LASER INTERFEROMETER GRAVITATIONAL WAVE OBSERVATORY - LIGO -

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Technical Note

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CO2 RIN coupling to DARM for aLIGO TCS

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1 Introduction

The coupling of CO2 laser intensity noise to DARM is described in detail in Section 2.8.5 of Stefan Ballmer's thesis. To convert this analysis to aLIGO, we must account for the change in the TCS configuration between eLIGO and aLIGO. In eLIGO, the TCS laser actuated on the HR surface of the ITM (within the arm cavity). In aLIGO, the TCS laser actuates on an AR surface of the compensation plate (within the PRC).

The difference allows us to ignore the surface thermal expansion of the optic, equation 2.36, and simply use equation 2.37 as a measure of the total change in optic thickness. The total displacement noise is given by this modified version of equation 2.38:

$$\Delta z(x,y) = \frac{\pi}{2F} \left[(n-1)(1+\eta)\alpha + \frac{dn}{dT} \right] \frac{1}{2\pi i f C \rho} p(x,y) \operatorname{RIN}(f)$$
 (1)

where RIN is the relative intensity noise. The mean displacement noise, $\langle \Delta z \rangle$, is given by the integral of $\Delta z(x,y)$ over the entire optic weighted by the intensity of the carrier laser beam profile.

$$\langle \Delta z \rangle = (\dots) \frac{\int I(x,y) \, p(x,y) \, dx \, dy}{\int I(x,y) \, dx \, dy}, \tag{2}$$

where the total power P is given by:

$$P = \int p(x, y) \, dx \, dy \tag{3}$$

2 Central heating

2.1 Central heating coupling

For central heating, the beam on the test mass is described by the following equation:

$$p_{cent}(r) = \begin{cases} P n_{cent} \exp\left(-2\frac{r^2}{w_{cent}^2}\right) & : r < a_{cent} \\ 0 & : r \ge a_{cent} \end{cases}$$

where:

$$n_{cent} = \frac{2}{\pi w_{cent}^2} \frac{1}{1 - \exp\left(\frac{-2a_{cent}^2}{w_{cent}^2}\right)} \tag{4}$$

For aLIGO TCS central heating, the following values apply:

Description	Symbol	Value
CO2 central beam radius	w_{cent}	215 mm
CO2 central mask radius	a_{cent}	97 mm
Specific heat capacity of CP	C	740 J/kg/K
Density of CP	ρ	2196 kg/m^3
Refractive index of CP	n	1.45
Poisson ratio of CP	η	0.17
Finesse of arm cavity	F	450
Thermo-refractive coefficient	$\frac{dn}{dT}$	$8.6E-6~K^{-1}$
Coefficient of thermal expansion	α	$0.55E-6~K^{-1}$

For aLIGO central heating, this translates to:

$$\langle \Delta z \rangle_{cent} = 1.2 \times 10^{-15} \,\mathrm{m} \, \left(\frac{100 \,\mathrm{Hz}}{f} \right) \, \left(\frac{P}{1 \,\mathrm{Watt}} \right) \mathrm{RIN}(f)$$
 (5)

2.2 Central heating alignment

Generally, the CO2 laser beam is not concentric with the IFO beam on the test mass after initial alignment.

The CO2 intensity noise coupling to DARM can be used to fine-tune the alignment of the central heating beam to the interferometer mode. This is done by injecting a large oscillation into the intensity of the AOM, observing the resulting peak in the DARM spectrum, and then adjusting the alignment of the CO2 laser beam in real-time to maximize the injected signal in DARM.

We can maximize the coupling to DARM by:

- Lowering the frequency of the injected signal. This is really only effective in frequency regimes where the DARM signal is flat. We recommend 85Hz.
- Increasing the absolute power onto the CP. We recommend using 100mW (this is small enough to inject a signal but not large enough to change the lens in the CP to such a point that the IFO becomes inoperable).
- Increasing the magnitude of the injected signal on the AOM. A RIN of 0.05 is the what we recommend.

