

**WASHINGTON SITE  
LEFT ARM STATIONS  
ACCEPTANCE TEST REVIEW DATA PACKAGE**

**CONTRACT NO:** PC 175730  
**PSI DOCUMENT NO:** V049-1-169, Rev. 0  
**PROGRAM I.D.:** LIGO VACUUM EQUIPMENT  
**ISSUE DATE:** May 28, 1998  
**CDRL NO:** 07-1  
**APPROVAL STATUS:** A

**SUBMITTED TO:**

California Institute of Technology  
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Pasadena, CA 91125

**SUBMITTED BY:**

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## LIGO VACUUM EQUIPMENT

### WASHINGTON SITE LEFT ARM STATIONS ACCEPTANCE TEST REVIEW DATA PACKAGE

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- I. AS-BUILT DRAWINGS (B-SIZE)
- II. MAJOR COMPONENT END ITEM DATA PACKAGE (TABLE OF CONTENTS ONLY)
- III. WA SITE CONTRACTOR QA DATA (TABLE OF CONTENTS ONLY)
- IV. SUBVENDOR QA DOCUMENTATION (TABLE OF CONTENTS ONLY)

## **1.0 INTRODUCTION/SCOPE**

This data package details the material to be presented at the Acceptance Test Review Meeting for the LIGO Washington Site Left End and Left Mid Stations. The specific station test report should be reviewed for detailed information.

The data package is intended to meet the requirements of CDRL No. 7 for the Vacuum Equipment Contract (PC 175730).

Vacuum equipment design, installation and acceptance testing was documented in the Final Design Report (FDR) CDRL No. 3 dated November 16, 1996.

**2.0 MEETING AGENDA**

**LIGO VACUUM EQUIPMENT (V.E.)  
WASHINGTON SITE LEFT MID & END STATIONS  
ACCEPTANCE TEST REVIEW MEETING  
JUNE 18, 1998**

***Location: Marriott Hotel, Westborough, MA***

**AGENDA**

**8:30 a.m. Start**

- Introduction
- General Acceptance Test Plan
- Component Fabrication
- Major Purchased Components
- Site Component Installation
- Component/Subsystem Testing
- System Testing
- Vacuum Equipment Performance Summary
- C.A.A. Noise/Shock/Vibration Testing
- Open Punch List Items
- GNB Valve Modification
- Equipment Warranty
- Operating and Maintenance Manuals
- Disposition of Equipment
- Closing

### **3.0 PROJECT ACCEPTANCE TEST PLAN**

Vacuum equipment testing was planned to be split as follows:

- Component testing at PSI
- Vendor testing at major equipment vendors
- Equipment installation and alignment
- Equipment and subsystem testing
- Final system testing
- Noise/shock/vibration testing



#### **4.0 MAJOR COMPONENT FABRICATION (PSI)**

- Component design was documented in the Final Design Report and approved by LIGO.
- Component fabrication was executed in accordance with procedures defined in the FDR.
- Components were inspected to the design documents. All deviations were identified to LIGO and were subsequently approved.
- Component QA documentation are summarized in the End Item Data Packages (Attachment II).



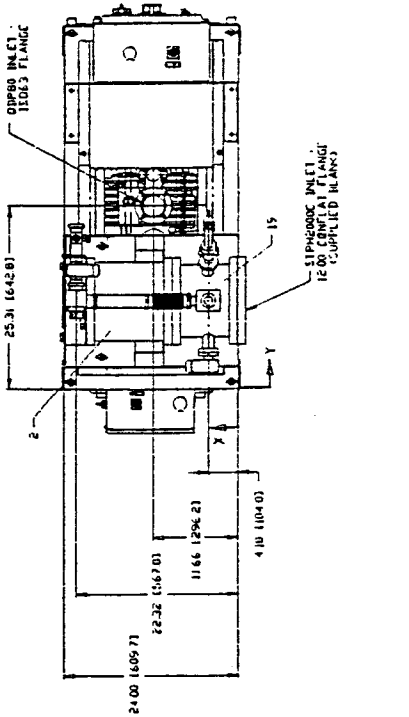
**TYPICAL END ITEM**  
**DATA PACKAGE CONTENTS – BSC**

1. BSC (Ranor) Quality Plan/Shop Traveler/Documentation Package
2. Material Test Reports
3. Certificate of Conformance for nozzles, small parts, small flanges (under 60) and bolting
4. Heat Treat Charts
5. Final Cleaning Certification
6. Final Vacuum Leak Reports
7. RGA/Bake-out Certification
8. Nonconformance Reports (use as is)
9. Certificate of Conformance

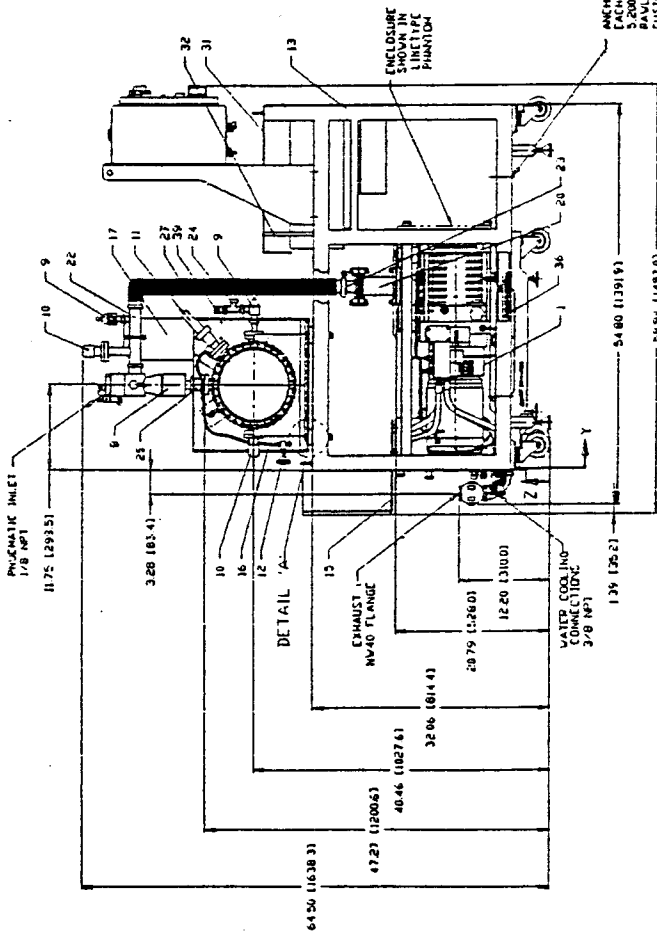
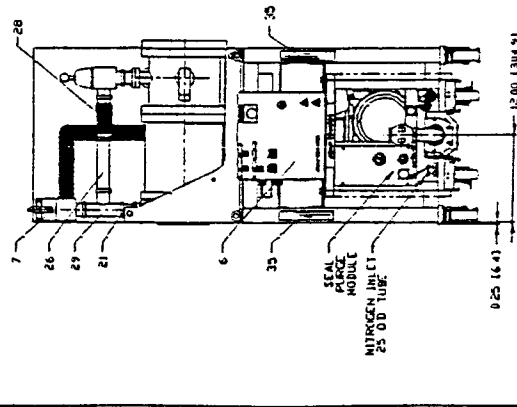
## **5.0 MAJOR PURCHASED COMPONENTS**

- Equipment procurement specifications were developed and approved by LIGO in the FDR.
- Equipment was purchased and tested to these specifications.
- Factory shop tests were conducted as specified in the FDR to verify critical system components (Edwards main turbo pump documents included as an example).

MAXIMUM SUPPLY PRESSURE	60 PSI
FLOWRATE	25 LPM
25 S/S VALVE FOR COMPRESSION	
VALVE PNEUMATIC	40-60 PSI
1/8 NPT CONN	
PROCESS COOLING WATER	
MAXIMUM PRESSURE	100 PSI
MAXIMUM PRESSURE DIFFERENTIAL	332 LPM
TYPICAL FLOWRATE AT 70°C	337 LPM
MAXIMUM FLOWRATE AT 55°C	20-21°C
RECOMMENDED SUPPLY TEMP	
3/8 NPT CONNECTION	
SUPPLY	SEE ELECTRICAL CONNECTION DIAGRAM AND WIRING DIAGRAM
FULL LOAD OPERATE	
RECOMMENDED SERVICE	
COMPACT TORQUE SPEC	
SIZE	1.44-2.8 x 1.25
2.75	1.44-2.8 x 1.25
12.00	2.75-4.4 x 2.00



DETAIL 'A'  
SCALE 25:100  
1-TYP 4 PLACES

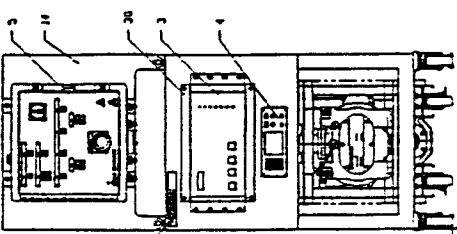


ANCHOR BOLTS ARE REQUIRED  
EACH BOLT SHALL HAVE A  
MINIMUM TENSILE MINIMUM YIELDING  
STRENGTH OF 100,000 PSI  
CUSTOMER SHALL SUPPLY BOLTS.

1	ENCLOSURE	1000	1000
2	VALVE	1000	1000
3	FLANGE	1000	1000
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100	FLANGE	1000	1000

NOTE: PARTS 21, 22, AND 23 ARE NOT SHOWN IN TOP VIEW, SO THAT 60990 PART 101 IS NOT SHOWN IN THE TOP VIEW. PARTS 21, 22, AND 23 SHOULD BE PLACED IN THE FOUR (4) UPPER CORNERS OF THE MAIN FRAME AND FOUR (4) ARE TO BE PLACED ON THE TURBO MOUNTING BRACKET (PART 1016).

