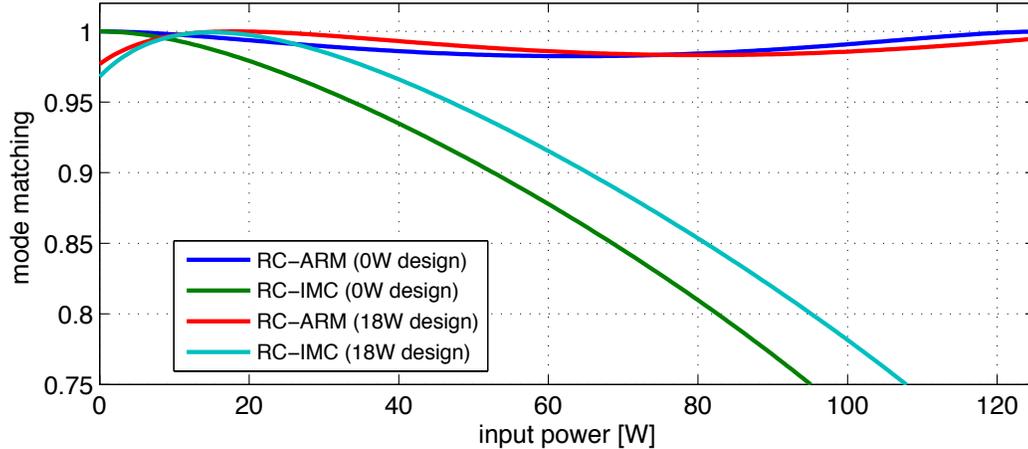


Figure 10.14: Plots showing mode matching at different input powers between the recycling cavities and the arms (RC-ARM) and recycling cavities and the input mode cleaner (RC-IMC) for the Advanced LIGO design. The mode overlap is calculated considering the thermal lens formed in the input test masses from predicted absorptions in the ITMs. Two different designs are considered, one optimised for mode matching at an input power of 0 W (cold optics) and one optimised for 18 W, the final Advanced LIGO design.

of the arm cavity is fixed, the recycling cavity eigenmode is affected by the thermal lens. The recycling eigenmode curvature is fixed at the reflective ITM surface, and the beam size at this point only varies a small amount, maintaining the mode matching between the arm and recycling cavity. However, the effect of the lens on the mode parameters is exaggerated during the large divergence between the recycling mirrors R2 and R3 (see figure 10.11) and this has a large impact on the beam size at the recycling mirror, and hence the mode matching between the input beam and recycling cavity is significantly degraded. As we saw previously for a single cavity, during high power operation the power coupled into the interferometer will be significantly reduced.

In Advanced LIGO *thermal compensation systems* (TCS) will be employed at high power, not only to avoid a low build up of power within the interferometer but to balance the lensing and eigenmodes of the two arms to prevent a high contrast defect [167]. The first is a ring-heater positioned near the anti-reflective surface of each test mass [14]. These are used to heat the outer edge of the mirror to produce a curvature in the opposite direction to that from heating by the beam. The ring heater also corrects some of the thermal lens in the ITM substrate. An additional system is required to complete the correction of the thermal lens. This involves a compensation plate, placed in front of the ITMs, made of the same material (fused silica). A heating pattern is projected onto this plate via a CO₂ laser. This pattern is designed to heat the compensation plate in such a way as to correct any thermal lensing in the ITM [41].

The output mode cleaner

Even with state of the art optics, alignment systems to correct any misalignments and thermal compensation systems to correct for differential mismatches some light at the Michelson anti-symmetric port will be in higher-order modes. There will also be some power in the control sidebands exiting the interferometer, as the dark fringe for the carrier is not the dark fringe for the sidebands due to the applied Schnupp asymmetry (see Section 8.13 and Appendix B.1). The only fields which should be present on the detection photodiode are the gravitational wave signal

sidebands and the local oscillator field, in case of Advanced LIGO this is the leaked carrier light for DC readout (see Section 6.2). If the power in the higher-order modes and control sidebands is sufficiently low they can be effectively stripped from the beam using an *output mode cleaner* (OMC), an optical cavity between the Michelson interferometer and the main photodiode.

The parameters of the output mode cleaner are carefully chosen to maximise the transmission of the gravitational wave signal and local oscillator field, whilst sufficiently filtering out the unwanted spatial modes and control sidebands. The OMC design for Advanced LIGO is a Fabry-Perot cavity in a 4-mirror bow tie configuration [12], consisting of two flat mirrors (the input and output mirrors) and two curved mirrors (high reflectors). To maximise the transmission of the desired fields the cavity is impedance matched between the input mirror and output mirrors. Ignoring any losses, the power in an individual field transmitted by an impedance matched cavity is

$$P_{\text{trans.}} = \frac{T^2}{1 + R^2 - 2R \cos(kL_{rt} - \Psi(n + m + 1))} P_0 \quad (10.21)$$

where T and R are the transmittance and reflectance properties of the input and output coupler, P_0 is the power in the incoming field, k is the wavenumber of the field, L_{rt} is the round-trip length of the cavity, Ψ is the round-trip Gouy phase and n and m are the higher-order mode indices of the field. In a lossless cavity all the power in a field is transmitted on resonance. For an Advanced LIGO OMC with realistic losses the transmission of the carrier TEM_{00} mode and signal sidebands is expected to be $\sim 98\%$. On anti-resonance the transmitted power can be approximated as

$$\min(P_{\text{trans.}}) = \frac{T^2}{1 + R^2 + 2R} P_0 \approx \frac{T^2}{4} P_0 \quad (10.22)$$

in the case of a high finesse cavity, $R \approx 1$. In order to avoid transmitting the unwanted fields the length and curvatures of the cavity mirrors are very carefully chosen. The length of the cavity must not be resonant for the 9 MHz and 45 MHz control sidebands. The curvatures of the mirrors are chosen to ensure sufficient Gouy phase to avoid the resonance of any higher-order modes entering the cavity. This requires careful modelling and a knowledge of which higher-order modes are expected to exit the main interferometer. In [G120111](#) the HOM content is modelled using a power law derived from the spectrum of higher-order modes observed in Enhanced LIGO. This predicts the total power in each order of modes exiting the interferometer as

$$P_{\text{HOM}} = 1.8 \times 10^{-3} \times 10^{-\frac{N}{4.8}} \quad (10.23)$$

where N is the mode order and $N \leq 2$ (1st order modes are reduced via alignment control). Using this power law different mirror curvatures and lengths were modelled to find the optimum design for minimum transmission of the expected undesired fields. This design is presented in [12] and the key parameters are summarised in table 6. With a finesse of ~ 400 and an expected round-trip loss of 140 ppm the transmission of undesirable fields is expected to be 10^{-5}W/W , relative to the power injected into the interferometer. This is equivalent to $\sim 1 \text{ mW}$ at high power, compared to $\sim 100 \text{ mW}$ of reference carrier light for DC readout.

10.8 Commissioning

Commissioning describes the process of tuning and improving a gravitational wave detectors after it's subsystems have been installed and before the full system. This process typically takes several years because the interferometer couples all the subsystems in a unique and complex way, which cannot be tested in advance. This is particularly important for advanced detectors which employ many cutting edge technologies which, although having been tested in the laboratory and at prototype facilities, have never been implemented together in interferometers of this scale. The

Parameter	Value
Length	1.132 m
Free spectral range	264.8 MHz
Input/output mirror R_C	∞
High reflectors R_C	2.5 m
Input/output mirror T	8300 ppm
High reflectors T	50 ppm
Finesse	390
Angle of incidence	4°

Table 6: Summary of key design parameters for the Advanced LIGO output mode cleaner [12]. The length, mirror radii of curvature (R_C) and transmittance (T) are given, as well as derived parameters the free spectral range and finesse.

efficiency of the commissioning process crucial for achieving the expected sensitivity and provide an instrument for scientific data taking in a timely manner.

Through the commissioning process we observe effects never seen before, the interferometer will be operated in a new regime, namely a full scale, high power, dual recycled interferometer with arm cavities. In this extremely sensitive configuration previously negligible effects could have a strong impact on interferometer performance. For example, parametric instabilities, where higher-order mode and radiation pressure effects couple together with the potential of ringing up high order sidebands, will likely be a factor in this high powered regime [39, 63, 81]. Subsystems of the interferometer also use cutting edge techniques which have yet to be tested within the full framework of our advanced detectors.

During commissioning the interferometers are assembled in increments, building towards the full dual recycled configuration. As the optics are installed many measurements are taken to test the behaviour of various subsystems and finally to test the response and noise budgets of the full interferometer. During this process it is crucial that we have accurate models of the interferometers. These must include possible defects and higher-order mode effects, typically going beyond the more simplified models used in the design phase. For example, in Advanced LIGO measurements of the surfaces of the mirrors were taken prior to installation. This surface data can be used in simulations to model the expected distortion of the beams within the real interferometers. During the commissioning process these models are used to check against experimental measurements. In the case where a measurement is not as expected models are used to investigate the possible causes, adding in more realistic measurements and tuning parameters to recreate the observed behaviour. From such models we can then suggest solutions in the case of underperformance.

The interested reader is directed to the following documents, which give details on specific modelling tasks to support the commissioning of for Advanced LIGO, particularly those which are concerned with higher-order mode effects¹⁷:

- Comparisons of alignment signals calculated for Fabry-Perot cavities using three methods: FINESSE, an analytic calculation and the FFT propagation simulation OSCAR [21]
- Comparisons of the control signals and sideband build up in Advanced LIGO, as modelled in FINESSE and Optickle [31, 29]
- Investigation into the effect of mode-mismatch in the control signals of the Advanced LIGO interferometer [32].

¹⁷Many more such documents exist for Advanced LIGO and other gravitational wave projects. This selection is based on our familiarity with the described work.

- A dedicated commissioning investigation into power loss at the central beam-splitter in Advanced LIGO using FINESSE [30]
- FINESSE simulations of the alignment control signal of the Advanced LIGO input mode cleaner [101]

10.9 Finesse examples

10.9.1 Higher-order mode resonances

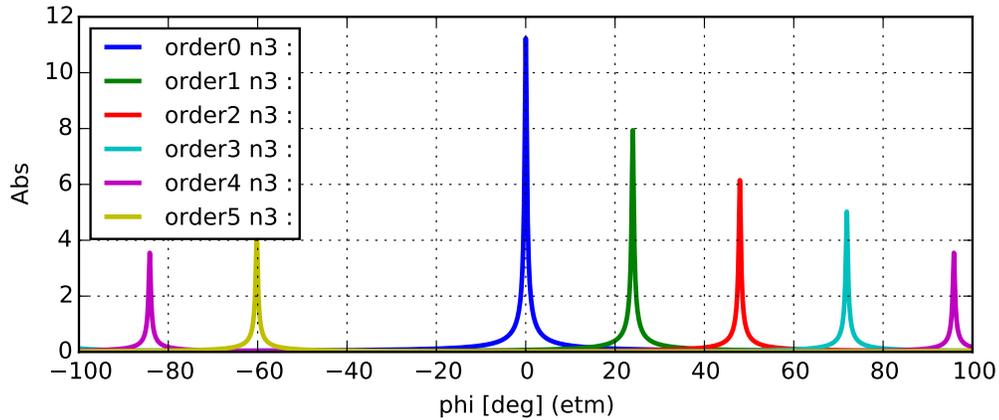


Figure 10.15: FINESSE example: Higher-order mode resonances

This example illustrates the different resonance conditions of the higher-order modes in an optical cavity. In the simulation an input beam made up of 6 different order modes is generated using the ‘tem’ commands. This beam is injected into an Advanced LIGO style cavity and the cavity length is tuned. Using amplitude detectors, ‘ad’, the different order modes are individually detected.

Finesse input file for ‘Higher-order mode resonances’

```

l i1 1 0 nin
tem i1 1 0 0.5 0
tem i1 2 0 0.3 0
tem i1 3 0 0.2 0
tem i1 4 0 0.1 0
tem i1 5 0 0.15 0

s s1 1 nin n1
m itm 0.986 0.014 0 n1 n2
s scav 4000 n2 n3
m etm 1 0 0 n3 n4
cav arm itm n2 etm n3
attr etm Rc 2245
attr itm Rc -1934

ad order0 0 0 0 n3
ad order1 1 0 0 n3
ad order2 2 0 0 n3

```

```

ad order3 3 0 0 n3
ad order4 4 0 0 n3
ad order5 5 0 0 n3
maxtem 5
phase 2
xaxis etm phi lin -90 90 10000
yaxis lin abs

```

10.9.2 Mode cleaner

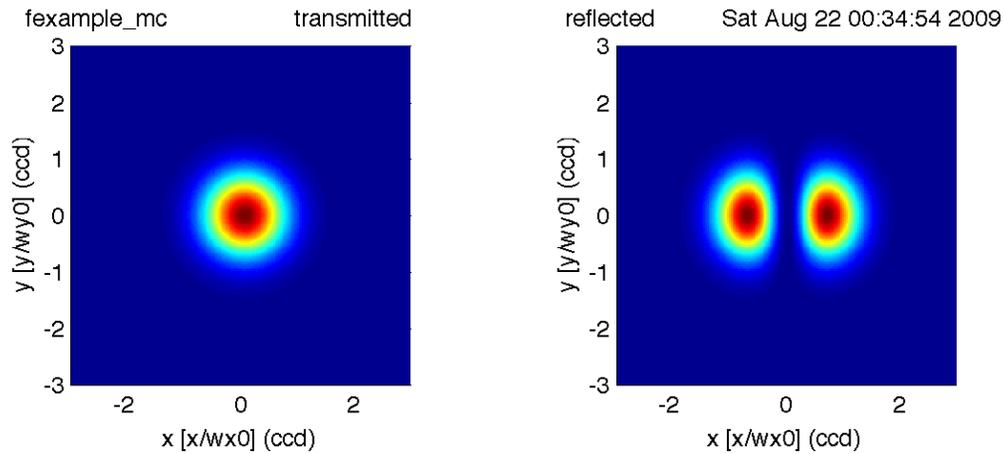


Figure 10.16: FINESSE example: Mode cleaner

This example uses the ‘tem’ command to create a laser beam which is a sum of equal parts in u_{00} and u_{10} modes. This beam is passed through a triangular cavity, which acts as a mode cleaner. Being resonant for the u_{00} , the cavity transmits this mode and reflects the u_{10} mode as can be seen in the resulting plots.