As the CO2 central heating beam is scanned across the CP surface, the overlap integral in Equation 6 becomes:

$$\langle \Delta z \rangle = (\dots) \frac{\int I(x,y) \, p(x+xc,y+yc) \, dx \, dy}{\int I(x,y) \, dx \, dy},\tag{6}$$

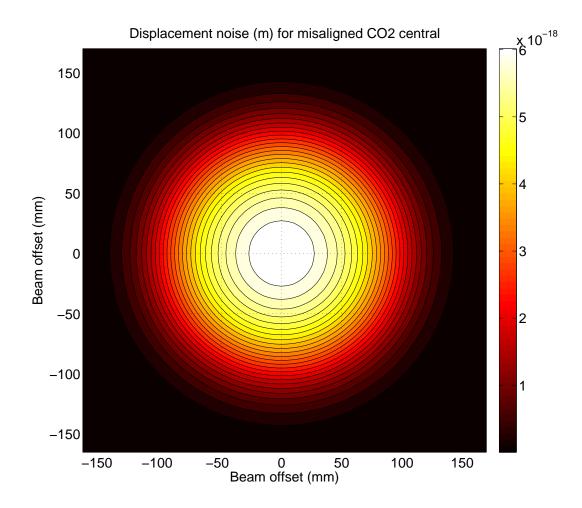


Figure 1: Model of the displacement noise amplitude in DARM for a CO2 central heating beam scanned across the ITM. Power = 100 mW, frequency = 85 Hz, RIN = 0.05.

3 Annular heating

3.1 Annular heating coupling

The optimum annular heat distribution, described in LIGO-T0900217-v2, is shown in the figure below. The data is at the end of this Technical Note.

The average intensity is, for 1 W of input power:

$$\langle p \rangle = \frac{\int r I(r) p(r) dr}{\int r I(r) dr}$$
$$= 11 \text{ W/m}^2$$
 (7)

Therefore, the annular heating coupling is:

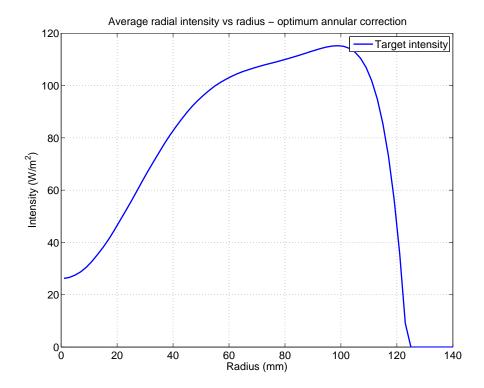


Figure 2: Optimum annular intensity to correct for residual thermal lensing from self absorption and ring heater. For $4.52\mathrm{W}$ of applied power

$$\langle \Delta z \rangle_{cent} = 3.3 \times 10^{-16} \,\mathrm{m} \, \left(\frac{100 \,\mathrm{Hz}}{f} \right) \, \left(\frac{P}{1 \,\mathrm{Watt}} \right) \mathrm{RIN}(f)$$
 (8)

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Radius[mm]	p(r)	[W/m^2]
1.0000	26.25	27
5.0000	27.53	10
9.0000	30.51	18
13.0000	35.37	41
17.0000	41.23	14
21.0000	48.31	41
25.0000	55.66	58
29.0000	63.42	74
33.0000	70.82	96
37.0000	77.91	45
41.0000	84.21	30
45.0000	89.77	37
49.0000	94.42	:03
53.0000	98.21	65
57.0000	101.23	16
61.0000	103.54	85
65.0000	105.35	72
69.0000	106.75	16
73.0000	107.97	61
77.0000		
81.0000	110.27	07
85.0000	111.54	75
89.0000	112.91	86
93.0000	114.21	21
	115.12	
	114.97	
105.0000		
109.0000	106.88	81
113.0000	94.80	
117.0000	72.84	
121.0000	35.67	
125.0000		0