INSTALL IDENTIFICATION TAGS AS SUPPLIED.



CUSTOMER SPEC.: V049-2-002

DATE	REV	DESCRIPTION
01/15/84	1	ISSUED FOR PRODUCTION
01/15/84	2	REVISED TO REFLECT CHANGES TO THE DRAWING
01/15/84	3	REVISED TO REFLECT CHANGES TO THE DRAWING
01/15/84	4	REVISED TO REFLECT CHANGES TO THE DRAWING
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01/15/84	99	REVISED TO REFLECT CHANGES TO THE DRAWING
01/15/84	100	REVISED TO REFLECT CHANGES TO THE DRAWING

11

**A.V.S. Air speed test procedure on STPH2000C/ODP80 Turbomolecular Pump Cart carried out for Process Systems International**

**1. Introductory Comments:**

- 1.1. The purpose of this test is to confirm that the STPH2000C/QDP80 Turbomolecular pump cart as supplied by Edwards High Vacuum International, performs to inlet pump speed specification as per V-049-2-002 rev 2 section 3.0 of a minimum of  $1400\text{ls}^{-1}$  at a pressure of  $1 \times 10^{-3}$  Torr and is capable of operating for extended periods of time at its maximum quoted inlet pressure of  $1 \times 10^{-1}$  Torr with water cooling of  $2.0 \text{ lmin}^{-1}$
- 1.2. The test performed will be following the American Vacuum Society AVS 4.1: Recommended procedure for measuring pumping speeds as revised in October 1986, see appendix 1
- 1.3. The method Chosen will be Method 3.1, flowmeter method, see appendix 1.
- 1.4. For the purpose of this test, N<sub>2</sub> will be used as the test gas.

**2. Apparatus**

- 2.1. Test dome see appendix 3
- 2.2. Edwards Model 1605, 5 channel Display/controller
- 2.3. Edwards Model 825 Mass flow controller 5 sccm calibrated for N<sub>2</sub>
- 2.4. Edwards Model 825 Mass flow controller 20 sccm calibrated for N<sub>2</sub>
- 2.5. Edwards Model 825 Mass flow controller 200 sccm calibrated for N<sub>2</sub>
- 2.6. Edwards Model 825 Mass flow controller 5lpm calibrated for N<sub>2</sub>
- 2.7. 4 branch MFC mounting manifold
- 2.8. Gas inlet tube
- 2.9. HPS model 937-120V60TR-CCTNA gauge system incorporating:
  - 2.9.1. HPS Series 937 system gauge controller
  - 2.9.2. 1 x SensaVac® Cold Cathode Gauge
  - 2.9.3. 2 x SensaVac® Pirani Gauge
  - 2.9.4. Calibrated HPS SensaVac® Cold Cathode Gauge, see appendix 6
- 2.10. N<sub>2</sub> test gas, regulated to 6-12 PSIG

**Note:**

The test dome will be fitted to the top of the measuring spool piece that is normally fitted to the Turbomolecular pump inlet. The test dome converts the spool piece to an AVS type test dome. see appendix 3 for details.

The gas inlet tube shall be fitted into the port normally occupied by item 9 PV16K manually operated valve, which will be removed during the period of this test.

The gauging is as supplied with the Turbomolecular pump cart, a specially calibrated gauge shall be fitted (per 2.9.4) and will be used to measure pressure lower than  $1 \text{E}-3$  Torr. Its certificates of calibration and correction data against a spinning rotor gauges can be found in appendix 6.

The mass flow controller will be mounted onto a 4 branch manifold, allowing any of the flow controllers to be operated, without dismantling the apparatus.

See appendix 2 for GA of Main Turbo molecular pumping cart

**3. Pressure measurements and calibration**

- 3.1. All Pressure measurements will be carried out using the Gauge heads normally fitted to the carts turbo inlet, see item 19, appendix 2. The gauge heads will be re-located on the test dome for the purposes of this test. A specially calibrated cold cathode gauge shall be used to take actual test data, see appendix 6 for certificate of calibration and correction table.

4. Test overview

- 4.1. The speed test will be carried out across the normal working range of the Turbomolecular pump, from  $1 \times 10^{-5}$  T to  $1 \times 10^{-3}$  T (per V049-2-002), utilizing 5, 20 and 200 sccm mass flow controllers accordingly. etc. a stabilization time of approximately 10 minutes between pressure changes to ensure equilibrium is reached.
- 4.2. Three measurement points will be taken at each decade of measured pressure. Data points will additionally be taken for the purposes of demonstrating throughput capability
- 4.3. The continuous inlet pressure test will raise the inlet pressure up to  $1 \times 10^{-1}$  T, the pumps maximum continuous inlet pressure. Once this pressure is reached, the pump will be left running for a period, not to exceed 24hrs, running at this pressure in order to demonstrate its robustness running at high pressure.

5. Procedure

5.1. Base pressure measurement

- 5.1.1. The Pump shall be started, with the massflow controllers all in zero flow condition, and the system allowed to reach equilibrium. This pressure shall be at least 10 times lower than the lowest pressure for which speed is to be measured. This Pressure is recorded as  $P_0$ .

5.2. Speed test

- 5.2.1. The inlet pressure, as read by the cold cathode gauge, is increased by increasing the flow through the appropriate mass flow controller in steps to establish pressures over the test range according to table 1 below. Adjust the flows by adjusting the setpoint potentiometers accessible on the front panel of the 1605 MFC display/controller
- 5.2.2. The massflow indicated, actual inlet pressure, and foreline pressure shall be noted see appendix 4.  
Between each pressure measurement change a period of at least 10 minutes shall be allowed for equilibrium to be reached.

5.3. Throughput test

- 5.3.1. Following the speed test, gas shall be inlet using the 5 LPM mass flow controller at pressures according to table 2 below to confirm the pumps throughput characteristics. These pressure readings shall be taken using the Pirani gauge only. Measurements shall be noted as per appendix 5  
When the pump has reached an inlet pressure of approximately  $1 \times 10^{-1}$  T (maximum continuous inlet pressure), the test rig shall be left for a period not to exceed 24hrs to demonstrate its operating capability at high throughput/pressure.

Reading #	Target Pressure (T)	Estimated massflow (sccm)
1	3.00E-06	0.3
2	5.00E-06	0.5
3	1.00E-05	1.0
4	3.00E-05	2.8
5	5.00E-05	5.0
6	1.00E-04	11
7	3.00E-04	30
8	5.00E-04	50
9	1.00E-03	100

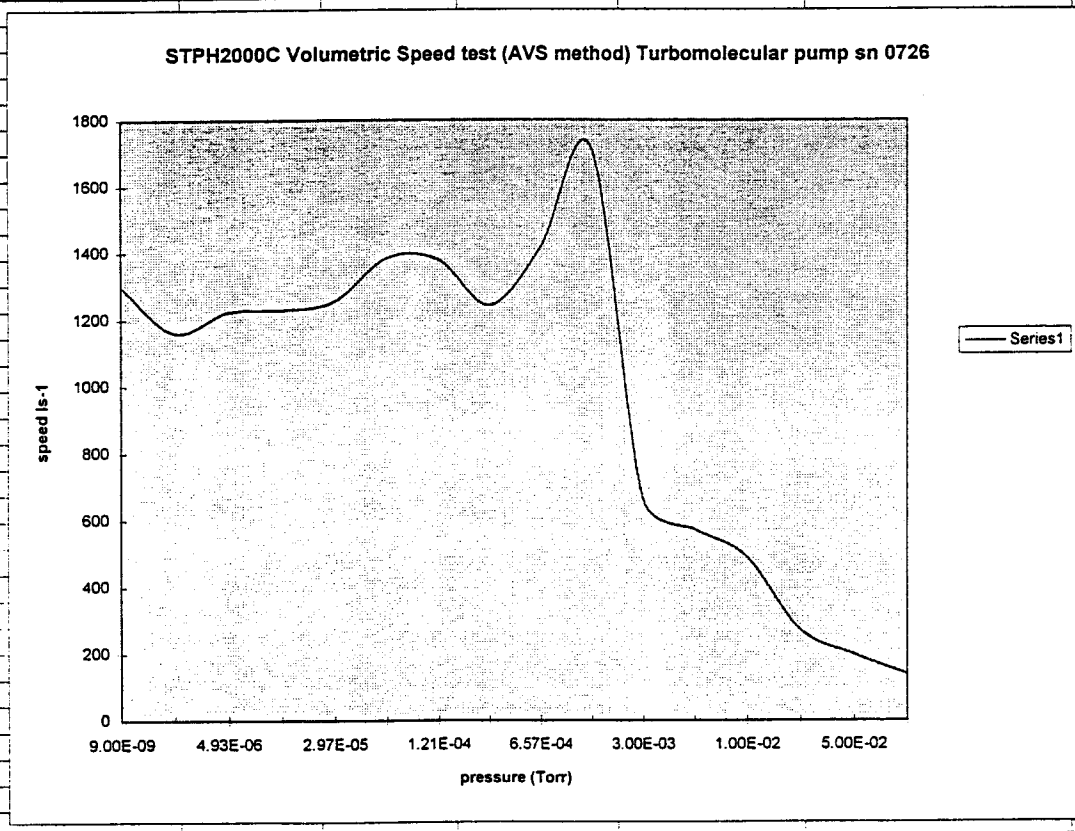
Table 1 target pressures for STPH2000C speed test