Finesse input file for ‘Mode cleaner’

```

laser i1 1 0 n1          % laser with P=1W
maxtem 1                % need Hermite-Gauss modes up to n+m=1
tem i1 0 0 1 0          % laser beam is a mix of u_00 and u_10
tem i1 1 0 1 0
s s1 1 n1 n2            % a space of 1m length
% triangular mode cleaner cavity
bs bs1 .9 .1 0 0 n2 nrefl n3 n4    % input mirror
s sc1 2 n3 n5           % distance between b1 and bs2
bs bs2 .9 .1 0 0 ntrans dump n5 n6 % output mirror
s sc2 49 n4 n7          % distance between b1 and bs3
s sc3 49 n6 n8          % distance between b2 and bs3
bs bs3 1 0 0 0 n7 n8 dump dump    % end mirror
attr bs3 Rc 150        % Rc=150m for bs3
cav cav1 bs1 n3 bs1 n4 % computing cavity parameters
run1: beam ccd ntrans  % beam shape in transmission
run2: beam ccd nrefl   % beam shape in reflection

```

```

xaxis ccd x lin -3 3 200 % tuning x,y axes of beam detector
x2axis ccd y lin -3 3 200
yaxis abs % plotting the absolute intensity

```

10.9.3 Misaligned cavity

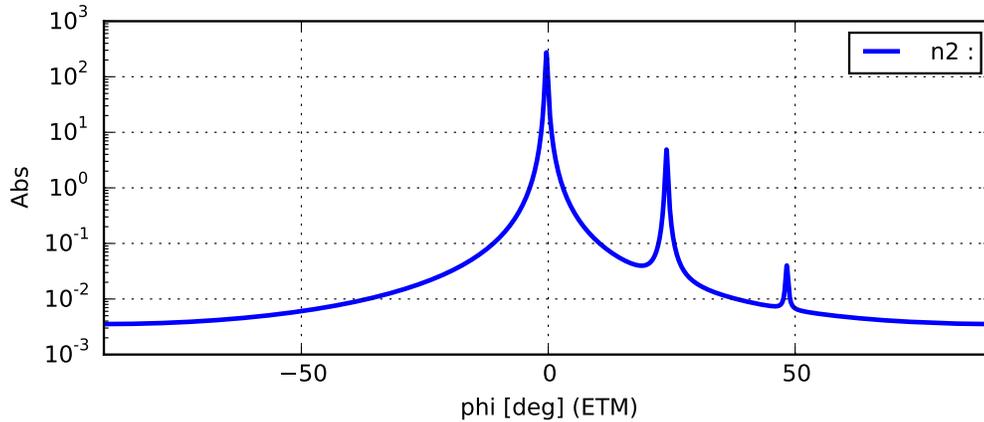


Figure 10.17: FINESSE example: Misaligned cavity

In this example a misaligned cavity is scanned and the circulating power is detected. Additional spikes in the cavity scan indicate the higher-order modes (order one and two are visible) created by the misalignment.

Finesse input file for ‘Misaligned cavity’

```

l i1 1 0 nin
s sin 1 nin n1
m1 ITM 0.014 35u 0 n1 n2
s scav 3994.5 n2 n3
m1 ETM 5u 35u 0 n3 n4
attr ITM Rc -1934
attr ETM Rc 2245
attr ETM xbeta 0.3u
cav FP ITM n2 ETM n3
maxtem 3
phase 2
pd pdscan n2
xaxis ETM phi lin -90 90 5000
yaxis log abs

```

10.9.4 Impact of thermal aberrations

This example shows the power circulating in an Advanced LIGO style arm cavity versus input laser power when we consider the impact of thermal effects (lensing of the input mirror and change

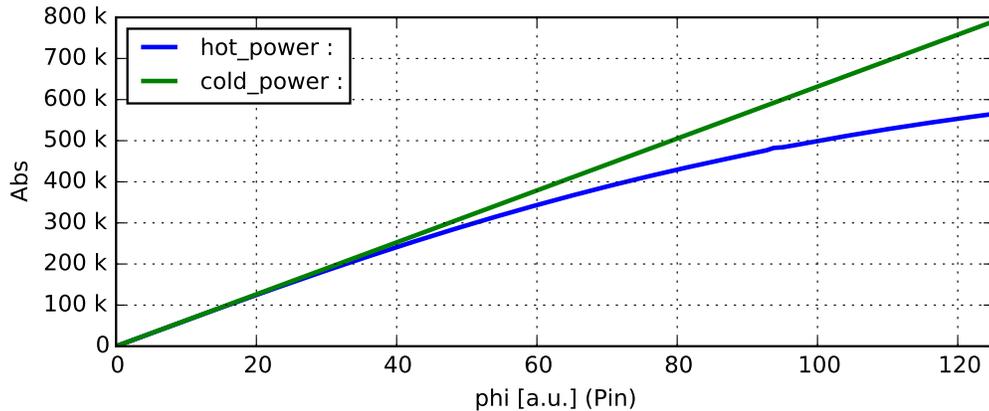


Figure 10.18: FINESSE example: Thermal cavity

in curvature of the mirror surfaces). The mode mismatches these aberrations cause results in less power coupled into the cavity.

We assume here that the thermal aberrations scale linearly with power [159]. As we tune the incident laser power we also tune the thermal changes in curvature ($dRc1$ and $dRc2$). Here we use the change in Rc calculated for an Advanced LIGO cavity operating at high power (125 W) and then scale the Rcs accordingly. The curvatures are combined with the cold state curvatures to give the final state of the cavity mirrors at a given laser power. Similarly for the thermal lens in the ITM we scale the focal length, calculated for high power, with input power.

Finally we scale the power circulating in an individual arm cavity ($\$Pc$) by the gain afforded by the power recycling cavity (45W/W) and the beam splitter (0.5) to represent the power in an arm of the full power recycled Michelson configuration. We also plot the theoretical linear circulating power, when thermal effects are not considered. Here the 280.7W is the circulating power in a cavity simulated with no thermal or higher order mode defects.

Finesse input file for 'Thermal cavity'

```

l i1 1 0 nin
gauss g1 i1 nin 12m -1.83522k
s sin 1 nin na
lens TL inf na nb
s sTL 0 nb n1
m1 ITM 0.014 35u 0 n1 n2
s scav 3994.5 n2 n3
m1 ETM 5u 35u 0 n3 n4
cav arm ITM n2 ETM n3
maxtem 6
attr ITM Rc -1934
attr ETM Rc 2245

pd Pcirc n2
noplots Pcirc
set Pc Pcirc abs
func hot_power = $Pc * $x1 * 45/2
func cold_power = $x1 * 280.7 * 45/2

```

```

phase 3
variable Pin 0
xaxis Pin phi lin 0 125 500
func dRc1 = 0 - 1/(1/55000*$x1/125 + 1E-20)
noplots dRc1
func Rc1 = 0 - 1/(1/1934+1/$dRc1)
noplots Rc1
func dRc2 = 0 - 1/(1/80000*$x1/125 + 1E-20)
noplots dRc2
func Rc2 = 1/(1/2245+1/$dRc2)
noplots Rc2
func foc = 6700*125/($x1+ 1E-20)
noplots foc
put TL f $foc
put ITM Ry $Rc1
put ITM Rx $Rc1
put ETM Ry $Rc2
put ETM Rx $Rc2
yaxis lin abs

```

11 NEW: Scattering into higher-order modes

Spatial variations in the optics that compose a laser interferometers, such as distortions of the mirror surfaces, will change the shape of the circulating beams. Methods for quantifying such optical imperfections and their effects are required during the design of an interferometer and for modelling efforts to characterise the instrument during operation. In particular, this is crucial during the design phase in order to produce, for example, polishing requirements for the mirror surfaces. At first glance it is not obvious how such optical defects should be characterised and we will show that the nature of the problem determines which approach to use.

Previously we introduced the idea that these distortions can be described as higher-order Gaussian modes and considered the impact of such modes on the interferometer performance. In this section we consider the mechanisms and mathematics of this scattering into higher-order modes, with particular emphasis on this process for mirror surface distortions. We will explore how different types of surface distortions impact the beam shape and quantify which mirror shapes produce which higher order modes. Throughout this section we use measured data from the Advanced LIGO mirrors, kindly provided by GariLynn Billingsley of the LIGO Laboratory [26].

11.1 Light scattering in interferometers

The term 'scattering' in interferometers can refer to several different processes. Most commonly it refers to imperfections of high spatial frequency that scatter light into large angles away from the optical axis and effectively scattered out of the path of the beam. This is a different problem to scattering into higher order modes, which occurs when the light is scattered back into the path of the beam (i.e. low angle scattering). Light scattered at high angles has the potential to be re-scattered back into the path of the beam by interactions with, for example, the walls of the beam tube. This will couple new noises into the interferometer, from the beam tubes into the circulating light field. Low angle scattering into higher order modes can introduce noise in other ways, as was discussed in Section 10. The effects of scattered light and mitigation solutions are an ongoing research topic in the gravitational wave community [160, 170, 4, 158].

The different scattering processes require different methods for efficient, accurate modelling. Whereas low-angle scattering can be modelled using a paraxial approach, either via a description of higher-order modes or using a Fourier propagation model, high-angle scattering is outside the paraxial approximation and can require computationally heavy numerical algorithms for accurate results.

In this review we focus on low angle scattering which manifests itself as changes in the beam shape. Of course low and high angle scattering are not two separate phenomena, and we see the paraxial method fail at scattering angles greater than $\sim 20^\circ$. This region between high and low-angle scattering can be difficult to model, falling between the two regimes. In addition, the finite size of the mirrors in real interferometers prevents the buildup of very high-order modes as these are wider than the mirrors and experience significant larger losses. In this way the finite size of the cavity mirrors can set a limit for high angle scattering.

The two regimes of scattering provide correspond to some extent to two commonly used categories for describing spatial surface defects:

1. Flatness, describing the overall shape of a mirror and its large scale, low spatial frequency features. These defects impact the shape of the beam within the path, as can be described with higher spatial modes.
2. Roughness, the high spatial frequency distortions of the mirror which scatter light out of the path of the beam.

11.2 Mirror surface defects

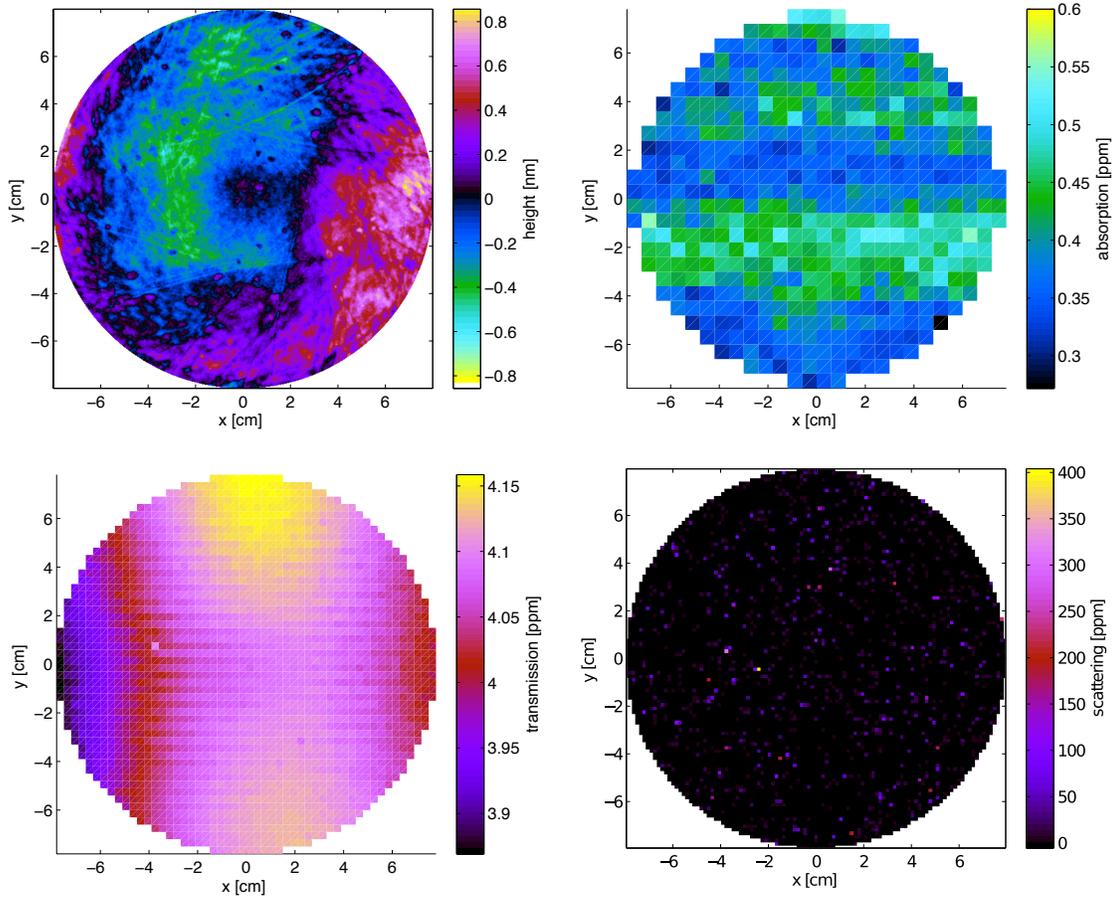


Figure 11.1: *Maps* showing different properties of an Advanced LIGO mirror, measured across the optic (end test mass ETM08) [26]. **Top left:** The surface height of the polished, uncoated substrate of the optic. **Top right:** The absorption of the coated mirror at 1064 nm. **Bottom left:** Transmission of light through the coated optic at 1064 nm. **Bottom right:** Average scatter from the coated mirror surface at 1064 nm.

Realistic mirrors differ from their ideal form in that their optical and geometric properties are not uniform over the optic. A possible categorisation of mirror imperfections in interferometers are:

- misalignment and curvature mismatch, i.e. a mismatch between the position, orientation and shape of the optics with respect to the laser beam
- non-uniform mirror phase effects, distorted surfaces and substrates will change the phase distribution of a reflected or transmitted beam
- non-uniform amplitude effects: dirty or distorted optics can cause non-uniform absorption and reflection

- apertures created by the finite size of the optics

The mirrors can be characterised in detail before installation, see for example the presentation [27]. Figure 11.1 shows plots detailing some measured properties from an Advanced LIGO mirror [26]. These *mirror maps* (see Section 11.5) can be used in simulations of detectors for a more accurate comparison with experimental results or for the purposes of producing design requirements for the mirrors. In following we discuss the effects of misalignment, mode mismatch and mirror surface distortions, as these are expected to be the dominant source of spatial beam distortions. Similar methods can be used to model non-uniform absorption or reflection properties.

11.3 Coupling between higher-order modes

Any paraxial beam can be expressed as a sum of Hermite or Laguerre-Gauss modes. An expansion, in terms of Hermite-Gauss modes, of the arbitrary field $u(x, y, z)$, can be written as [147]:

$$u(x, y, z) = \sum_{n,m} k_{nm} u_{nm}(x, y, z) \quad (11.1)$$

where k_{nm} refer to coefficients which describe the amplitude and phase of each Gaussian mode in the field $u(x, y, z)$. The Hermite-Gauss (and Laguerre-Gauss) modes are orthonormal and the coefficients can be calculated from an inner product with the relevant HG (or LG) mode:

$$k_{nm} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} u(x, y, z) u_{nm}^*(x, y, z) dx dy. \quad (11.2)$$

The integral for a generic distortion from an input mode $u_{n'm'}$ to an output mode u_{nm} due to some distortion to the input beam described by the complex function $A(x, y)$ is:

$$k_{n,m,n',m'}(q, q', A) = \iint_{-\infty}^{\infty} u_{nm}(x, y; q) A(x, y) u_{n'm'}^*(x, y; q') dx dy. \quad (11.3)$$

In the special case when $A(x, y)$ presently only misalignment

$$A(x, y) \Rightarrow A(x, y, \gamma_x, \gamma_y) = e^{i2kz'(\sin^2(\gamma_x/2) + \sin^2(\gamma_y/2))e^{ik}}, \quad (11.4)$$

the integral can be simplified to the Bayer-Helms coupling equation 9.68 as described in Section 9.16. In general, however, the integral cannot be solved analytically. To model realistic mirror surfaces and how they couple higher-order-modes, numerical metrology data is used directly in the coupling coefficient integral. In the generic case $A(x, y)$ represents a complex valued function that interpolates the measured data. For example, for the coupling in reflection from a mirror surface we have

$$k_{nm,n'm'}^{\text{refl.}} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} u_{nm}(x, y, z) \exp(2i k n_1 z(x, y)) u_{n'm'}^*(x, y, z) dx dy \quad (11.5)$$

where $z(x, y)$ describes the distorted surface height and n_1 is the index of refraction for the incident and reflected fields. Similarly, for transmission through a distorted surface we have

$$k_{nm,n'm'}^{\text{trans.}} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} u_{nm}(x, y, z) \exp(i k (n_2 - n_1) z(x, y)) u_{n'm'}^*(x, y, z) dx dy \quad (11.6)$$

where n_1 is the index of refraction for the incident beam and n_2 is the index for the transmitted beam. This process of distorting the beam is referred to as coupling into other modes, as the action of reflection from a distorted surface creates modes other than those contained in the incoming beam.

In interferometer simulations such as FINESSE that use modes to describe the beam shape, a maximum order of the modes included O_{\max} must be defined for each model. The coupling between all modes with an order less than the maximum order of modes is calculated in reflection and transmission of a distorted optic. This is represented as a coupling coefficient matrix, as described in Section 9.16, which computes the transformation of the incident light field as it interacts with the distorted optic. These coupling matrices are inserted into the matrix describing the interferometer behaviour, as described in Section 2.3, giving the higher-order mode content at any position within the simulated setup. For well behaved optics, such as those installed in gravitational wave detectors, we can accurately model realistic distortions of the beam with a finite number of modes, as long as we chose a good Gaussian basis (eigenmode) to work in. The further from the ideal eigenmode the more modes you will require to converge to the correct result. It has been our experience that the best eigenmode is most often that of the optical cavity, as given by the mirror curvatures and positions.

11.4 Simulation methods

Optical simulation tools inherently involve approximations in order to provide meaningful results within practical computation times. The most common approximation when modelling laser interferometers for gravitational wave detectors is assuming a paraxial beam, allowing the use of a small angle approximation. There are two distinct simulation methods based on the paraxial approximation:

1. Modal decomposition with light fields expressed as linear combinations of Gaussian modes (solutions to the paraxial wave equation).
2. Fast Fourier Transform (FFT) methods where the light fields are represented as finite numerical grids which are propagated through an optical system in the Fourier domain.

The most important aspects of performing simulations with modal models are: 1) to use the correct Gaussian basis for the higher-order mode expansion; and 2) to use enough higher-order modes to recreate distortions of the wavefront. A good choice of Gaussian basis means a small number of modes should be sufficient to reproduce the distortions we expect in gravitational wave interferometers. In this review we make extensive use of the modal simulation FINESSE, see Appendix A. Other modelling tools for laser interferometers are based on, or are using, Gaussian modes [62, 157]. The FFT method formed the beginning of optical modelling in the gravitational wave community and has been used extensively since [161, 28, 59, 94]. Both methods contain further approximation, in the addition to assuming paraxial behaviour. In the case of modal models this arises from the finite number of modes. In FFT codes the finite grid size and resolution restricts the accuracy. A balance between accuracy and efficiency often determines the number of modes and grid dimensions used in these simulations. Some powerful tools have been developed which can use modal and FFT based methods internally [45, 171].

11.5 Mirror surface maps

In order to analyse the effects of mirror surface distortions we require numerical descriptions of actual mirrors. In this section we discuss several methods for representing mirror surface data, with some methods more suited to use in numerical simulations, whilst others allow an analytic analysis.

A powerful way to implement mirror surface distortions in modal models is by using a numerical grid representing the surface height of the real mirrors, known as *mirror maps*. This is how mirror surface effects are implemented in the interferometer simulation FINESSE [70, 72]. The surface data is given as a function over the x - y surface of the optic and can either be measured data from a

real mirror or data generated from mathematical functions, for example, describing the expected thermal distortion of a mirror. Mirror map data can be produced for surface height, reflectivity, transmissivity or absorption over the surface of the optic. Unless otherwise notes we use the generic term mirror map referring to surface height. Figure 11.2 shows an example of a mirror map depicting the surface of an end test mass produced for Advanced LIGO (shown here with any curvature, tilt and offset removed) to illustrate the kinds of distortions of the mirrors we can expect. Note the nano-metre scale of the graph, which is typical for mirrors in such high-precision interferometers. We can also see that the central region of the mirror exhibits less surface height variation. Again this is expected, as the requirements on the polishing of the mirror are much more stringent in the centre of the optic where the beam is most intense.

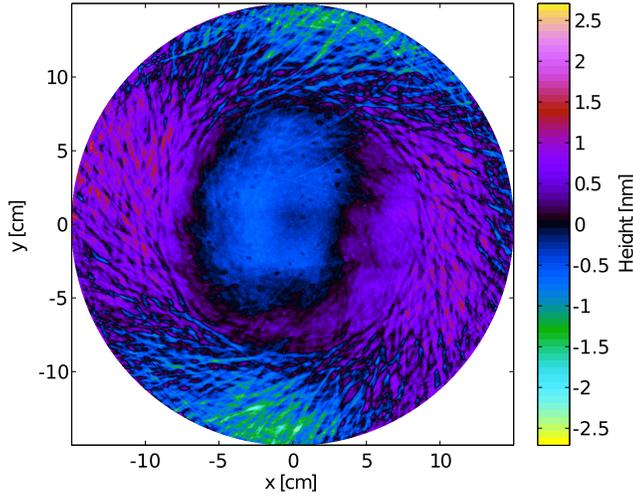


Figure 11.2: Mirror map describing the measured surface height of an Advanced LIGO end test mass, before coating. The curvature, tilt and average offset of the surface are removed from the data, to clearly show the higher-order distortions of the mirror surface.

Essentially mirror maps characterise the surfaces by their deviation from a perfect sphere. The terms for any piston, tilt and curvature are then expressed by individual numbers (amplitude, angle and radius of curvature respectively). This raises the problem of how to optimally define these low-order features for a distorted surface. For example, measuring the curvature of a real mirror is done by fitting a spherical function to the measured surface data, minimising the difference between our reference function, the spherical surface Z_{sphere} , and our data, the mirror map Z_{map} . This is represented by minimising the function

$$f = \int_0^{2\pi} \int_0^R [Z_{map} - Z_{sphere}]^2 r \, dr \, d\theta \quad (11.7)$$

where R is the radius over which we are measuring. For a typical distorted surface the result can vary greatly with R . We could chose R to be the radius of the mirror, taking a measure of the curvature over the whole surface. However, if we consider the part of the mirror over which the Gaussian beams interact we can measure the curvature the beam ‘sees’ more effectively. Therefore, it makes sense to weight our fitting routine using a Gaussian function:

$$f = \int_0^{2\pi} \int_0^R W(r, \theta) [Z_{map} - Z_{sphere}]^2 r \, dr \, d\theta \quad (11.8)$$

where $W(r, \theta)$ is the weighting function, in most cases given by the intensity distribution of the fundamental Gaussian beam and R is the radius of the mirror. The plots in figure 11.3 show different estimates for the curvature of a mirror surface measured over different regions and using a weighted fitting function. There is a significant difference in curvature depending on the area

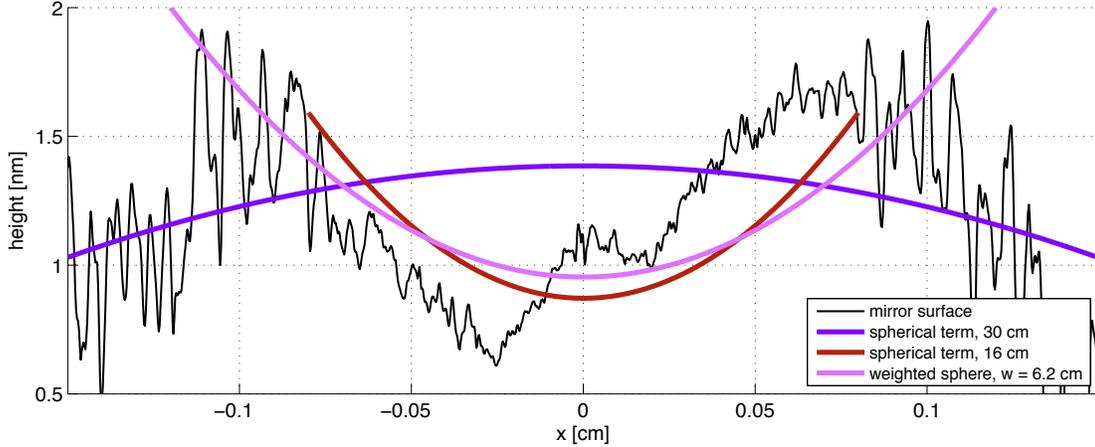


Figure 11.3: Estimates of mirror curvature over different radii and with different weightings for a distorted mirror surface. 3 different estimates for the curvature of the surface are shown, 1) the spherical term over the whole 30 cm; 2) the spherical term over the central 16 cm region; and 3) the Gaussian weighted curvature of the surface, using a weighting beam size of $w = 6.2$ cm.

or weighting used and we must take care to use the correct measurement for accurate models. It is especially important for modal simulations that the correct curvature is measured, as this will determine the cavity eigenmodes, and the basis of our calculations. In most cases working in the cavity eigenmodes ensures efficient simulations: accurate results using the least higher order modes. The offset and tilt can be measured using similar methods, specifying the area or weighting with which to measure the defect.

11.6 Spectrum of surface distortions

It is desirable to have an analytic description of a mirror surface, not just numeric data, for example, to categorise specific types of distortion. A commonly used method for describing surfaces is to use a spectrum over spatial frequencies or wavelengths. The distortion of a surface along the x -axis at a specific spatial frequency, F , can be written as:

$$Z(x) = A \cos(2\pi Fx + \phi) \quad (11.9)$$

where A is the amplitude of the distortion and ϕ is the initial phase of the distortion. For a purely cosine distortion $\phi = 0$ and for purely sine $\phi = \frac{\pi}{2}$. A generic distortion can be described by a sum of sines and cosines at different frequencies, F_n :

$$Z(x) = \sum_n A_n \cos(2\pi F_n x + \phi_n) \quad (11.10)$$

The coefficients and phases can be extracted from a discrete Fourier transform of measured surface data $z(x)$, calculated using a Fast Fourier Transform (FFT) algorithm:

$$Z(k) = \sum_{n=0}^{N-1} z(n) \exp\left(-\frac{i 2\pi(k-1)(n-1)}{N}\right) \quad (11.11)$$

where N is the number of elements in z , and n and k are integer indices related to the spatial coordinate x and k and spatial frequency F respectively. This method can be adapted to a 2 dimensional surface, for example, by averaging a 2D Fourier transform into a single 1D amplitude spectrum, similar to the root mean squared (*rms*) for each spatial frequency. In figure 11.4 this analysis is shown for an Advanced LIGO mirror. From such an analysis we can identify what spatial frequencies are present or dominant in the mirror surfaces distortions. Low spatial

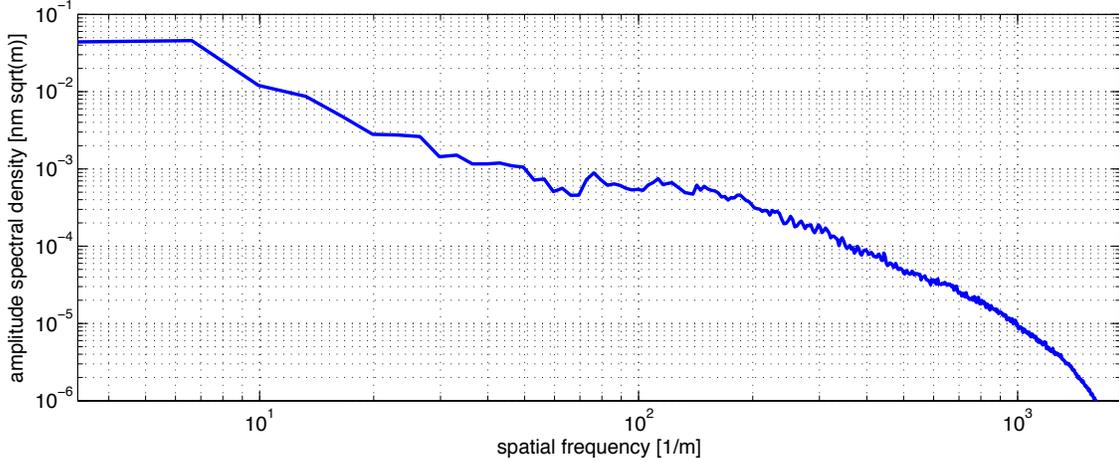


Figure 11.4: Amplitude spectral density of the different spatial frequencies present in the Advanced LIGO mirror map ETM08, calculated using a 2D FFT and computing a radial average. The offset, tilt and common curvature terms have been removed prior to this analysis.

frequency distortions correspond to the overall mirror shape, higher spatial frequencies refer to the *roughness* of the mirror. The amplitude of the lower spatial frequencies is significantly higher, as expected. Higher spatial frequencies occur naturally with smaller amplitudes but are also required to be very small in gravitational wave mirrors to reduce wide angle scattering out of the beam path.