Reading #	Target Pressure (T)
1	3e-3
2	5e-3
3	1e-2
4	3e-2
5	5e-2
6	1e-1

Table 2 target pressures for STPH2000C throughput test

STPH2000C SN0726 speed test

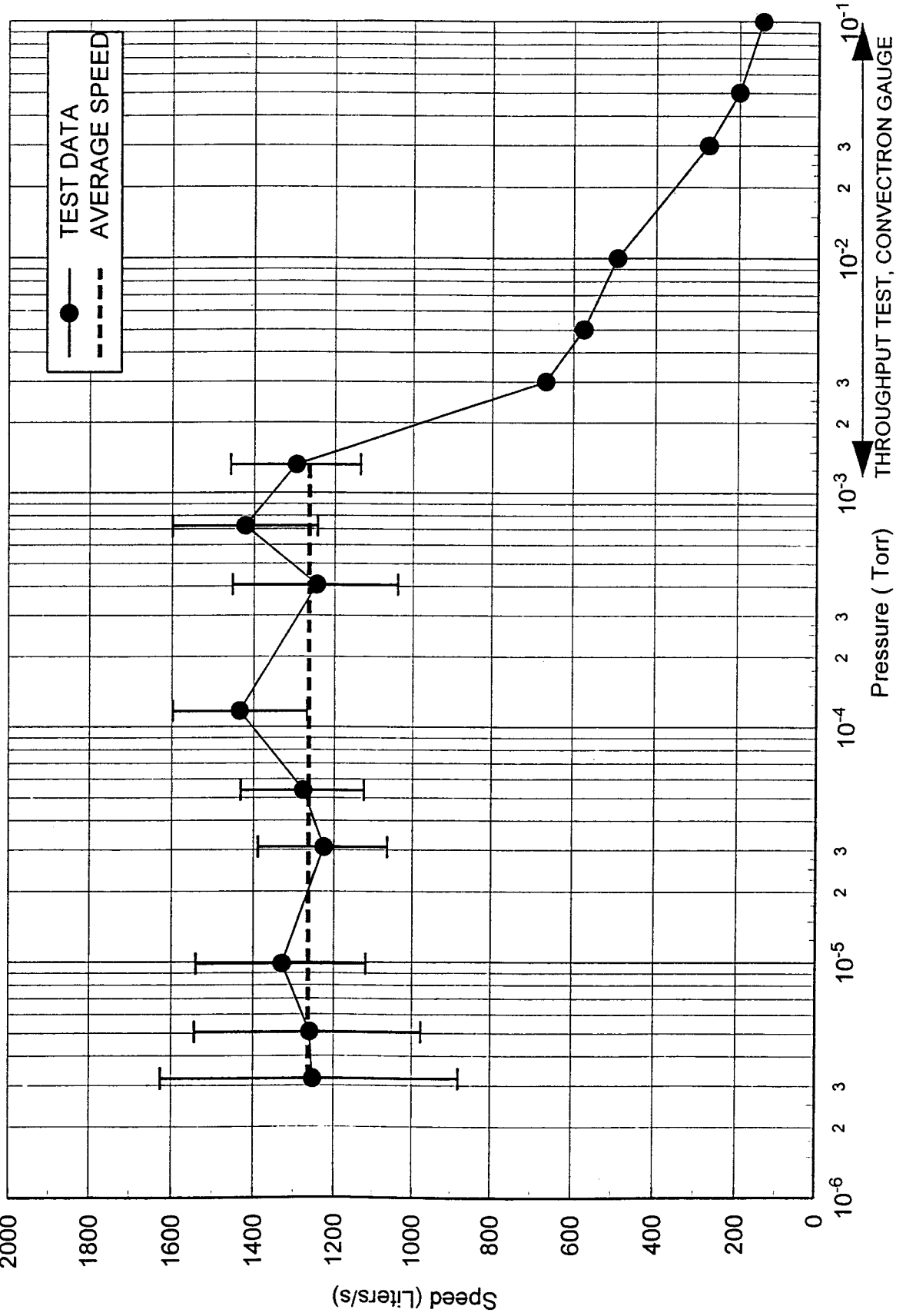
Reading #	Target Pressure (T)	Gauge type	Foreline (Torr)	Massflow (sccm)	Actual Pressure (T)	Corrected Pressure(T)	Pumpspeed (l/s)
1	Base Pressure	Cold Cathode	5.00E-03	0	9.00E-09	9.00E-09	1300
2	3.00E-06	Cold Cathode	6.40E-03	0.25	3.00E-06	2.96E-06	1161
3	5.00E-06	Cold Cathode	7.10E-03	0.44	5.00E-06	4.93E-06	1225
4	1.00E-05	Cold Cathode	8.25E-03	0.93	1.00E-05	1.04E-05	1229
5	3.00E-05	Cold Cathode	1.30E-02	2.72	3.00E-05	2.97E-05	1256
6	5.00E-05	Cold Cathode	1.70E-02	5	5.00E-05	4.95E-05	1385
7	1.00E-04	Cold Cathode	2.80E+00	12.2	1.00E-04	1.21E-04	1379
8	3.00E-04	Cold Cathode	5.50E-02	33	3.00E-04	3.64E-04	1243
9	5.00E-04	Cold Cathode	8.30E-02	68	5.00E-04	6.57E-04	1418
10	1.00E-03	Cold Cathode	1.30E-01	125	1.00E-03	1.00E-03	1712
11	3.00E-03	Pirani	1.40E-01	146	3.00E-03	3.00E-03	667
12	5.00E-03	Pirani	1.90E-01	210	5.00E-03	5.00E-03	575
13	1.00E-02	Pirani	2.80E-01	360	1.00E-02	1.00E-02	493
14	3.00E-02	Pirani	4.20E-01	600	3.00E-02	3.00E-02	274
15	5.00E-02	Pirani	5.00E-01	730	5.00E-02	5.00E-02	200
16	1.00E-01	Pirani	6.50E-01	1030	1.00E-01	1.00E-01	141



# STPH2000C SN0726 SPEED TEST

Error bar includes accuracy of mass flow controller and  $\pm 10\%$  error of pressure gauge

Pressure gauge calibrated against spinning rotor gauge





## **6.0 COMPONENT INSTALLATION**

- Major equipment is set and aligned by PSI's site contractor.

*See Sample #1*

- PSI verifies the alignment.
- LIGO checks critical component alignments.
- LIGO approves alignment and releases components for grouting.

*See Sample #2*

- PSI conducts grout testing to verify grout strength.

*See Sample #3*

COMPONENT CLOSE-OUT DATA SHEET

Component Tag Number: WB96-6

Component Name: BEAM SPLITTER CHAMBER

Component S/N: S/N-07

Vacuum Sealing Surfaces Inspection

By: [Signature] FOR FOREMAN ROCKWELL 12/10/97

Buyer: [Signature] 10 DEC 97

Cleanliness Inspection

By: [Signature] FOR FOREMAN ROCKWELL 12/10/97

Buyer: [Signature] 10 DEC 97

O-rings Installed

By: [Signature] FOR FOREMAN ROCKWELL 12/10/97

Buyer: [Signature] 10 DEC 97

Comments:

Rework Required:

SAMPLE #1  
BSC ALIGNMENT Q.A.  
PAGE 1 OF 5

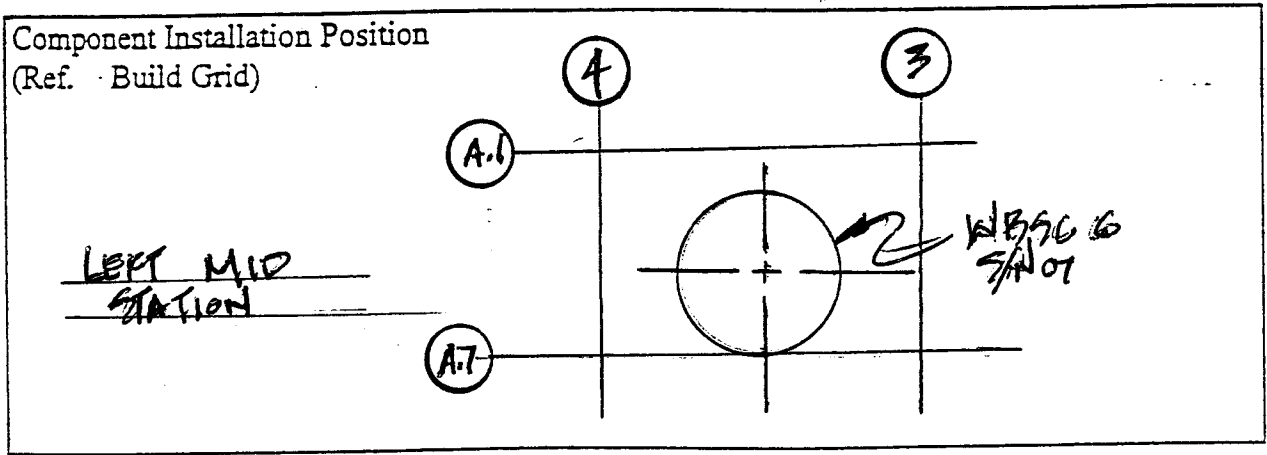
Title

COMPONENT ALIGNMENT PROCEDURE

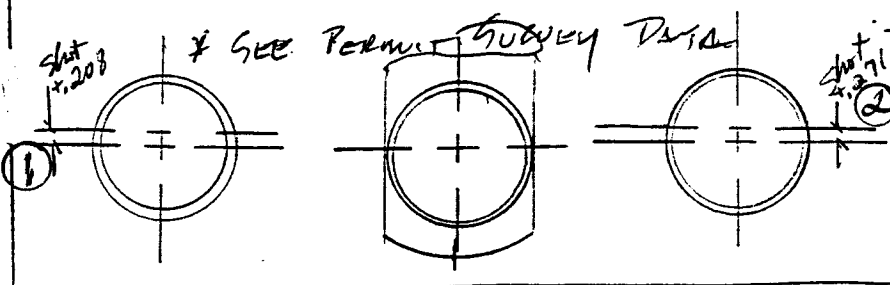
ATTACHMENT B

COMPONENT INSTALLATION DATA SHEET

Component Tag Number WBSC 6  
 Component Name BEAM SPLITTER CHAMBER  
 Component S/N 9/N 07  
 Component Installation Weight (lb.) 15,000 lb.



Signoffs (Contractor Unless Otherwise Noted)	By	Date
1. Snapping Cover Cross hairs verified	<i>[Signature]</i>	10-30-97
2. Component Located For Anchor Bolt Marking	Vern Coyne Bill Folster V.C.	10-30-97
	Buyer <i>[Signature]</i>	300597
3. Final Component Location Complete	<i>[Signature]</i>	11-4-97 *
	Buyer	



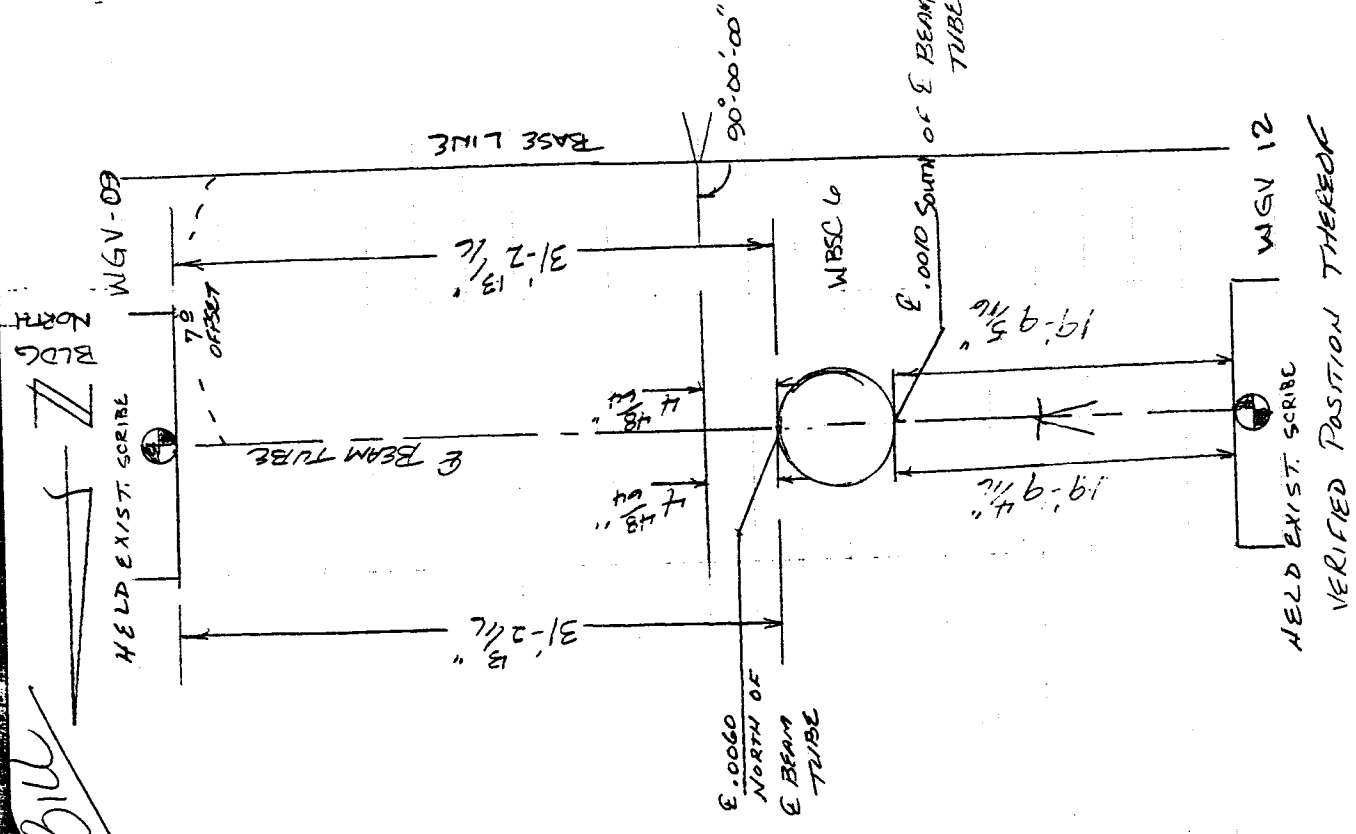
WBSC 6	①	②	△
calc	+ .21	+ .275	+ .065
shot	+ .208	+ .271	.063

SPECIFICATION		
Number	A	Rev. 1
V049-2-174		

Number  
Rev.