11.7 Surface description with Zernike polynomials

A convenient model for describing the overall shape and low spatial frequency distortion of a mirror surface are Zernike polynomials. Zernike polynomials are a complete set of functions which are orthogonal over the unit disc and defined by radial index, n , and azimuthal index, m , with $m \leq n$. For any index m we have

$$Z_n^{+m}(\rho, \phi) = \cos(m\phi)R_n^m(\rho) \quad \text{the even polynomial} \quad (11.12)$$

$$Z_n^{-m}(\rho, \phi) = \sin(m\phi)R_n^m(\rho) \quad \text{the odd polynomial}$$

with ρ the normalised radius, ϕ the azimuthal angle and $R_n^m(\rho)$ the radial function

$$R_n^m(\rho) = \begin{cases} \sum_{h=0}^{\frac{1}{2}(n-m)} \frac{(-1)^h (n-h)!}{h! (\frac{1}{2}(n+m)-h)! (\frac{1}{2}(n-m)-h)!} \rho^{n-2h} & \text{for even } n-m \\ 0 & \text{for odd } n-m \end{cases} \quad (11.13)$$

This gives $n+1$ non-zero Zernike polynomials for each value of n (for $m=0$ the odd polynomial is zero). Some common optical features are described by the low order Zernike polynomials, as shown

in Figure 11.5. The simplest polynomials represent effects we are familiar with: offset (longitudinal tuning), tilt (misalignment) and curvature (mode mismatch). The higher n polynomials represent higher spatial frequencies.

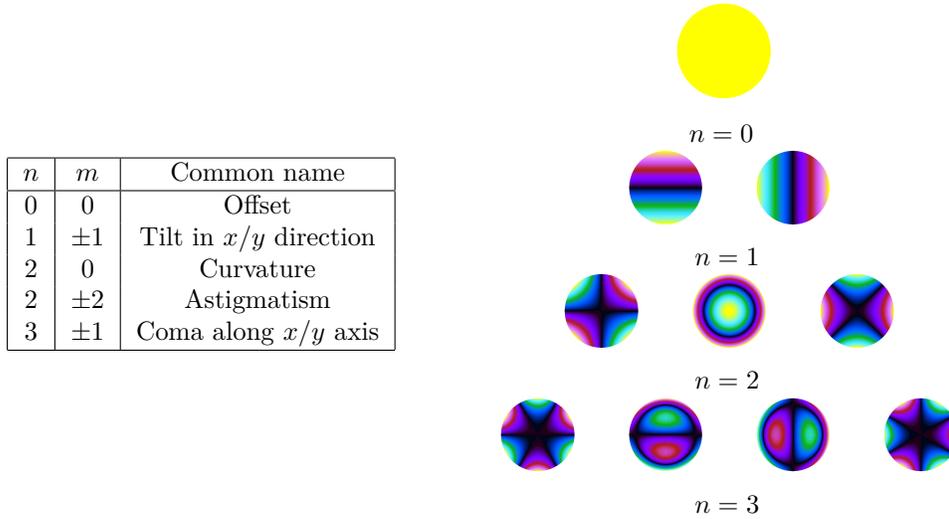


Figure 11.5: Plots of all the non-zero Zernike polynomials from $n = 0$ to $n = 3$. They go from odd polynomials with $m = -n$ on the far left to even polynomials with $m = n$ on the far right, in steps of 2. The colour scale represents negative surface heights with greens and blues, zero with black and positive surface heights with reds and purples.

Odd and even Zernike polynomials describe the same shape for given n and m , with a rotation of $\frac{90^\circ}{m}$ with respect to each other. A combination of the odd and even polynomials result in the same shape rotated by a given angle with an amplitude:

$$A_n^m = \sqrt{(A_n^{-m})^2 + (A_n^{+m})^2} \quad (11.14)$$

Any surface defined over a disc can be described as a sum of Zernike polynomials, in the same way any beam shape can be described as a sum of Gaussian modes, making these function suitable for the purposes of describing mirror surface distortions. Mirror surface data, Z_{map} , can be expressed as

$$Z_{\text{map}} = \sum_{n,m} A_n^m Z_n^m \quad (11.15)$$

where A_n^m is the amplitude of the relevant Zernike polynomial in the surface. In the approach taken here this amplitude has the same units as the the map data. We can analyse the surface data contained in mirror maps by decomposing the surface into Zernike polynomials, calculating the Zernike coefficients using an inner product and exploiting the orthogonal nature of the polynomials

$$\int_S Z_{\text{map}} (N_n^m)^2 Z_n^m dS = A_n^m (N_n^m)^2 \int_S Z_n^m Z_n^m dS = A_n^m \quad (11.16)$$

N_n^m is a normalisation factor which gives $\int_S (N_n^m Z_n^m)(N_n^m Z_n^m) dS = 1$ and has the form

$$N_n^m = \sqrt{\frac{2(n+1)}{(1+\delta_{m,0})\pi}} \quad (11.17)$$

Using numerical integration routines real surface data can be represented as a sum of Zernike polynomials. This is illustrated in figure 11.6, where an Advanced LIGO mirror map is recreated using low order Zernike polynomials ($n \leq 20$). The overall shape of the Zernike surface looks very

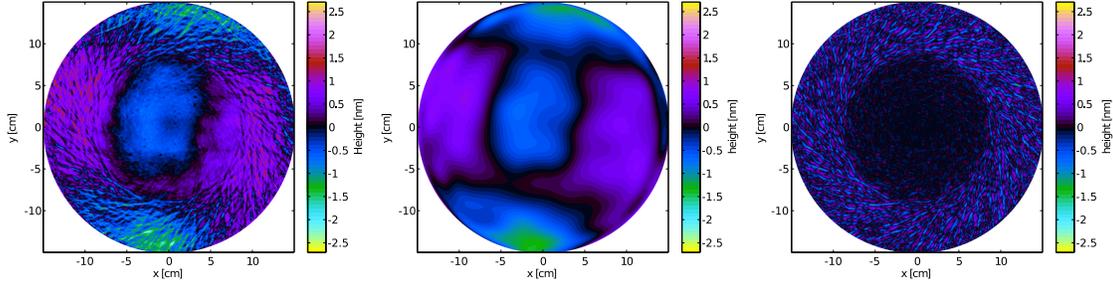


Figure 11.6: Representations of an Advanced LIGO mirror surface. **Left:** Original surface map over 30 cm region, with offset, tilt and curvature (Z_0^0) removed. **Centre:** Map recreated from Zernike polynomials with $n \leq 20$, representing the overall shape of the mirror. **Right:** Residual surface after the Zernike map is removed, showing the higher spatial frequencies.

similar to the original map, but lacks the high spatial frequencies. These are shown in the residual map which also illustrates the high polishing requirements for the central 16 cm region. Although high spatial frequencies can be represented by Zernike polynomials it is often convenient for mirror surface analysis to consider only the low order Zernike polynomials, with the rest of the mirror description contained in spectra of spatial frequencies. In figure 11.7 the spectrum of an Advanced LIGO mirror map is shown, as well as the spectra for Zernike maps recreated using polynomials up to a given order, illustrating how low order polynomials correspond to low spatial frequencies. Including more polynomials in our model tends towards the original map.

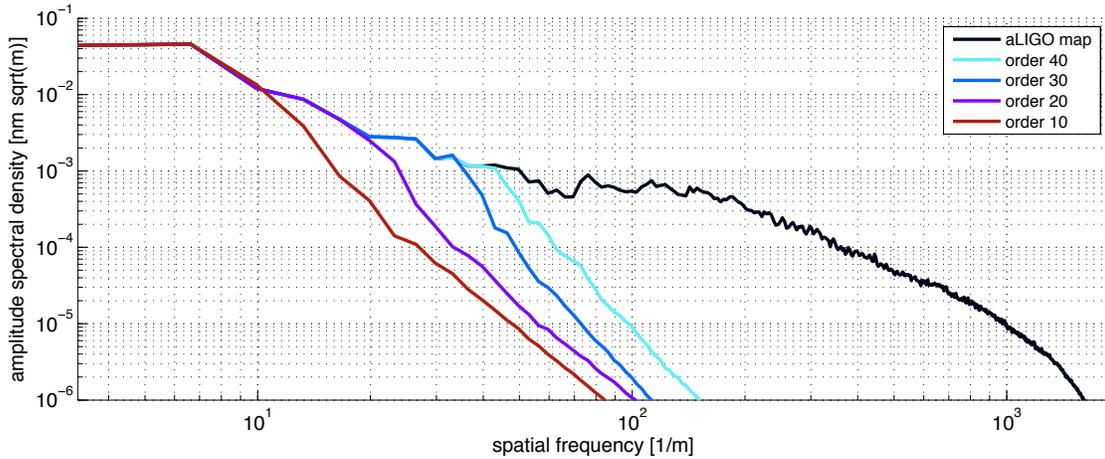


Figure 11.7: Spectra of spatial frequencies in different ETM08 maps. The spectrum for the original map is shown, as well as those for maps created from Zernike polynomials up to a given order. As more polynomials are added to the model the spectra tend to the original result.

11.8 Mode coupling due to mirror surfaces defects

In Section 11.3 the method for calculating coupling coefficients numerically, for a generic surface distortion, was discussed. For design of new laser interferometers we want tools to predict which types of distortions will couple light into which higher-order Gaussian modes. Such a tool would allow us to compute specific requirements for the distortions in optics for future detectors. For example, in [33] the proposal of a new input laser mode, LG₃₃, is analysed in terms of the performance of such a high-order mode with the current mirrors. This involves an analysis of the mirror shapes which will couple between LG₃₃ and other modes of the same order, as these modes have the potential to seriously degrade the performance. In such a case an analytic approach to coupling, where the distortions are described by functions such as the Zernike polynomials, is highly desirable.

Scattering into HOMs

In [168] Winkler presents an analytic approach to the scattering of light in the modal picture, taking the approach of describing a mirror surface using spatial frequencies and considering the x and y spatial components separately:

$$Z(x) = h_0 \cos\left(\frac{2\pi}{\Lambda}x + \phi\right) \quad (11.18)$$

where h_0 is the amplitude of the distortion and Λ is the spatial wavelength of the distortion. For symmetric distortions $\phi = 0$, for anti-symmetric $\phi = \frac{\pi}{2}$. The coupling from a particular spatial wavelength can be calculated using Hermite-Gauss modes and splitting them into separate x and y components (see equation 9.75). For the coupling in x we have

$$k_{n,n'} = \int_{-\infty}^{+\infty} U_n \exp(2ikZ)U_{n'}^* dx \quad (11.19)$$

Winkler took this approach, and an assumption of relatively small mirror surface distortions, to derive coupling coefficients for an incident HG₀₀ mode. Here we present this result and expand it for the case of a generic incident mode.

U_n is the x component of a Hermite-Gauss mode in the incident beam and $U_{n'}$ is the x component of a mode in the reflected beam.

$$U_n U_{n'}^* = \frac{1}{w} \sqrt{\frac{2}{\pi}} \frac{\exp(i(n-n')\Psi)}{\sqrt{2^{n+n'} n! n'}} H_n\left(\frac{\sqrt{2}x}{w}\right) H_{n'}\left(\frac{\sqrt{2}x}{w}\right) \exp\left(-\frac{2x^2}{w^2}\right) \quad (11.20)$$

Assuming the distortion of the surface is small compared to the wavelength of the light, a valid assumption when considering the mirrors of gravitational wave detectors, we can approximate

$$\exp(2ikZ) = 1 + 2ikZ \quad (11.21)$$

The integral becomes

$$\begin{aligned} I &= C \int_{-\infty}^{\infty} H_n(v) H_{n'}(v) \exp(-v^2) \cos\left(\frac{\sqrt{2}\pi w}{\Lambda}v + \phi\right) dv \\ &= C \cos(\phi) \int_{-\infty}^{\infty} H_n(v) H_{n'}(v) \exp(-v^2) \cos\left(\frac{\sqrt{2}\pi w}{\Lambda}v\right) dv \\ &\quad - C \sin(\phi) \int_{-\infty}^{\infty} H_n(v) H_{n'}(v) \exp(-v^2) \sin\left(\frac{\sqrt{2}\pi w}{\Lambda}v\right) dv \end{aligned} \quad (11.22)$$

where

$$C = \frac{2i k h_0 \exp(i(n-n')\Psi)}{\sqrt{\pi} \sqrt{2^{n+n'} n! n'!}} \quad \text{and} \quad v = \frac{\sqrt{2}x}{w} \quad (11.23)$$