3 of 5

Bill

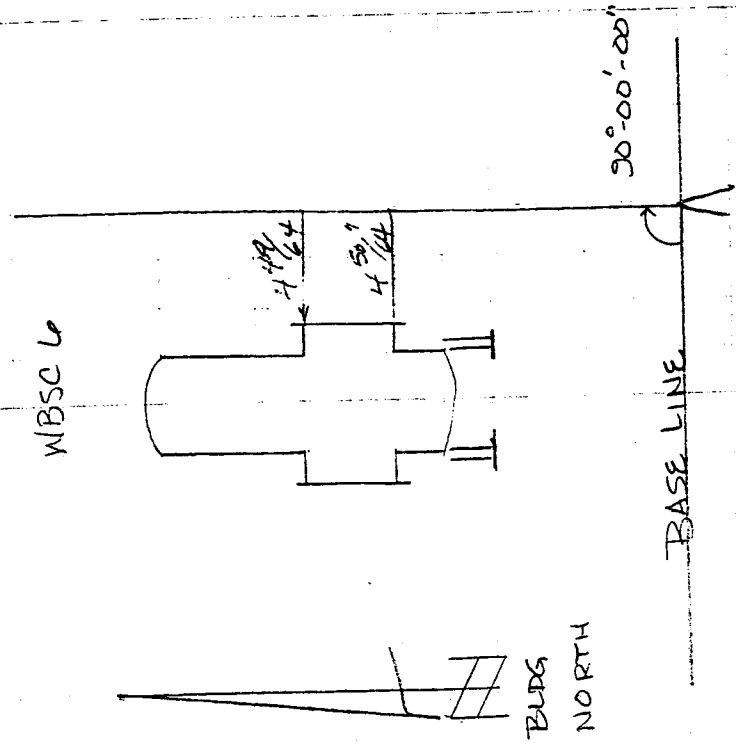


FROM VERN

1160 LEFT MID STATION

10 30 97

V. COYNE  
B. PALSTER



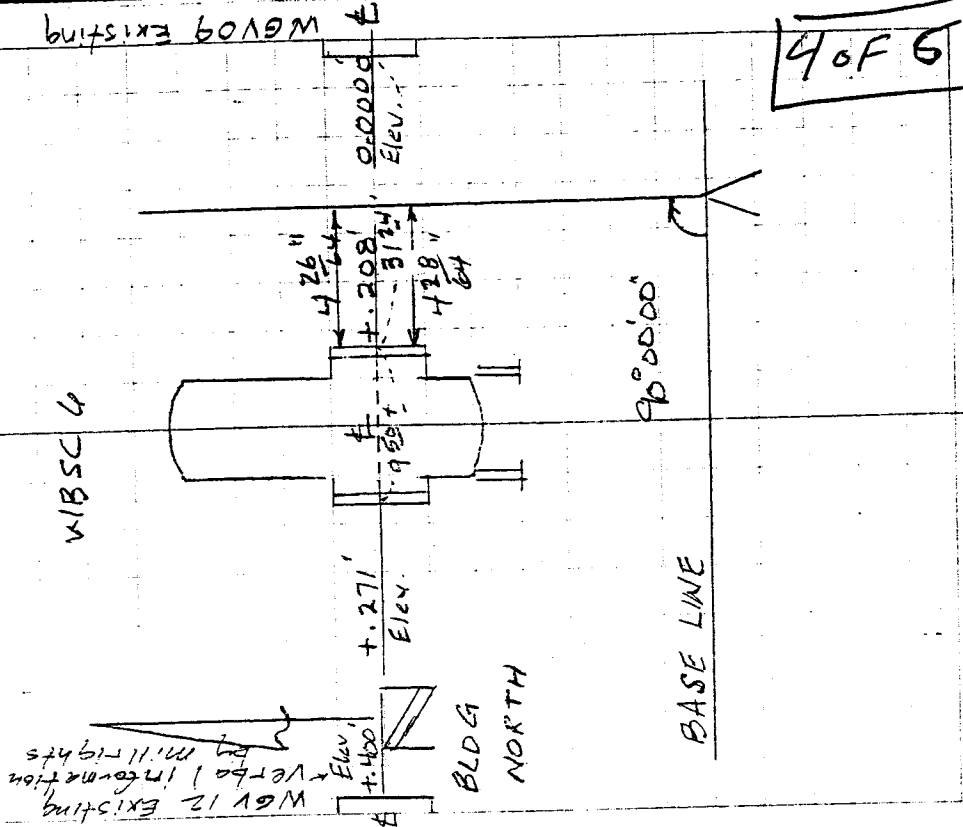
3 of 6

2/90

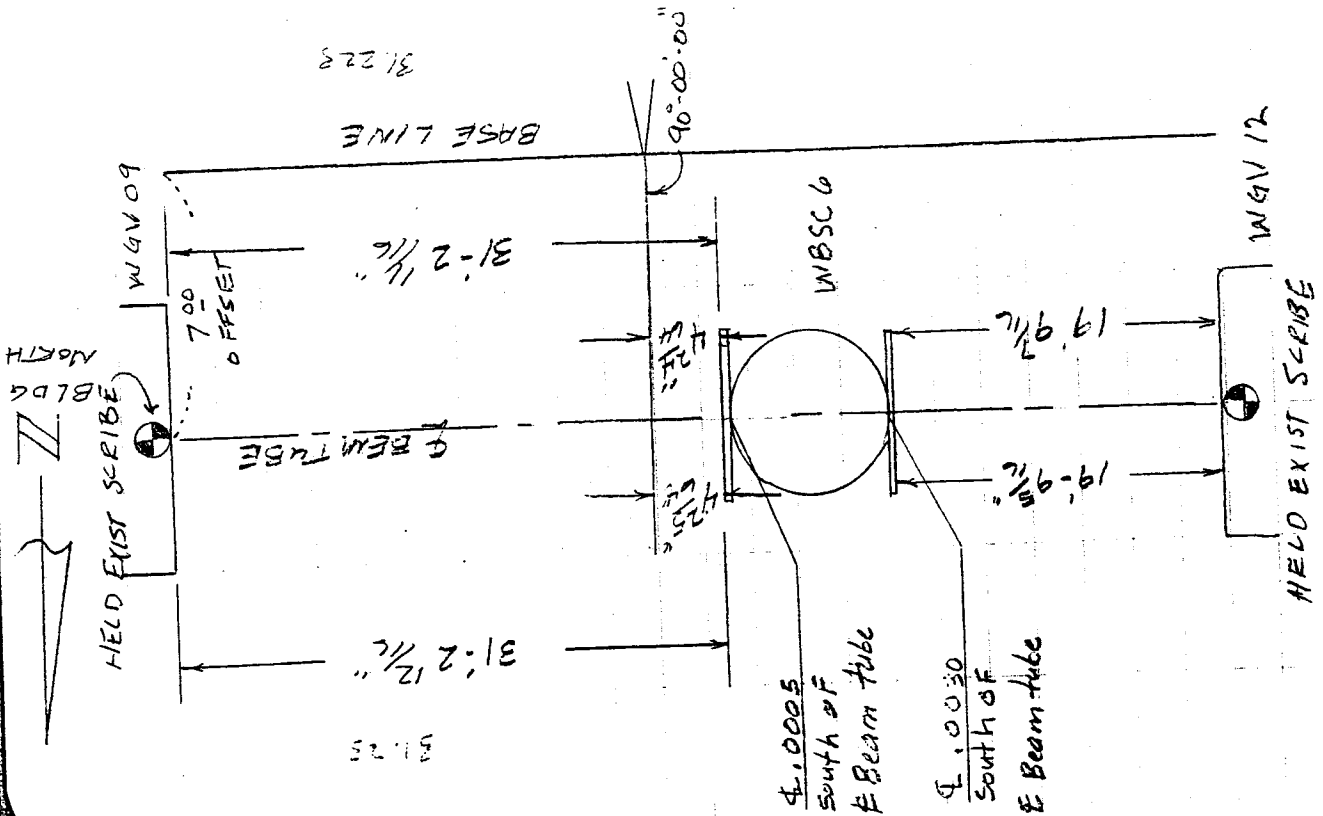
#9783 LIGO LEFT MID STATION

11-4-97

After Floor Anchor Bolts installed.  
V. Coyne  
K. Sarchett



4 of 6



3/90

9183 LIPO LEFT MID STATION 11-4-97

V. Coyne  
K. Serechett

± W 9109 Gate Valve

± WBSG6 East side

± WBSG6 West side

+ H.I. - Rod Elev.

0-0000

-11.637 11-637

+ .208

11.845

+ .211

11.908

5 OF 6

11.110  
11.908  
11.637



SAMPLE #2



PROCESS SYSTEMS INTERNATIONAL, INC.

**LIGO Project**

Doc.No.V049- PL - 511

**Vacuum Equipment Grouting Request**

**Date:** December 19,1997

**Location:** LIGO Washington Site

**Subject:** LIGO Vacuum Equipment Grouting Request

**CC:** R.Bagley Fax 508.898.0322

PSI requests permission from LIGO to grout all vacuum equipment in the Left Mid and Left End Stations.

By granting this request, LIGO agrees with the final alignment measurements and equipment sets performed by the Vacuum Equipment Contractor, Apollo Sheet Metal.

Request Approved John Worden  
 John Worden - LIGO

12/19/97  
 Date





- Consulting Engineers
- Environmental Scientists
- Special Structural Inspections
- Construction Materials Testing

SAMPLE #3  
1 of 3

722 N. 16th Ave. #31  
Yakima, WA 98902  
(509) 248-9798  
Fax (509) 248-4220

6713 W. Clearwater #F  
Kennewick, WA 99336  
(509) 734-9320  
Fax (509) 734-9321

1515 N. Miller Street  
Wenatchee, WA 98801  
(509) 664-8931  
Fax (509) 665-0931

Sunnyridge Building #2  
Rt. 2 Box 2555  
Hermiston, OR 97838  
(541) 564-0991  
Fax (541) 564-0928

(800) 428-9798

20F3

**PROCESS SYSTEMS INTERNATIONAL, INC  
LIGO VACUUM EQUIPMENT INSTALLATION**

**INSPECTION SERVICES FOR GROUTING  
FINAL REPORT**



# Northern, Inc.

• Consulting Engineers • Environmental Scientists • Construction Materials Testing

3 of 3

722 N. 16th Ave. Suite 31  
P.O. Box 1463  
Yakima, WA 98907  
(509) 248-9798  
Fax (509) 248-4220

6713 W. Clearwater #F  
Kennewick, WA 99336  
(509) 734-9320  
Fax (509) 734-9321

Sunnridge Building #2  
Rt. 2 Box 2555  
Hermiston, OR 97838  
(541) 564-0991  
Fax (541) 564-0928

## GROUT PRISM TEST REPORT

REPORT TO: PROCESS SYSTEMS INTERNATIONAL, INC  
20 WALKUP DRIVE  
WESTBOROUGH, MA 01581-5003

DATE: 01-19-98  
JOB NO.: 97-734  
W/ORDER NO.: 7290YM

PROJECT: LIGO VACUUM EQUIPMENT INSTALLATION  
CONTRACTOR: APOLLO  
STRUCTURE: VACUUM BASES  
LOCATION: HANFORD/MID WEST STATION

### MIX AND MATERIALS DATA

REPORTED BY APOLLO  
MIX NUMBER: -  
SACKS/CY.: -  
CEMENT TYPE: CG200PC  
ADMIXTURES: -

GROUT SUPPLIER: HILTI  
MIXING METHOD: HAND MIX  
AGGREGATE SOURCE: HILTI  
WATER SOURCE: ON-SITE

### SPECIFICATIONS:

SLUMP, INCHES: -  
AIR CONTENT, %: -

### REQUIRED STRENGTH, PSI:

7 DAY: -  
28 DAY: 7000

### FIELD TEST DATA

SLUMP, IN.: - (ASTM C143)  
AIR CONT. %: - (ASTM C231)  
GROUT TEMP: 70 (ASTM C1064)  
AIR TEMP: 68  
UNIT WT, PCF: N/R (ASTM C138)  
YIELD: N/R (ASTM C138)  
GROUT SAMPLED, (ASTM C172),  
TESTED, & CYLINDERS CAST (ASTM C31)  
DATE CAST: 12/22/97  
TIME CAST: -  
CAST BY: J. CAFFREY

TRUCK NO.: MIXED ON SITE  
TIME BATCHED: -  
TICKET NO.: -  
NO. CY REP.: 1 SACK  
WATER ADDED ON SITE,  
GALLONS: -  
CYLINDER CURING (ASTM C31)  
FIELD CURE, DAYS: 1  
AT TEMP RANGE: - TO -  
LAB CURE FROM: -  
(DATE RECV'D): 12/23/97

### LABORATORY TEST DATA

SAMPLE NUMBER: 5888-1

CYL. NUMBER	AGE/DATE	DATE TESTED	X-SEC DIM.	AREA IN 2"	LOAD LBS.	COMP. STR. PSI
5888-1	7	12/29/97	2X2	4.0	22,940	5,740
5888-2	7	12/29/97	2X2	4.0	20,340	5,090
5888-3	7	12/29/97	2X2	4.0	24,480	6,120
5888-4	14	01/05/97	2X2	4.0	42,760	10,690
5888-5	28	01/19/97	2X2	4.0	53,720	13,430
5888-6	28	01/19/97	2X2	4.0	58,340	14,590

REVIEWED BY: Gerald Harper

Gerald Harper  
Division Manager

## **7.0 COMPONENT MECHANICAL/ELECTRICAL INSPECTIONS/ TESTING**

- P&ID/Piping Drawing Walkdowns
- Utility Systems Testing (Water, Class 100 Air, etc.)
  - Pressure tests
  - Particle count
  - Hydrocarbon level
  - Moisture level
- Electrical System Testing/Approvals

*See Sample #1*

SAMPLE #1

WRING TEST DATA SHEET

Project No.: 97047  
 Megger: \_\_\_\_\_  
 M&TE: \_\_\_\_\_  
 Calibration Date: \_\_\_\_\_

Title: 1160  
 Test Voltage: CONTINUITY  
 Conducted By: KEN GALPIN  
 Witnessed By: HARLAN BRADY

VOM: FLUKE  
 M&TE: 97-22  
 Calibration Date: 4/22/97

CDS-17  
 MECHANICAL  
 ROOM

WIRE RUN/CABLE # OR LOCATION	CONTINUITY		O TO O MEGGER READING			O TO GROUND MEGGER READING		
	CONDUCTORS	SHVNO	A-B	B-C	CA	A	B	C

II-111	O.K.	O.K.	/	/	/	/	/	/
II-115	O.K.	O.K.	/	/	/	/	/	/
II-117	O.K.	O.K.	/	/	/	/	/	/
II-121	O.K.	O.K.	/	/	/	/	/	/
II-125	O.K.	O.K.	/	/	/	/	/	/
II-127	O.K.	O.K.	/	/	/	/	/	/
II-131	O.K.	O.K.	/	/	/	/	/	/
II-135	O.K.	O.K.	/	/	/	/	/	/
II-137	O.K.	O.K.	/	/	/	/	/	/
ZSC-109	O.K.	O.K.	/	/	/	/	/	/
ZSO-109	O.K.	O.K.	/	/	/	/	/	/
ZSC-145	O.K.	O.K.	/	/	/	/	/	/
ZSO-145	O.K.	O.K.	/	/	/	/	/	/
EI-161A	O.K.	O.K.	/	/	/	/	/	/
II-161A	O.K.	O.K.	/	/	/	/	/	/
EI-161B	O.K.	O.K.	/	/	/	/	/	/
II-161B	O.K.	O.K.	/	/	/	/	/	/
EI-162A	O.K.	O.K.	/	/	/	/	/	/
II-162A	O.K.	O.K.	/	/	/	/	/	/
EI-162B	O.K.	O.K.	/	/	/	/	/	/
II-162B	O.K.	O.K.	/	/	/	/	/	/
EI-163A	O.K.	O.K.	/	/	/	/	/	/
II-163A	O.K.	O.K.	/	/	/	/	/	/
EI-163B	O.K.	O.K.	/	/	/	/	/	/
II-163B	O.K.	O.K.	/	/	/	/	/	/
EI-164A	O.K.	O.K.	/	/	/	/	/	/
II-164A	O.K.	O.K.	/	/	/	/	/	/
EI-164B	O.K.	O.K.	/	/	/	/	/	/
II-164B	O.K.	O.K.	/	/	/	/	/	/
XA-161A	O.K.	O.K.	/	/	/	/	/	/
XA-161B	O.K.	O.K.	/	/	/	/	/	/
XA-162A	O.K.	O.K.	/	/	/	/	/	/
XA-162B	O.K.	O.K.	/	/	/	/	/	/
XA-163A	O.K.	O.K.	/	/	/	/	/	/
XA-163B	O.K.	O.K.	/	/	/	/	/	/
XA-164A	O.K.	O.K.	/	/	/	/	/	/
XA-164B	O.K.	O.K.	/	/	/	/	/	/
HS-161A	O.K.	O.K.	/	/	/	/	/	/
HS-161B	O.K.	O.K.	/	/	/	/	/	/

## 8.0 VACUUM EQUIPMENT PERFORMANCE VERIFICATION

### 8A. LEFT END STATION

The left end vacuum performance data is detailed in Acceptance Test Report V049-1-168.

All test results met or exceeded the requirements.

The following is a summary of that report:

## LEFT END STATION

### ACCEPTANCE TEST RESULTS SUMMARY

As shown in Section 3 the WA Left End Station has been successfully tested to meet the Acceptance Test Criteria with the following comments:

#### **System Leak Check**

The system is believed to be leak tight to a level of  $6 \times 10^{-9}$  Torr-L/s Air. The minimum detectable leak from the RGA scan with the sensitivity obtained during the scan for the Left End Station is about  $6 \times 10^{-9}$  Torr-L/s Air. This was deduced based on mass 32 ion current. The Argon signal is not used because the pumping speed of the ion pump is not known accurately for Argon.

The RGA scans of just the calibration chamber isolated from the main volume, indicates that there is a leak in the calibration chamber. The observed signal for mass 32 was almost  $5 \times 10^{-13}$  A with the RGA chamber by itself. With a calibrated sensitivity of 3 Torr/Amp the partial pressure is  $1.5 \times 10^{-12}$  Torr. With a calibration chamber speed of 3.7 liter/s the leak in the RGA chamber is estimated at  $3 \times 10^{-11}$  Torr-L/s Air. If there was no leak in the RGA chamber the minimal detectable leak would be  $6 \times 10^{-9}$  Torr-L/s Air. Bagging the entire chamber with helium did not lead to a helium signal on the RGA scan.

#### **System Bakeout**

The bakeout ramp up and ramp down rates exceeded the specified rate. The design ramp rates were selected to minimize thermal stress and to keep input power requirements at reasonable levels. The actual ramp rates, although in excess of the acceptance criteria are still low and are not considered to be sufficient to cause thermal stresses, and are therefore acceptable.

The loss of the temperature data is unfortunate, but the subsequent excellent RGA scans after bakeout indicate that the system is clean and the bakeout was therefore effective.

LEFT END STATION

**Ultimate Pressure Test**

The partial pressure measurements after bakeout readily exceeded the acceptance criteria and match very well with the LIGO goals indicating that the volume is clean and leak tight. A comparison table of the actual results vs. the LIGO is included for information.

AMU	LIGO Goals	Acceptance Test
	Partial Pressure	Partial Pressure
(Torr)	(Torr)	(Torr)
2	$5 \times 10^{-9}$	$4.4 \times 10^{-9}$
16	$2 \times 10^{-10}$	$2.2 \times 10^{-11}$
18	$5 \times 10^{-9}$	$1.7 \times 10^{-11}$
28	$1 \times 10^{-9}$	$8.9 \times 10^{-10}$
44	$2 \times 10^{-10}$	$2.5 \times 10^{-11}$
Other	$1.9 \times 10^{-9}$	$1.3 \times 10^{-10}$

**Backfill/100 Hour Pumpdown Test**

A comparison of the partial pressures before and after the backfill is shown below. As expected an approximate one-decade increase in N<sub>2</sub> and CO<sub>2</sub> pressures are observed. This is consistent with the prototype test program. There is also a factor of 4-5 increase for H<sub>2</sub>O, CH<sub>4</sub>, and a one decade increase for the other gasses that did not occur in the Left Mid Station. The resulting partial pressures for all gasses are still below the LIGO goals.

	After Bakeout	After Backfill & 100 hr Pumpdown
AMU	Partial Pressure	Partial Pressure
	(Torr)	(Torr)
2	$4.4 \times 10^{-9}$	$3.3 \times 10^{-9}$
16	$2.2 \times 10^{-11}$	$8.8 \times 10^{-11}$
18	$1.7 \times 10^{-11}$	$9.4 \times 10^{-11}$
28	$8.9 \times 10^{-10}$	$7.7 \times 10^{-9}$
44	$2.5 \times 10^{-11}$	$3.8 \times 10^{-10}$
Other	$1.3 \times 10^{-10}$	$9.7 \times 10^{-10}$

**LN2 Consumption**

Results of the Left End Station Cryopump indicates a full tank capacity of more than 100 days.



LEFT END STATION

**ACCEPTANCE TEST CRITERIA**

Item	Acceptance Criteria	Acceptance Results
Interface to CDS	Functional Checkout per V049-2-163	Checkout completed on 1/27/98
Clean Air System Test	Functional Checkout per V049-2-109 Dewpoint: <-60 C Particle Count: Class 100 @ .5 micrometer. Hydrocarbon Check:	Dewpoint: -75. C Particle Count: 0 Hydrocarbon Check: 0 PPM
Class 100 Cleanroom Test	Functional Checkout per V049-2-110 Particle Count: <100	Particle Count: <17.1
System Leak Check	Individual leaks greater than $1 \times 10^{-9}$ torr-L/s will be repaired.  Vacuum Check: Annulus: $P < 3 \times 10^{-4}$ torr 60 min for vessels and 30 min for spools and ate valves.  Main Volume: by RGA air signature. Maximum rate to be consistent with system requirements and RGA sensitivity.	All components comprising the isolatable volume were helium leak checked via evacuation and spray prior to bakeout.  All flange annuli checked and passed. Data recorded in site test logs.  The volume is leak tight to $< 6 \times 10^{-9}$ torr-L/s
System Bake-out	Functional Checkout per V049-2-112 Rev1 Bakeout: Ramp Rate: <1C/hour Uniformity: 150 C +/- 20C	The station was ramped from 18 C to 150 C over a period of 93 hours (1.4 C/hr) and held for 49 hours at 150C. Temperature data recorded in the bakeout cart data acquisition system was subsequently overwritten; therefore no temperature uniformity data is available. After the 48-hour hold, the temperature was ramped to 48 C over 48.5 hours (2.1C/hr) prior to shutting off the power.