These two integrals can be solved using these identities [80]

$$\begin{aligned} \int_0^\infty e^{-x^2} \sin(bx) H_p(x) H_{p+2m+1}(x) dx &= 2^{p-1} (-1)^m \sqrt{\pi} p! b^{2m+1} \exp\left(-\frac{b^2}{4}\right) L_p^{2m+1}\left(\frac{b^2}{2}\right) \\ \int_0^\infty e^{-x^2} \cos(bx) H_p(x) H_{p+2m}(x) dx &= 2^{p-1} (-1)^m \sqrt{\pi} p! b^{2m} \exp\left(-\frac{b^2}{4}\right) L_p^{2m}\left(\frac{b^2}{2}\right) \end{aligned} \quad (11.24)$$

for $b > 0$ and where $L(x)$ refer to the Laguerre polynomials. The first integral will refer to coupling where $n - n'$ is odd from asymmetric distortions (sine term) and the second refers to even $n - n'$ couplings from symmetric distortions (cosine term). The integral solutions look very similar to the amplitude of the Laguerre-Gauss modes

$$|U_{p,l}| = \frac{1}{W} \sqrt{\frac{2p!}{\pi(|l|+p)!}} \exp\left(-\frac{r^2}{W^2}\right) \left(\frac{\sqrt{2}r}{W}\right)^{|l|} \left|L_p^{|l|}\left(\frac{2r^2}{W^2}\right)\right| \quad (11.25)$$

Note that r and W are not the radial coordinate and beam spot size as in the definition of an LG mode, but related to the ratio of the beam size to the spatial wavelength, $\frac{w}{\Lambda}$. For a complete solution with the correct phase the sign of the Laguerre-polynomial should be included, as this disappears when taking the amplitude of the LG mode. Using these identities we have

$$\begin{aligned} I &= C 2^p \pi W \sqrt{\frac{p!(|l|+p)!}{2}} (\sqrt{2})^{|l|} |U_{p,l}| [\cos(\phi) \cos(|l|\frac{\pi}{2}) - \sin(\phi) \sin(|l|\frac{\pi}{2})] \\ &= C 2^p \pi W \sqrt{\frac{p!(|l|+p)!}{2}} (\sqrt{2})^{|l|} |U_{p,l}| \cos(\phi + |l|\frac{\pi}{2}) \end{aligned} \quad (11.26)$$

where

$$p = \min(n, n') \quad l = n - n' \quad \frac{r}{W} = \frac{\pi}{\sqrt{2}} \frac{w}{\Lambda} \quad (11.27)$$

The factors $\sin(|l|\frac{\pi}{2})$ and $\cos(|l|\frac{\pi}{2})$ come from the combination of the factors $(-1)^{|l|/2}$, $(-1)^{(|l|-1)/2}$ and the fact that the integral including the sine term is 0 for even $n - n'$ and integral including the cosine term is 0 for odd $n - n'$. For simplicity we set $W = \frac{\sqrt{2}}{\pi}$, which gives $r = \frac{w}{\Lambda}$, the ratio of the beam spot size to the wavelength of the spatial distortion. Finally substituting in the values for C and using $p + |l| = \max(n, n')$ and $n + n' = 2p + |l|$ gives

$$k_{n,n'}^1 = \delta_{n,n'} + \text{sign}\left(L_p^{|l|}(\pi^2 r^2)\right) \frac{2i k h_0}{\sqrt{\pi}} \exp(i l \Psi) |U_{p,l}(W = \frac{\sqrt{2}}{\pi})| \cos(\phi + |l|\frac{\pi}{2}) \quad (11.28)$$

adding in the sign of the Laguerre-polynomial to get the correct phase. The coupling between Hermite-Gauss modes of different orders is well expressed by this first order approximation, where the coupling is described with Laguerre-Gauss modes of order $n+n'$. This is illustrated in figure 11.8 where the first order analytical coupling is compared with the numerical solution of the coupling integral for $k_{2,6}$ over a range of spatial frequencies.

For coupling back into the same order ($n = n'$) we require up to second order, derived using the same method as described above. We have

$$k_{n,n'} \approx k_{n,n'}^1 - k^2 h_0^2 \delta_{n,n'} - \text{sign}\left(L_p^{|l|}(4\pi^2 r^2)\right) \frac{k^2 h_0^2}{\sqrt{\pi}} |U_{p,l}(W = \frac{1}{\sqrt{2}\pi})| \cos(2\phi + |l|\frac{\pi}{2}) \quad (11.29)$$

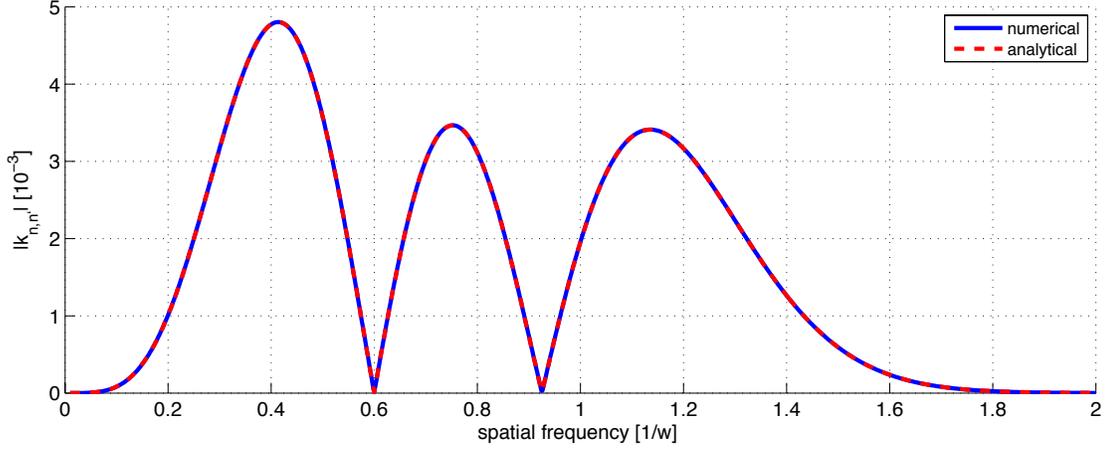


Figure 11.8: Comparison of the first order coupling approximation (analytical) with the numerical solution of the coupling between the x components of the Hermite-Gauss modes, U_2 and U_6 .

where the second order corrections are also described by Laguerre-Gauss modes of order $n + n'$ but with a beam spot parameter half the size of the that of the first order coupling.

Figure 11.9 illustrates the scattering into a range of higher order modes for different spatial frequency mirror distortions. Two examples are given, an incident mode with $n = 0$ and an incident mode with $n = 3$. For low frequency spatial distortions the coupling occurs mostly into low orders. For higher spatial frequencies, where the wavelength of the spatial distortion is smaller than the beam spot size, coupling occurs into a vast number of higher order modes. In practice the amplitude of spatial distortions is not constant across the spectrum of spatial wavelengths, as is illustrated here ($h_0 = 1$ nm), but decreases with spatial frequency. In realistic simulations and in experiments the low order modes dominate, so much so that we can model gravitational wave interferometers well with a finite number of modes.

Typically individual $k_{n,n'}$ (where $n \neq n'$) are of the order 10^{-3} for 1 nm distortions. For

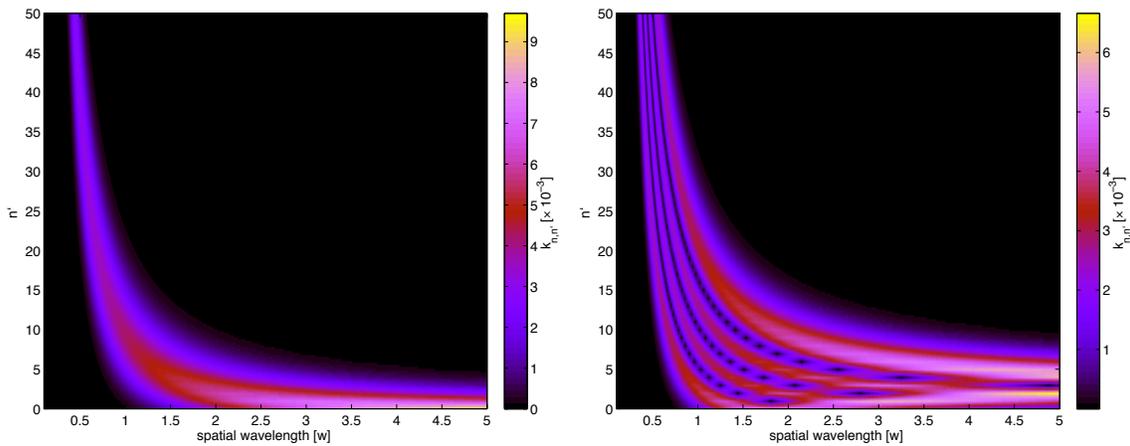


Figure 11.9: The scattering into higher order modes across a range of spatial distortions (frequencies) for an incident U_0 mode (left) and an incident u_3 mode (right).

coupling back into the same mode $k_{n,n} \approx 1$ for small distortions. We would therefore expect coupling from $\text{HG}_{n,m}$ to $\text{HG}_{n,m'}$ or $\text{HG}_{n',m}$ would be significantly larger than coupling where both indices change, as these are of the order 10^{-3} rather than 10^{-6} .

Zernike coupling

Common analysis using spatial frequencies involves taking a statistical approach: performing numerous simulations using randomly generated realisations of mirror surfaces to determine the higher order mode behaviour for a mirror conforming to a particular spectrum of spatial frequencies. Such an approach for an LG_{33} mode investigation is detailed in [91]. Here we present an analytic approach which aims to identify the exact shapes which couple between different modes.

An analysis of mirror surface distortions in terms of Zernike polynomials is complementary to the approach of describing the shape of the beam in terms of Gaussian modes. Both methods deal with the overall shape of the beam/mirror by expressing them as sums of orthonormal functions. Now we have an analytic representation of mirror surface distortions we can try and formulate a relation between particular mirror shapes and their impact on the beam. The coupling on reflection from a mirror described by an individual Zernike polynomial, Z_n^m , is

$$k_{p,l,p',l'}^{n,m} = \int_S U_{p,l} \exp(2i k Z_n^m) U_{p',l'}^* dS \quad (11.30)$$

where $U_{p,l}$ is a mode in the incident beam and $U_{p',l'}$ is a mode in the reflected beam. The Laguerre-Gauss modes are most suited for this analysis as they, like the Zernike polynomials, are naturally described in cylindrical coordinates. Assuming the distortions are small enough that the beam parameter remains unchanged, the product of the two LG fields is

$$U_{p,l} U_{p',l'}^* = \frac{1}{w^2} \frac{2}{\pi} \sqrt{\frac{p! p'!}{(|l|+p)! (|l'|+p')!}} \exp(i(2p+|l|-2p'-|l'|)\Psi) \left(\frac{\sqrt{2}r}{w}\right)^{|l|+|l'|} L_p^{|l|} \left(\frac{2r^2}{w^2}\right) L_{p'}^{|l'|} \left(\frac{2r^2}{w^2}\right) \exp\left(-\frac{2r^2}{w^2}\right) \exp(i\phi(l-l')) \quad (11.31)$$

To simplify the integral we can simplify the expansion of $\exp(2i k Z)$. Assuming $2kZ$ is small we can use the approximation

$$\exp(2i k Z) \approx 1 + 2i k Z \quad (11.32)$$

This is a valid approximation for advanced gravitational wave interferometers, where the scale of distortions is not expected to exceed the order of 1 nm. $Z = 10$ nm and a wavelength of 1064 nm gives $2kZ \approx 0.1$. Making this approximation the coupling coefficients are simplified

$$k_{p,l,p',l'}^{n,m} = \int_S U_{p,l} U_{p',l'}^* (1 + 2i k Z_n^m) = \delta_{p,p'} \delta_{l,l'} + \int_0^{2\pi} \int_0^R U_{p,l} U_{p',l'}^* (2i k Z_n^m) r dr d\phi \quad (11.33)$$

where $\delta_{p,p'} \delta_{l,l'}$ refers to coupling back into the same mode. The integral to calculate is over the surface with $r \rightarrow \infty$, as Laguerre-Gauss modes are orthogonal over this range. But since the integrand is proportional to the Zernike polynomial, S becomes the Zernike surface as $Z_n^m(\frac{r}{R} > 1) = 0$, with R the Zernike radius.

Both Zernike polynomials and Laguerre-Gauss modes can be separated into there angular and radial parts. The angular integrand is

$$\exp(i\phi(l-l')) \begin{cases} \cos(m\phi) & \text{even } Z_n^m \\ \sin(m\phi) & \text{odd } Z_n^m \end{cases}$$

Considering the even Zernike polynomial the angular integral becomes

$$I_\phi = \int_0^{2\pi} e^{i\phi(l-l')} \frac{e^{im\phi} + e^{-im\phi}}{2} d\phi = \left[\frac{e^{i\phi(l-l'+m)}}{2i(l-l'+m)} + \frac{e^{i\phi(l-l'-m)}}{2i(l-l'-m)} \right]_0^{2\pi} \quad (11.34)$$

As $e^{i0} = e^{iN \times 2\pi} = 1$, for integer N , the integral is equal to 0. The only combination of Zernike polynomials and Laguerre-Gauss modes to give a non-zero result occurs when one of the exponentials disappears before the integration takes place. This occurs for $l-l'+m=0$ or $l-l'-m=0$. These same conditions also give the only non-zero results for the odd Zernike polynomials. This forms a *coupling condition* between the azimuthal indices of the shape of the mirror, the Zernike polynomial (m), and the LG modes such a mirror couples between (l/l'). This is summarised as

$$m = |l - l'| \quad (11.35)$$

Unless this condition is satisfied the coupling between modes l and l' is 0, to first order. This condition allows quick identification of the modes which are created from certain mirror shapes. It also agrees with previous work on misalignment and mode-mismatch. For example, the Zernike polynomial Z_1^1 corresponds to misalignment and couples from the fundamental mode into $LG_{0,\pm 1}$, the order 1 Laguerre-Gauss modes. Similarly the curvature polynomial, Z_2^0 , couples from $LG_{0,0}$ to the order 2 mode $LG_{0,1}$.

Using this condition we can integrate with respect to ϕ :

$$I_\phi = \begin{array}{ll} 0 & m \neq |l - l'| \\ \pi & \text{even } Z_n^m \\ \pm i \pi & \text{odd } Z_n^m \\ 2\pi & m = |l - l'| = 0 \end{array} \quad (11.36)$$

The next step is to solve the radial integration. Making the variable substitution $x = \frac{2r^2}{w^2}$ the coefficient becomes

$$k_{p,l,p',l'}^{n,m} = \delta_{p,p'} \delta_{l,l'} + i k \frac{I_\phi}{\pi} \sqrt{\frac{p!p'!}{(|l+p|!(|l'|+p')!)} \exp(i\Delta o\Psi)} \int_0^X x^{\frac{|l|+|l'|}{2}} L_p^{|l|}(x) L_{p'}^{|l'|}(x) \exp(-x) Z_n^m \left(\sqrt{\frac{x}{2}} w \right) dx \quad (11.37)$$

with $X = \frac{2R^2}{w^2}$ and $\Delta o = 2p + |l| - 2p' - |l'|$, the difference in order between the incident and reflected modes. The integrand is in the form of $f(x)g(x)$, where $f(x)$ is a polynomial of x whose order depends on the mode and Zernike indices, and $g(x) = \exp(-x)$. This integration is solved using the incomplete gamma function, $\gamma(n, x) = \int_0^x t^{n-1} e^{-t} dt$ [80], which for integer $n = 1, 2, \dots$ is

$$\gamma(n, x) = (n-1)! \left[1 - e^{-x} \sum_{m=0}^{n-1} \frac{x^m}{m!} \right] \quad (11.38)$$

Substituting in this solution to the integral we have the final solution to this coupling approximation as

$$k_{p,l,p',l'}^{n,m} = \delta_{p,p'} \delta_{l,l'} + A_n^m i k \frac{I_\phi}{\pi} \sqrt{p!p'!(p+|l|)!(p'+|l'|)!} \\ \times \sum_{i=0}^p \sum_{j=0}^{p'} \sum_{h=0}^{\frac{1}{2}(n-m)} \frac{(-1)^{i+j+h}}{(p-i)!(p'-j)! (|l|+i)! (|l'|+j)! i! j!} \frac{1}{X^{\frac{1}{2}(n-2h)}} \\ \times \frac{(n-h)!}{\left(\frac{1}{2}(n+m)-h\right)! \left(\frac{1}{2}(n-m)-h\right)! h!} \gamma\left(i+j-h + \frac{1}{2}(|l|+|l'|+n)+1, X\right) \quad (11.39)$$

It is worth noting that the first order direct coupling described here is proportional to the amplitude of the Zernike polynomial, A_n^m .

As with the Winkler scattering approximation detailed above we require up to second order in the exponential expansion to accurately calculate the coupling back into the incident mode. We have:

$$\begin{aligned} k_{p,l,p',l'}^{n,m} &= \int_S u_{p,l} \exp(2i k Z_n^m) u_{p',l'}^* dS \\ &\approx \delta_{p,p'} \delta_{l,l'} + k_{p,l,p',l'}^{n,m,1} + k_{p,l,p',l'}^{n,m,2} \end{aligned} \quad (11.40)$$

where $k_{p,l,p',l'}^{n,m,1}$ is the first order coupling as given by equation 11.39 and $k_{p,l,p',l'}^{n,m,2}$ is the second order coupling, given by:

$$k_{p,l,p',l'}^{n,m,2} = \int_S u_{p,l} u_{p',l'}^* (-2k^2 (Z_n^m)^2) dS \quad (11.41)$$

As with the first order coupling we can split the integration into the radial and angular parts. The angular integration is:

$$I_\phi = \int_0^{2\pi} \frac{\cos^2(m\phi)}{\sin^2(m\phi)} \exp(i\phi(l-l')) d\phi \quad (11.42)$$

Taking the even Zernike polynomial we have:

$$\int_0^{2\pi} \frac{1}{4} (e^{im\phi} + e^{-im\phi})^2 e^{i\phi(l-l')} d\phi = \int_0^{2\pi} \frac{1}{4} [e^{i\phi(l-l'+2m)} + e^{i\phi(l-l'-2m)} + 2e^{i\phi(l-l')}] d\phi \quad (11.43)$$

As with the angular integration for the first order coupling, a non-zero value is only achieved when the exponentials disappear before the integration. We therefore have conditions for non-zero second order coupling:

$$\begin{aligned} 2m &= |l-l'| \\ \text{or} \\ l &= l' \end{aligned} \quad (11.44)$$

Integrating with respect to ϕ we have:

$$I_\phi = \begin{cases} 0 & 2m \neq |l-l'|, \quad l \neq l' \\ \frac{\pi}{2} & 2m = |l-l'|, \quad \text{even } Z_n^m \\ -\frac{\pi}{2} & 2m = |l-l'|, \quad \text{odd } Z_n^m \\ \pi & l = l', \quad m \neq 0 \\ 2\pi & l = l', \quad m = 0 \end{cases} \quad (11.45)$$

For the radial integration we make the variable substitution $x = \frac{2r^2}{w^2}$ which gives:

$$\begin{aligned} k_{p,l,p',l'}^{n,m,2} &= -2k^2 \frac{1}{w^2} \frac{2I_\phi}{\pi} \sqrt{\frac{p!p'}{(|l+p|!|l'+p'|!)}} \exp(i\Delta\phi) \psi \\ &\int_0^X x^{\frac{|l+l'|}{2}} L_p^{|l|}(x) L_{p'}^{|l'|}(x) \exp(-x) \left[R_n^m \left(\sqrt{\frac{x}{2}} \frac{w}{R} \right) \right]^2 \sqrt{\frac{x}{2}} w dx \end{aligned} \quad (11.46)$$

where $\Delta\phi$ is the difference in order between the incident and coupled mode and $X = \frac{2R^2}{w^2}$ is the limit of the exponential. As with the first order coupling we use the lower incomplete gamma

function, $\gamma(a, x) = \int_0^x t^{a-1} e^{-t} dt$ to get the final solution:

$$k_{p,l,p',l'}^{n,m,2} = -\frac{I_\phi}{\pi} k^2 A^2 \sqrt{p!p'!(p+|l|)!(p'+|l'|)!} \exp(i\Delta\phi) \psi$$

$$\sum_{i=0}^p \sum_{j=0}^{p'} \sum_{h=0}^{\frac{1}{2}(n-m)} \sum_{g=0}^{\frac{1}{2}(n-m)} \frac{(-1)^{i+j+h+g} (n-h)!(n-g)! X^{h+g-n}}{(p-i)!(p'-j)! (|l|+i)! (|l'|+j)! i! j! h! g!} \quad (11.47)$$

$$\frac{\gamma(i+j+n-h-g + \frac{1}{2}(|l|+|l'|)+1, X)}{(\frac{1}{2}(n+m)-h)! (\frac{1}{2}(n+m)-g)! (\frac{1}{2}(n-m)-h)! (\frac{1}{2}(n-m)-g)!}$$

Using this derivation of the second order term, combined with our previous derivation of the first order coupling, the amplitude/ power coupled back into the incident mode can be calculated. In the left panel figure 11.10 the power scattered out of an LG₀₀ mode incident on an mode-mismatched mirror is plotted against the relative beam size. The larger the beam size the more of the distortion the beam ‘see’ and hence the more power is scattered into higher order modes. In the right panel shows the power coupled from an LG₃₃ mode incident on an astigmatic mirror into 2 other order 9 modes, LG₄₁ and LG₂₅. In both cases the analytic coupling approximation and numerical results agree.

This coupling approximation has proved particularly useful as it allows for quick identification of the sources of coupled modes. For example, this approximation was used in the case of an investigation into the compatibility of the LG₃₃ mode with the current advanced detector mirrors [33]. The main cause of worse performance, compared to the fundamental mode, is coupling into modes of the same order (in the case of LG₃₃ order 9). This approximation means we can quickly identify which mirror distortions will couple between LG₃₃ and other order 9 modes, and hence which mirror shapes need stricter requirements to produce LG₃₃ compatible mirrors. Table 7 summarise the shapes which couple (to first order) into each order 9 mode from LG₃₃. Only shapes with specific azimuthal structures cause coupling between specific modes, and here we see only even azimuthal indices (m) will cause problems for the LG₃₃ mode. Using this approximation mirror requirements were derived to produce an equivalent performance between an injected LG₃₃ laser mode and a fundamental mode.

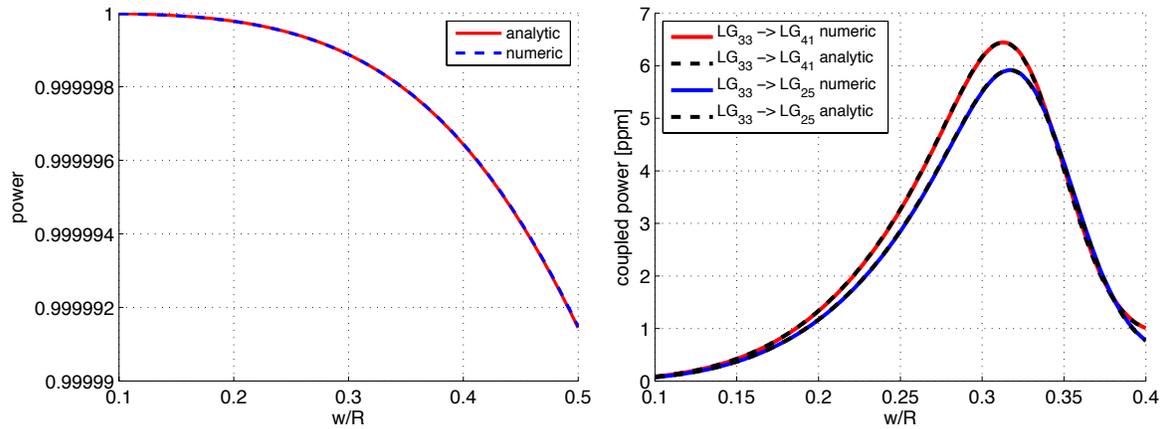


Figure 11.10: Plots illustrating relationship between power scattered into higher order modes by a curvature mismatched mirror and the relative beam size. **Left:** Power scattered out of an incident 00 mode. **Right:** Power scattered from LG₃₃ into 2 other order 9 modes, LG₄₁ and LG₂₅. For both plots both the analytical coupling approximation and numerical results are shown.

mode (p,l)	4,1	2, 5	4, -1	1, 7	3, -3	0, 9	2, -5	1, -7	0, -9
m	2	2	4	4	6	6	8	10	12

Table 7: Azimuthal index (m) of the Zernike shapes required to cause first order coupling from an incident LG₃₃ mode into each of the other order 9 modes.

11.9 Efficient coupling matrix computations with multiple distortions

Evaluating coupling coefficients numerically is a computationally expensive task if an analytic solution is not known for a particular distortion to the beam shape. Analytic solutions such as those from Bayer-Helms [23] for mode-mismatches and misalignments (see Section 9.16) provide a fast way to compute the matrices for such effects. However, if a surface defect or some other distortion is also applied to a mirror this can require full numerical integration which is very slow, especially if the simulation varies the mode-mismatch or alignments. Different distortions can mathematically be separated into multiple coupling coefficient matrices, allowing a fast method to solve one which varies often, like mode-mismatch, and a slow numerical integration which often need only be performed once.

Consider two general distortions to the beam A and B , these could tilts, apertures, surface defects, etc.

$$k_{MN} = \iint_{-\infty}^{\infty} U_N(x, y, q_1)A(x, y)B(x, y)U_M^*(x, y, q_2)dx dy. \quad (11.48)$$

What we want to be able to do is separate the effects as the coupling caused by the distortion A might be analytically solveable and variable and whereas B may take along time to recompute and is constant, therefore we only want to compute it once. This is the typical scenario when considering simulating varying mode-mismatches and static surface distortions or apertures on a mirror for example.

Such a coupling coefficient computation can be represented as vectors in a Hermite-Gaussian polynomial basis - for convenience we write for shorthand $|U_N(x, y, q_1)\rangle \rightarrow |N, q_1\rangle$.

$$k_{MN} = \langle N, q_1|A(x, y)B(x, y)|M, q_2\rangle, \quad (11.49)$$

$$|N, q\rangle = \begin{bmatrix} 0 \\ \vdots \\ U_N^*(x, y, q) \\ \vdots \\ 0 \end{bmatrix}, \quad \langle N, q| = [0 \quad \dots \quad U_N(x, y, q) \quad \dots \quad 0], \quad (11.50)$$

$$\langle N, q_1|M, q_2\rangle = \iint_{-\infty}^{\infty} U_N(x, y, q_1)U_M^*(x, y, q_2)dx dy \quad (11.51)$$

$$\hat{I}_{MN} = \sum_M^{\infty} \sum_N^{\infty} |N, q\rangle\langle M, q| = \sum_{N, M=N}^{\infty} \left(\iint_{-\infty}^{\infty} U_N(x, y, q)U_N^*(x, y, q)dx dy \right) \quad (11.52)$$

We then define two new vectors and the inner product between them

$$k_{MN} = \langle v_N | v_M \rangle \quad (11.53)$$

$$|v_M, q_2\rangle = \begin{bmatrix} 0 \\ \vdots \\ U_M^*(x, y, q_2)B(x, y) \\ \vdots \\ 0 \end{bmatrix}, \quad \langle v_N, q_1| = [0 \quad \dots \quad A(x, y)U_N^*(x, y, q_1) \quad \dots \quad 0] \quad (11.54)$$

We then insert the identity matrix, formed by a complete orthonormal basis set of modes,

$$k_{MN} = \langle v_N, q_1 | \hat{I} | v_M, q_2 \rangle \quad (11.55)$$

$$= \langle v_N, q_1 | \left(\sum_L^\infty |L, q_l\rangle \langle L, q_l| \right) | v_M, q_2 \rangle \quad (11.56)$$

$$= \sum_L^\infty \langle v_N, q_1 | L, q_l \rangle \langle L, q_l | v_M, q_2 \rangle \quad (11.57)$$

$$= \sum_L^\infty \langle N, q_1 | A(x, y) | L, q_l \rangle \langle L, q_l | B(x, y) | M, q_2 \rangle \quad (11.58)$$

$$(11.59)$$

From this we can see that we now have two separate inner products and a sum over the infinite number of Hermite basis functions. In practice this is limited to a certain number of modes of interest. The last line is identical to a matrix multiplication where each inner product represents the element of a matrix,

$$k_{MN} = \sum_L \langle N | A(x, y) | L \rangle \langle L | B(x, y) | M \rangle \quad (11.60)$$

$$= \sum_L \hat{A}_{NL} \hat{B}_{LM} = (\hat{A}\hat{B})_{MN} \quad (11.61)$$

Where each matrix is now coupling coefficients for each distortion. The expansion beam parameter q_l can in theory be set to any value; however the computational requirements can be reduced if it is chosen sensibly. Remember that a mode-mismatch is present if $q_1 \neq q_2$, so if q_l is chosen to be either q_1 or q_2 the mode-mismatch is present in only one of the matrices. This is beneficial as coupling coefficient matrices are Hermitian if there is no mode-mismatch. Thus only one half of the matrix elements need to be computed – when solving via numerical integration this can save a great deal of time. There is also the issue of matrix commutation, $A(x, y)$ and $B(x, y)$ are interchangeable in the derivation thus it appears $[\hat{A}, \hat{B}] = 0$, which is a surprising result seeing as the functions can be any arbitrary values. In practice it is found that commutation errors are only present if the functions are not described using enough higher-order-modes. If significant amount of information is lost in modes that are not considered, commutation errors are likely to occur.

11.10 Clipping by finite apertures

Another spatial affect present in real interferometers is the finite size of the optics. Often in simulations with Gaussian modes or plane waves there is some intrinsic assumption that the optics are infinite. In reality the size of the optics is carefully chosen, optimising between large optics to contain the power of the incident beams and smaller optics to reduce the impact of thermal noise.

A finite aperture in the path of a laser beam will produce higher-order modes. However, in the case of well designed interferometers, such as gravitational wave detectors, the effect can often be modelled as just a loss of power in the fundamental mode, so called *clipping loss*. In such interferometers the size of the optics are chosen such that they are large enough, compared to the beam size, that very little power is lost over the edges. For an LG mode this loss is given by:

$$l_{clip} = 1 - \int_S |u_{p,l}|^2 dS \quad (11.62)$$

The integral represents the normalised power reflected by a mirror with a finite aperture. For a large mirror the loss is effectively 0. The loss for LG modes is derived as:

$$l_{clip} = 1 - p!(p + |l|)! \sum_{m=0}^p \sum_{n=0}^p \frac{(-1)^{n+m}}{(p-n)!(p-m)!} \times \frac{1}{(|l+n|!(|l+m|)!n!m!)} \gamma(|l+n+m+1, X) \quad (11.63)$$

where $X = \frac{2R^2}{w^2}$ and γ is the lower incomplete gamma function. Generally a clipping loss of the order 1 ppm (10^{-6}) is desirable.

Generic analytic coupling coefficients describing clipping at a circular aperture is available in [162].

11.11 Cavity modes of many shapes

A realistic cavity has an resonate mode which deviates slightly from that of a pure Gaussian eigenmode: i.e. it is a perfect resonator for a slightly distorted Gaussian beam, as described by the distorted cavity mirrors. As an example we consider the case of an astigmatic cavity and the Laguerre-Gauss modes. An astigmatic cavity has differing curvatures along the x and y axes. The Laguerre-Gauss modes, with their cylindrically symmetric properties, are not eigenmodes of such a system. In cases with a large astigmatism *frequency splitting* can be observed, where an injected Laguerre-Gauss mode is broken down into the eigenmodes of the cavity. For an astigmatic cavity these eigenmodes are astigmatic Hermite-Gauss modes, which can be separated in x and y

$$u_{n,m}(x, y, z) = u_n(x, z, R_{C,x})u_m(y, z, R_{C,y}) \quad (11.64)$$

with different curvature associated with the x and y . The frequency splitting phenomenon has its cause in the difference in Gouy phase accumulated in x and y for the different modes. The total Gouy phase is:

$$\varphi_{n,m} = (n + \frac{1}{2})\psi_x(z) + (m + \frac{1}{2})\psi_y(z) \quad (11.65)$$

This results in slightly different resonance frequencies for different Hermite-Gauss modes of the same order. Consider for instance the Laguerre-Gauss mode LG₃₃, an order 9 mode. As described in Section 9.11 this mode can be described as a sum of order 9 Hermite-Gauss modes. In the case where this mode is injected into an astigmatic cavity, instead of a single clean resonance peak at the order 9 resonance, we see a spread of resonances corresponding to the different Hermite-Gauss modes. This is illustrated in figures 11.11 and 11.12 where the individual higher-order resonances are split across the resonances of the astigmatic Hermite-Gauss modes: the eigenmodes of such a cavity.

This example is illustrative of a more general effect: the fact that the resonant modes of a distorted cavity will differ from a perfect Gaussian mode. We also note that the finite size of the cavity mirrors makes the situation more complex, for example it affects the orthogonality of the cavity eigenmodes [146].

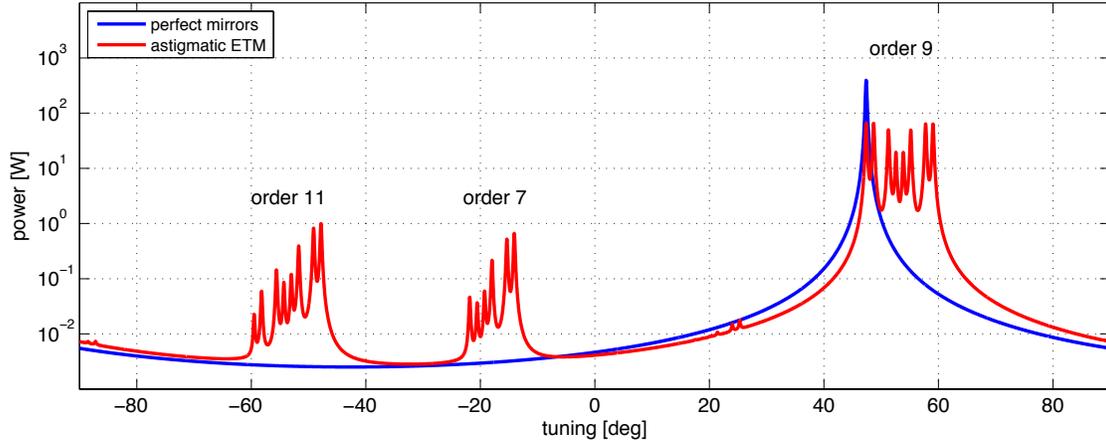


Figure 11.11: Scan of a cavity injected with an LG_{33} mode. The results for a cavity with perfectly spherical mirrors show a single resonance for the order 9 mode. For an astigmatic cavity the high order resonances are split into the resonances of the astigmatic Hermite-Gauss modes, the eigenmodes of the cavity. Coupling into orders 7 and 11 caused by the astigmatism also display this frequency splitting.

12 Acknowledgements

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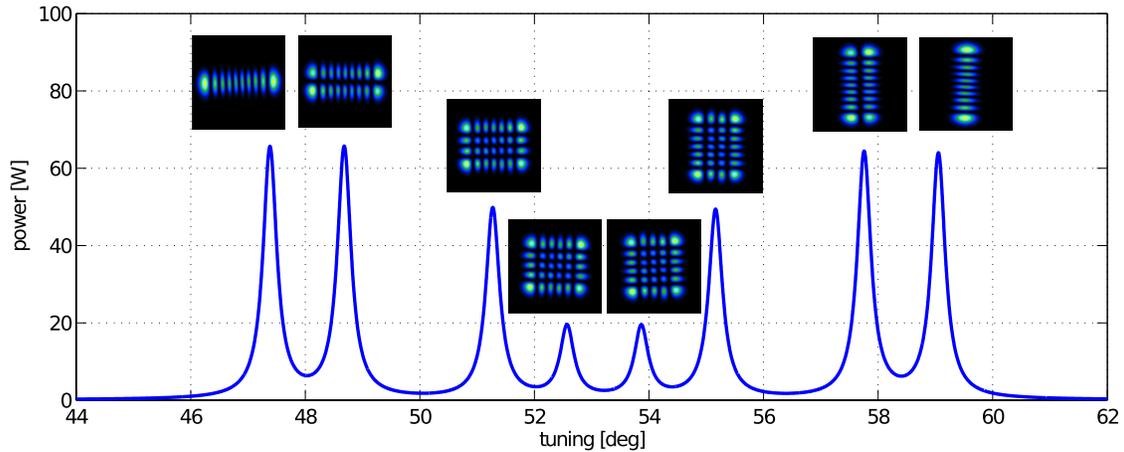


Figure 11.12: Scan over the order 9 peak in an astigmatic cavity injected with an LG_{33} mode. The peak is split into the resonances of the order 9 Hermite-Gauss modes, the eigenmodes of the cavity.

A The Interferometer Simulation Finesse

Throughout this document we have provided a number examples using the interferometer simulation FINESSE [70, 72]. We encourage the reader to obtain FINESSE and to learn its basic usage by running the included example files (and by making use of its extensive manual). The program has been designed to allow the analysis of arbitrary, user-defined optical setups. In addition, it is easy to install and use. Therefore FINESSE is well suited to study basic optical properties. The FINESSE input files provided in this article are in most cases very simple and illustrate single concepts in interferometry. We believe that even a FINESSE novice should be able to use them as starting points to play and explore freely, for example, by changing parameters, or by adding further optical components. This type of ‘numerical experimentation’ can provide insights similar to real experiments, supplementing the understanding through a mathematical analysis with experience and intuitions.

Free software:

FINESSE is a free software package developed and maintained by some of us (AF and DB): we provide free downloads of binaries for Linux, Windows and Macintosh computers online at: <http://www.gwoptics.org/finesse/>. The code is available under the GPLv2 license and does not require any commercial software (such as Matlab) to compile and run.

Development:

FINESSE is a numerical simulation written in the C language; it is actively developed to fix bugs as they are found and to add new features required to simulate new interferometric systems. The recent updates allow modelling of suspended optics that are effected by radiation pressure of the laser light as well as quantum effects such as squeezing and vacuum noise. We are further developing PYKAT [42], a Python based toolbox to extend the use of FINESSE, in particular for automating tasks and data post-processing.

Gravitational wave research:

The FINESSE development started in 1997 to support the design and commissioning of the gravitational wave detector GEO 600 and FINESSE has remained the standard simulation software of that project. Since then FINESSE has been developed continuously to meet the new challenges of the interferometric gravitational wave detectors world wide such as LIGO, Virgo and KAGRA¹⁸. FINESSE provides a fast and versatile tool that is optimised for the type of low-noise, steady state laser interferometry used by gravitational-wave detectors.

¹⁸A list of scientific papers and reports citing FINESSE is provided in [70].

B NEW: Advanced LIGO optical layout

In this review the specific example of Advanced LIGO has been used to illustrate the operation of an advanced gravitational wave detector. In this section the layout and parameters of Advanced LIGO are presented, with a brief description of the motivation for some of the key parameters.

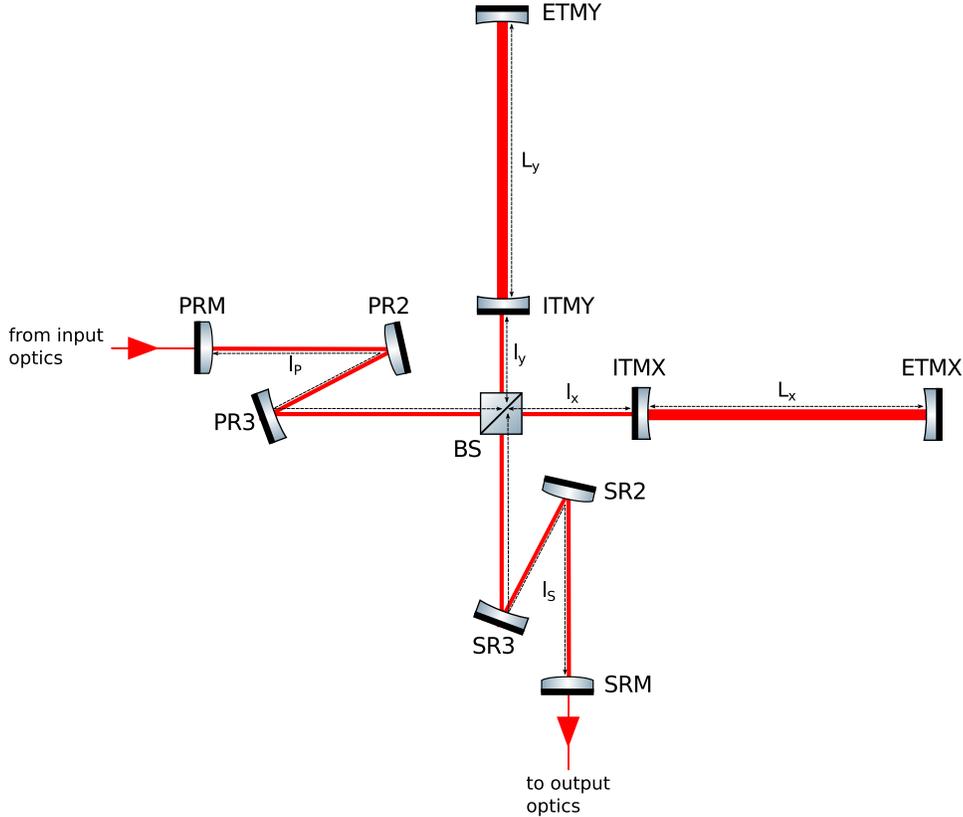


Figure B.1: Optical layout of the central interferometer of Advanced LIGO, a dual recycled Michelson interferometer with Fabry-Perot arm cavities. The input beam comes from an input mode cleaner, which filters the beam of unwanted spatial and frequency components. The output beam is sent to an output mode cleaner before it reaches the final detection photodiode. The arm cavities are characterised by the input and end test masses (ITMs and ETMs). Each recycling cavity consists of 3 mirrors, the power/signal recycling mirror (PRM/SRM) and two folding mirrors (PR2/SR2 and PR3/SR3). The distances between the key optics are labelled: the distance between the recycling mirrors and the beam-splitter (l_P and l_S), the short Michelson arms (l_x and l_y) and the arm cavity lengths (L_x and L_y).

B.1 Advanced LIGO configuration

Figure B.1 shows the configuration of the central interferometer of Advanced LIGO, a dual recycled Michelson interferometer with Fabry-Perot arm cavities. The interferometer is characterised by the parameters and performance of the different subsystems of the interferometer: the arm cavities, power recycling cavity, signal recycling cavity and the Michelson.

Table 8 summarises the design optical parameters of the key components of Advanced LIGO: the input and end test masses (ITM and ETM) and the power and signal recycling mirrors (PRM and SRM). A 50:50 beam-splitter is used and the design assumes a loss per optic of 37.5 ppm. The additional mirrors which make up the recycling cavities are highly reflective with a transmittance on the order of 1 ppm.

Parameter	Value
ITM T	1.4%
ETM T	5 ppm
PRM T	3.0%
SRM T	20%
BS T	50%
Arm cavity finesse	450
Loss per optic	37.5 ppm

Table 8: Summary of the key optical parameters of the Advanced LIGO design. The transmittance, T , of the main mirrors is quoted (in % or parts-per-million, ppm), as well as the expected loss per optic and the finesse of the arm cavities. The reflectivity of the mirrors is simple calculated as $R = 1 - T - L$, where T is the transmittance and L is the loss for each mirror [15]. Note that these parameters represent the design at a certain period in time and not always the exact parameters of the currently operating detectors. For example at the time of writing the transmittance of the installed SRM mirror is $\approx 35\%$.

As well as the optical properties the response of an interferometer is also characterised by it’s geometric parameters, such as the lengths of the arm cavities. Table 9 summarises the key lengths of the Advanced LIGO design: the lengths of the arm and recycling cavities. Also included is the Schnupp asymmetry length, a small difference in the short Michelson length of the x and y arms.

Length	Symbol	Value [m]
Power recycling cavity	$L_{\text{PRC}} = l_P + \frac{l_x + l_y}{2}$	57.656
Signal recycling cavity	$L_{\text{SRC}} = l_S + \frac{l_x + l_y}{2}$	56.008
Arm cavity	$L_x = L_y$	3994.5
Schnupp asymmetry	$l_{\text{Sch.}} = l_x - l_y$	0.050

Table 9: Key lengths of the Advanced LIGO design. The length of the recycling cavities ($L_{\text{PRC}}/L_{\text{SRC}}$) is the average distance between the recycling mirror (PRM or SRM) and the ITMs (using the average of the short Michelson arms for the distance from the BS and ITM, $\frac{l_x + l_y}{2}$). The arm cavity length is the distance between the highly reflective surfaces of the ITM and ETM (L_x/L_y). Finally, the Schnupp asymmetry, $l_{\text{Sch.}}$, is the difference between the short Michelson arms $l_x - l_y$ [15]. Figure B.1 shows a diagram of the Advanced LIGO layout which illustrates these lengths.

B.2 Choice of parameters

Above the parameters of Advanced LIGO as used in models throughout this review are summarised. In this section we provide a brief description of the motivation behind the choice of specific parameters. The majority of the parameters and arguments presented in this section are taken from [1].

Arm cavity finesse

The first consideration is the arm cavities. The length of the arms is set to ~ 4 km, from the existing LIGO infrastructure. This gives a free spectral range of 37.5 kHz. The choice of the reflectivity of the mirrors, or the finesse of the arm cavities, will impact other aspects of the design, so is chosen with care. The decision to have ~ 800 kW circulating in the arms (during high power operation) was made early on, in order to reduce shot noise in the interferometer, the limiting noise source at most frequencies for initial LIGO. A combination of parameters determine this intra-cavity power: input laser power, power recycling gain and arm cavity finesse; the finesse was designed to be 450 [75].

PRM transmission

The transmission of the power recycling mirror (PRM) is carefully chosen to be close to impedance matched with the Fabry-Perot Michelson, ensuring maximum power coupled into the interferometer and close to zero reflected. This requires some knowledge or estimate of the loss per mirror, which the design states should not be greater than 37.5 ppm per optic. In figure B.2 the power coupled into the interferometer for different PRM transmissions is modelled, considering different mirror losses [1]. A PRM transmission of 3% was chosen, giving slight over-coupling for 37.5 ppm losses but providing robustness against greater losses and the potential to detect error signals in reflection. It should be noted that most of the power is ‘transmitted’ through the losses in the arms, rather than through the end mirrors.

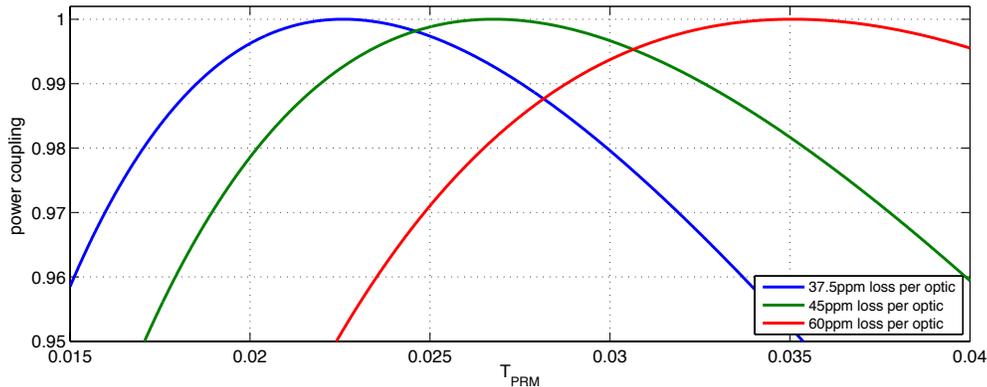


Figure B.2: Power coupled into an Advanced LIGO interferometer versus power recycling mirror transmission. The power coupled is simulated for 3 different values of scattering loss per optic, 37.5 ppm (nominal value), 45 ppm and 60 ppm.

Recycling cavity lengths

The choice of lengths for the power and signal recycling cavities are closely linked to the control scheme of Advanced LIGO. This involves injecting 2 pairs of control sidebands into the interferometer, at two different frequencies. The 2 sidebands have (design) frequencies of $f_1 = 9099471$ Hz and $f_2 = 5 \times f_1 = 45497355$ Hz, which are chosen to be anti-resonant in the arm cavities when the carrier is resonant (i.e. they are reflected by the arm cavities) and to avoid coinciding with any higher order mode resonances in the arms.

In the case of Advanced LIGO both sidebands must be resonant in the power recycling cavity when it is locked to the carrier. This puts a strict condition on the PRC length:

$$L_{PRC} = \left(N + \frac{1}{2}\right) \frac{c}{2f_1} \quad (\text{B.1})$$

The factor of $\frac{1}{2}$ is included as the sidebands are 180° out of phase with the carrier, as the carrier enters the arm cavities whilst the sidebands do not. A power recycling cavity length of 57.6557 m ($N = 3$) was chosen to be compatible with the opto-mechanical layout for a stable recycling cavity [1]. The signal recycling cavity length was chosen to be resonant for f_2 but not for f_1 , i.e. [1]

$$L_{SRC} = M \frac{c}{2f_2} \neq Q \frac{c}{2f_1} \quad (\text{B.2})$$

where M and Q are integers. An SRC length of 56.0084 m was chosen [1].

For control of Advanced LIGO one of the sidebands should exit the Michelson into the signal recycling cavity and eventually the output port. However, in a Michelson where the short arms between the beam-splitter and ITMs (l_x/l_y) are the same length the dark fringe for the carrier will also be the dark fringe for the sidebands. In order for one of the sidebands (f_2) to leak into the signal recycling cavity we need some asymmetry between the two arms, the so-called *Schnupp asymmetry*, $l_{Sch} = l_x - l_y \neq 0$ [90]. In the case of Advanced LIGO a Schnupp asymmetry of 5 cm was a compromise between maximising the coupling of f_2 into the signal recycling cavity for two different cases: broadband signal recycling and slightly detuned signal recycling (optimised for neutron star – neutron star in-spiral (NS – NS) signals).

Mode-matching

The curvatures of the highly reflective mirror surfaces and distances between individual mirrors determine the size and shape of the resonating beams. The individual cavities in the detector need to be well mode matched to maximise the power build up and avoid high contrast defects.

The eigenmode of the arm cavities is selected to produce large beams at the ITM (5.3 cm) and ETM (6.2 cm) to reduce thermal noise, with slightly smaller beams at the ITM due to lower thermal noise (fewer coating layers) and to prevent scattering into the recycling cavities. The curvatures are also carefully selected for a specific Gouy phase to avoid higher order modes easily ringing up in the arms: $R_C = 1934$ m (ITM) and $R_C = 2245$ m (ETM).

In initial LIGO the power recycling cavity was marginally unstable, enhancing the power in higher order modes in the control sidebands and causing problems for control [82]. To avoid this in Advanced LIGO the interferometer was designed with stable recycling cavities: folded cavities which do not share the arm cavity eigenmode [13], see section 10.7. These cavities consist of 3 mirrors, the primary recycling mirrors (PRM/SRM) and two additional mirrors to shape and direct the beam (PR2/SR2 and PR3/SR3). The curvatures and positions of the mirrors are chosen to ensure good mode matching into the arm cavities and to achieve a good spacing between higher order resonances (see section 10.7).

The mode matching of the beams between the recycling cavities and arms is complicated by thermal effects, specifically thermal lensing and the change in mirror curvatures. Although this will be corrected by thermal compensation systems [167] it was decided to match the recycling cavities to the arms in the presence of 50 km lenses in the ITMs, as expected for an input power of ~ 12.5 W with coating absorptions of 0.5 ppm [15]. This will potentially mitigate the use of TCS at low power. In the end the cavities were designed for a 50 km lens inside the substrate (effective 34.5 km lens) corresponding to 18 W input power.

B.3 Degrees of freedom

In figure B.3 a simplified diagram of the Advanced LIGO dual recycled configuration is shown, with the lengths which require control labelled. The microscopic degrees of freedom associated with these lengths are:

- **CARM** Common-mode arm motion, $\text{CARM} = L_x + L_y$. This tunes the average length of the arm cavities and is used to keep the arms on resonance.
- **PRCL** Power recycling cavity length, $\text{PRCL} = l_p + \frac{l_x + l_y}{2}$. The power recycling cavity is operated on resonance to maximise the power coupled into the central interferometer.
- **MICH** Michelson arm length, $\text{MICH} = l_x - l_y$. MICH controls the short arms of the Michelson (between the ITMs and beam-splitter) and determines the fringe at the output port. Generally the Michelson is operated on the dark fringe.
- **DARM** Differential arm motion, $\text{DARM} = L_x - L_y$. This controls the difference in length of the two arm cavities and is used to get the best interference between the two arms at the dark port.
- **SRCL** Signal recycling cavity length, $\text{SRCL} = l_s + \frac{l_x + l_y}{2}$. Used to control the operation of the signal recycling cavity. The operating point of SRCL depends on the mode of operation of the interferometer. It can be tuned for a particular frequency of gravitational wave or for broadband operation.

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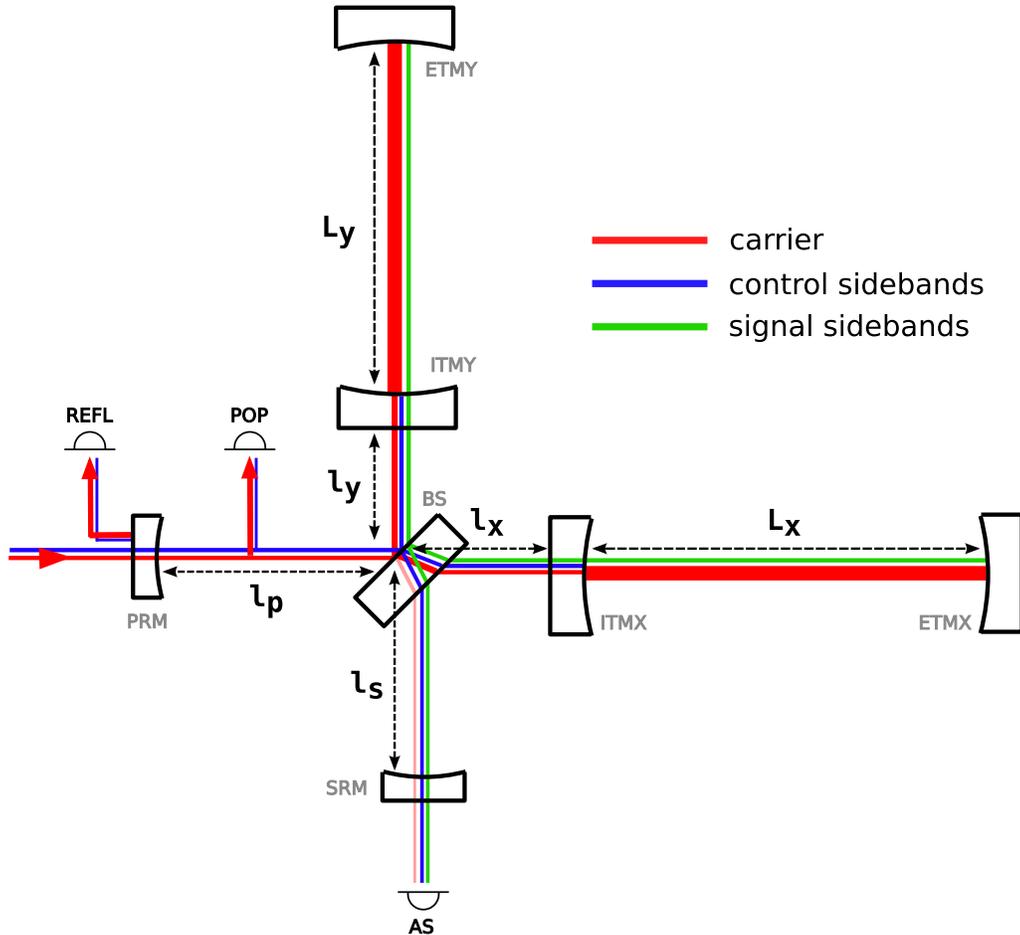


Figure B.3: Simplified layout of the dual recycled Fabry-Perot Michelson of Advanced LIGO, illustrating the fields inside the interferometer. All main mirrors are shown: power and signal recycling mirrors (PRM and SRM); input test masses (ITMX and ITMY); end test masses (ETMX and ETMY); and the central beam-splitter. Also shown are the locations of various photodiodes: REFL (reflected port), POP (power recycling pick off port) and AS (anti-symmetric port). The paths of the different light fields in the interferometer are shown. The carrier resonates inside the arm cavities and power recycling cavity, with the Fabry-Perot Michelson tuned close to the carrier dark fringe. A small amount of carrier light leaks into the anti-symmetric port due to a small DC offset. The RF sidebands used for control resonate in the power recycling cavity but are reflected from the arms. The Michelson is not at the dark fringe for the control sidebands and they appear in the signal recycling cavity and at the Michelson output. The signal sidebands generated by a gravitational wave originate in the arm cavities and then exit the Michelson through the anti-symmetric port.