LEFT END STATION

Item	Acceptance Criteria	Acceptance Results																
Ultimate Pressure Test (After Bake-out)	Total Pressure: $<2 \times 10^{-8}$ torr Partial Pressure Measurements: Sum of all gasses other than H <sub>2</sub> and H <sub>2</sub> O: $<3 \times 10^{-9}$ torr	Total Pressure: $5.5 \times 10^{-9}$ torr Partial Pressure Measurements: Sum of all gasses other than H <sub>2</sub> and H <sub>2</sub> O: $1.1 \times 10^{-9}$ torr																
Backfill/100 Hr. Pumpdown Test	Roughing to $< 0.2$ torr in 15 hours Roughing to $5 \times 10^{-6}$ torr in 24 hours RGA scan after 100 hours for information only	Roughing to 0.5 torr in 4 hours Roughing to $8 \times 10^{-7}$ torr in 18.75 hours Partial pressures: <table border="0" style="margin-left: 40px;"> <tr> <td>AMU</td> <td>torr</td> </tr> <tr> <td>2</td> <td><math>3 \times 10^{-9}</math></td> </tr> <tr> <td>16</td> <td><math>9 \times 10^{-11}</math></td> </tr> <tr> <td>18</td> <td><math>9 \times 10^{-11}</math></td> </tr> <tr> <td>28</td> <td><math>7 \times 10^{-9}</math></td> </tr> <tr> <td>44</td> <td><math>4 \times 10^{-10}</math></td> </tr> <tr> <td>all others</td> <td><math>1 \times 10^{-9}</math></td> </tr> <tr> <td>Total</td> <td><math>1.4 \times 10^{-8}</math></td> </tr> </table>	AMU	torr	2	$3 \times 10^{-9}$	16	$9 \times 10^{-11}$	18	$9 \times 10^{-11}$	28	$7 \times 10^{-9}$	44	$4 \times 10^{-10}$	all others	$1 \times 10^{-9}$	Total	$1.4 \times 10^{-8}$
AMU	torr																	
2	$3 \times 10^{-9}$																	
16	$9 \times 10^{-11}$																	
18	$9 \times 10^{-11}$																	
28	$7 \times 10^{-9}$																	
44	$4 \times 10^{-10}$																	
all others	$1 \times 10^{-9}$																	
Total	$1.4 \times 10^{-8}$																	
LN <sub>2</sub> Consumption Test	LN <sub>2</sub> consumption per V049-2-208 90 days without refill.	119 days without refill.																
Noise/Shock/Vibration Field Test	Per CAA Test Plan	See CAA Test Report																

# Partial Pressure Calculation

Acceptance of the Bakeout with respect to Air Signature and Partial Pressures

Date: 03/29/98

Test ID: WLERGA

PSI Engineer: S.MOTEW

AMU	F (amu) transmission efficiency wrt N2	E (amu) ionization efficiency wrt N2	S (p_amu) sensitivity (Torr/A)	I (amu) ion current (A)	PP (amu) (Torr)
2	-	-	2.47	1.80E-09	4.45E-09
16	0.57	1.60	-	1.50E-11	2.18E-11
18	0.64	1.12	-	7.90E-12	1.73E-11
28	-	-	3.08	2.90E-10	8.93E-10
44	1.57	1.42	-	9.20E-12	2.50E-11
all others	-	-	3.08	4.30E-11	1.32E-10

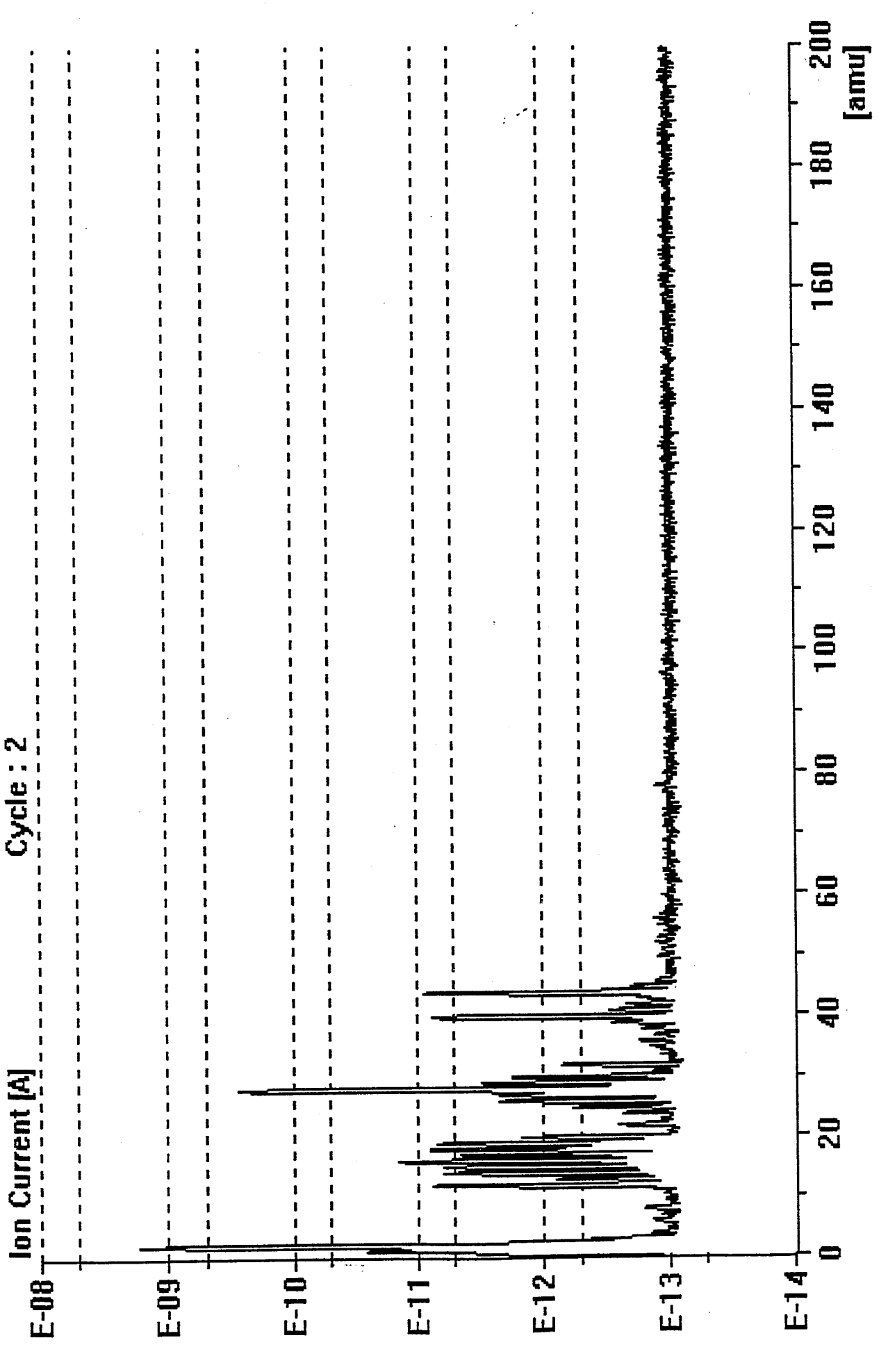
		<u>LIGO Contract Limits</u>	<u>Actual</u>	<u>Pass</u>
Primary Criteria -	Total Pressure:	2.00E-08 Torr	5.54E-09 Torr	Yes
Secondary Criteria -	Others except H2 & H2O:	3.00E-09 Torr	1.07E-09 Torr	N/A

LIGO:

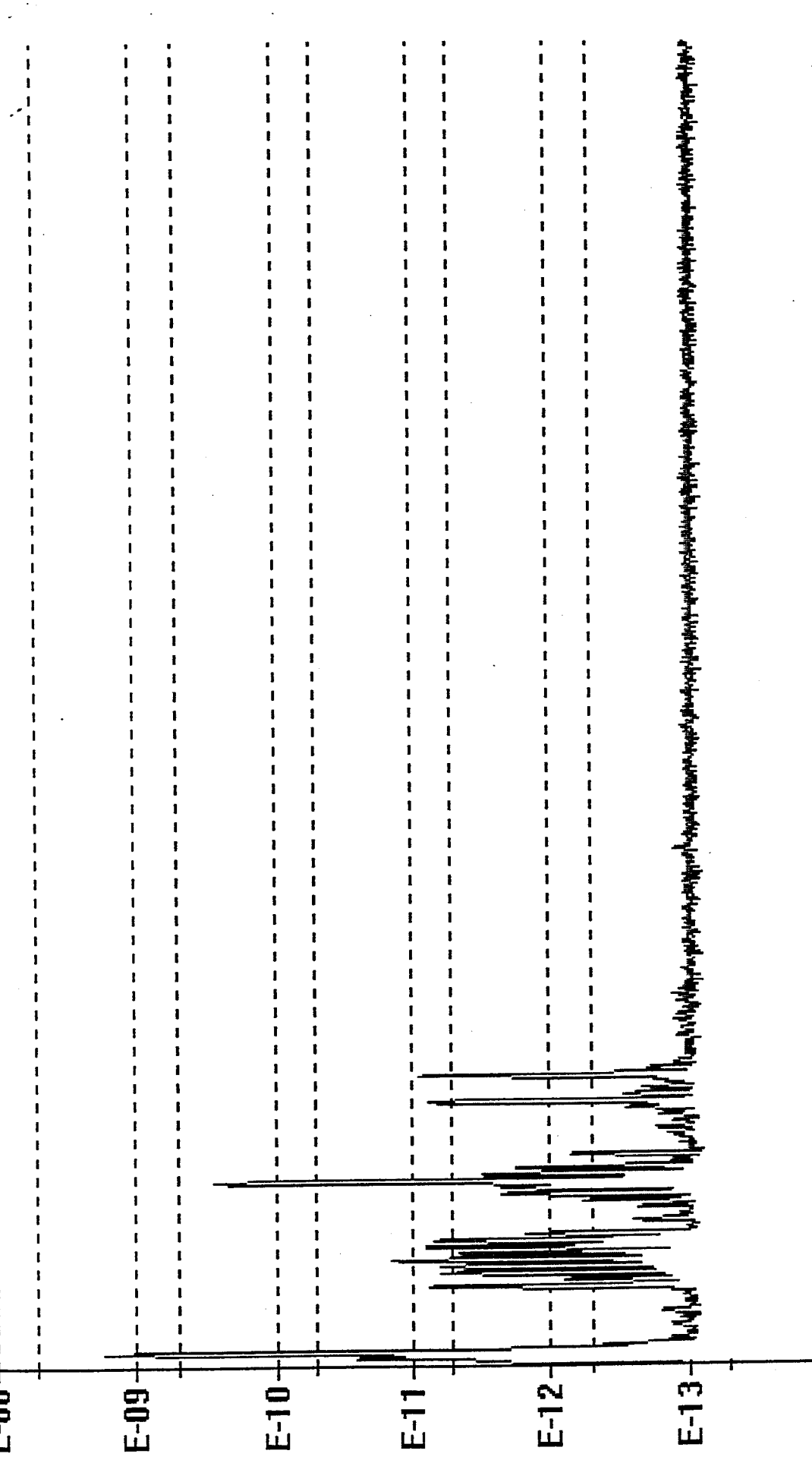
John Wolder

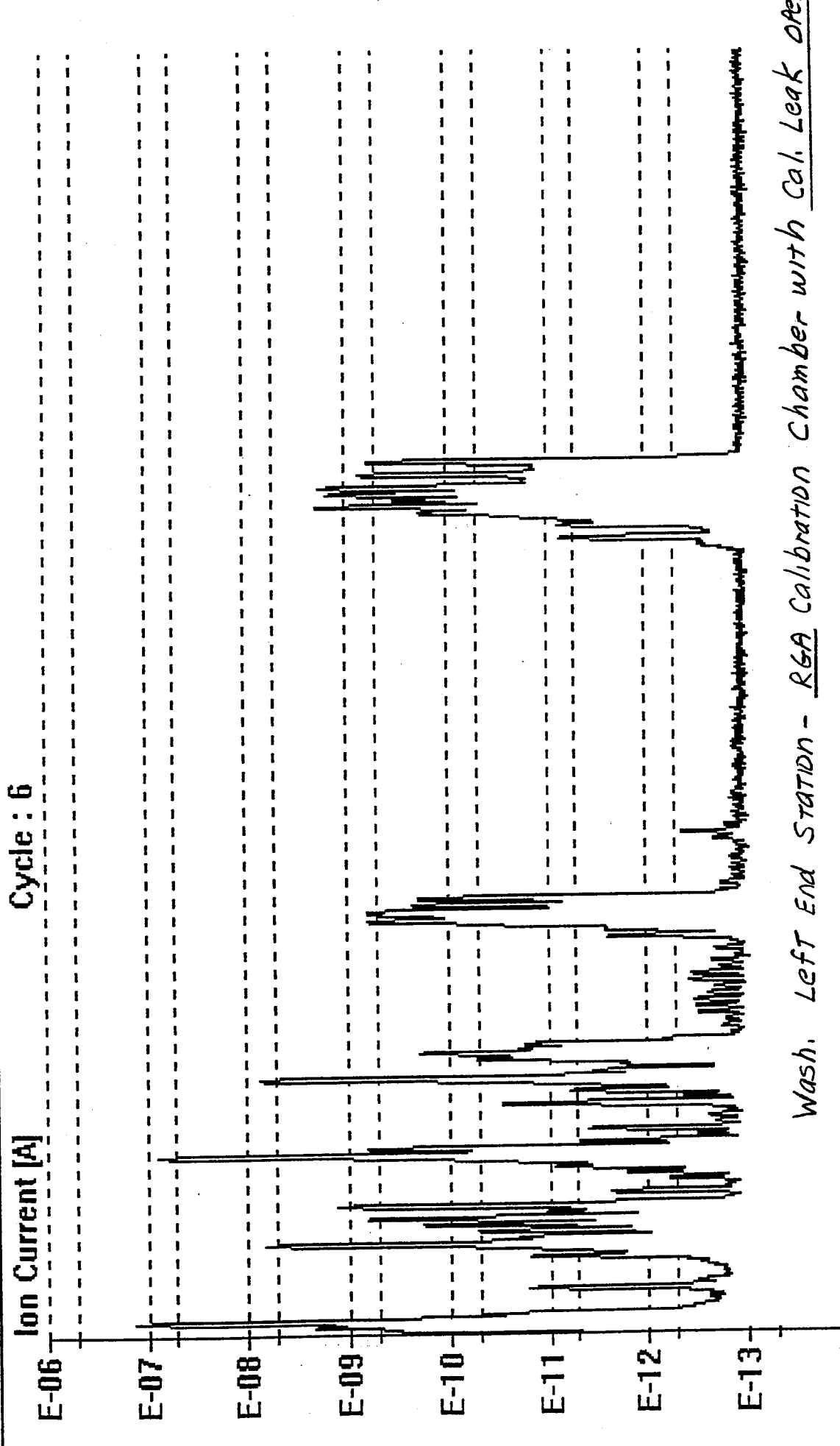
PSI:

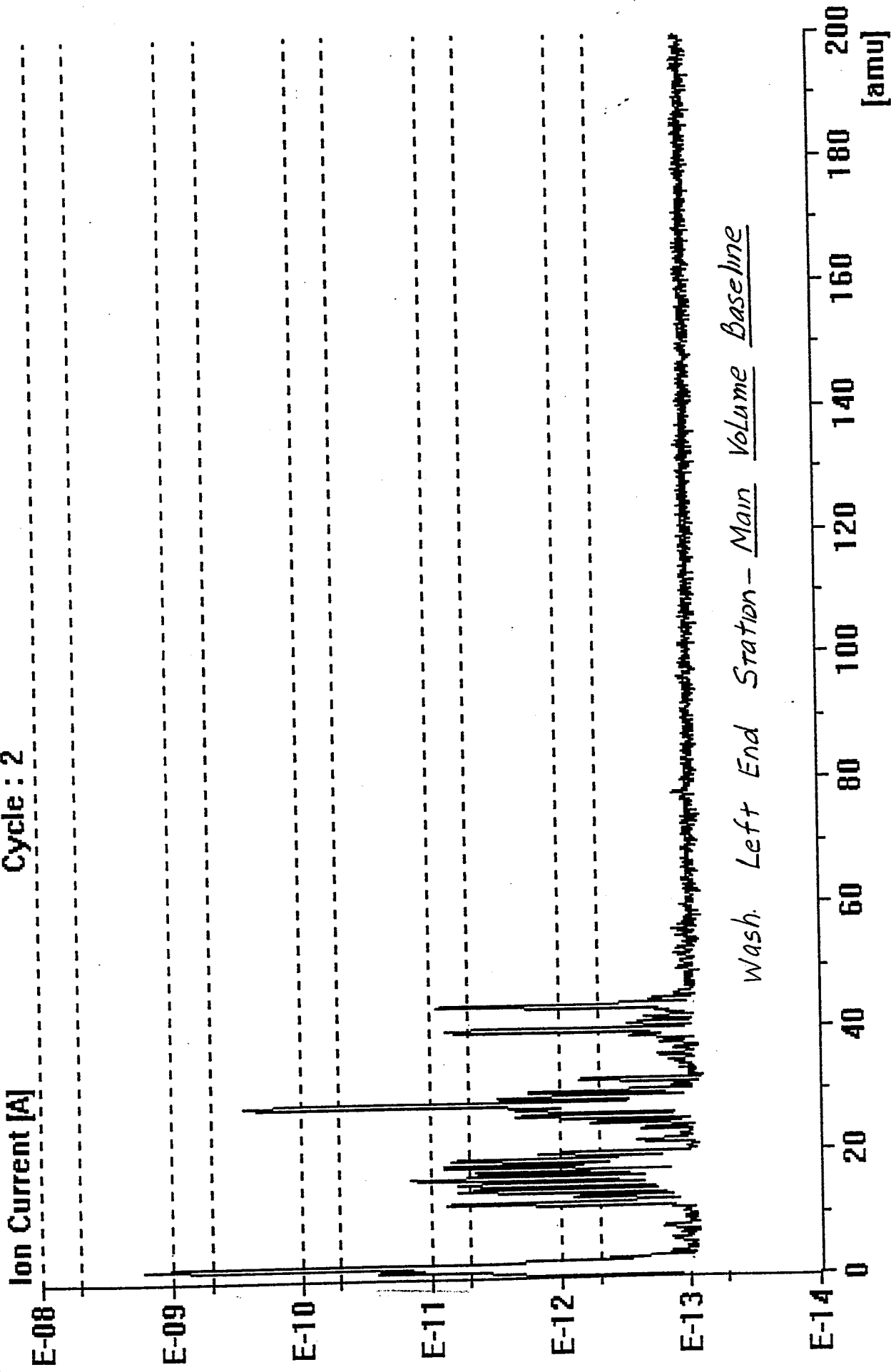
Brent Bay



Ion Current [A] Cycle : 2







## **LIGO VACUUM EQUIPMENT**

### **ACCEPTANCE TEST REPORT SUMMARY**

#### **Backfill/100 Hr. Pumpdown Test – Left End Station**

The backfill and 100 hr. pumpdown test was conducted per Acceptance Test Procedure V049-2-114.

The roughing and turbo pumping requirements met or exceeded the requirements.

The ultimate pressure and partial pressure results are detailed herein. This test was for demonstration purposes only.



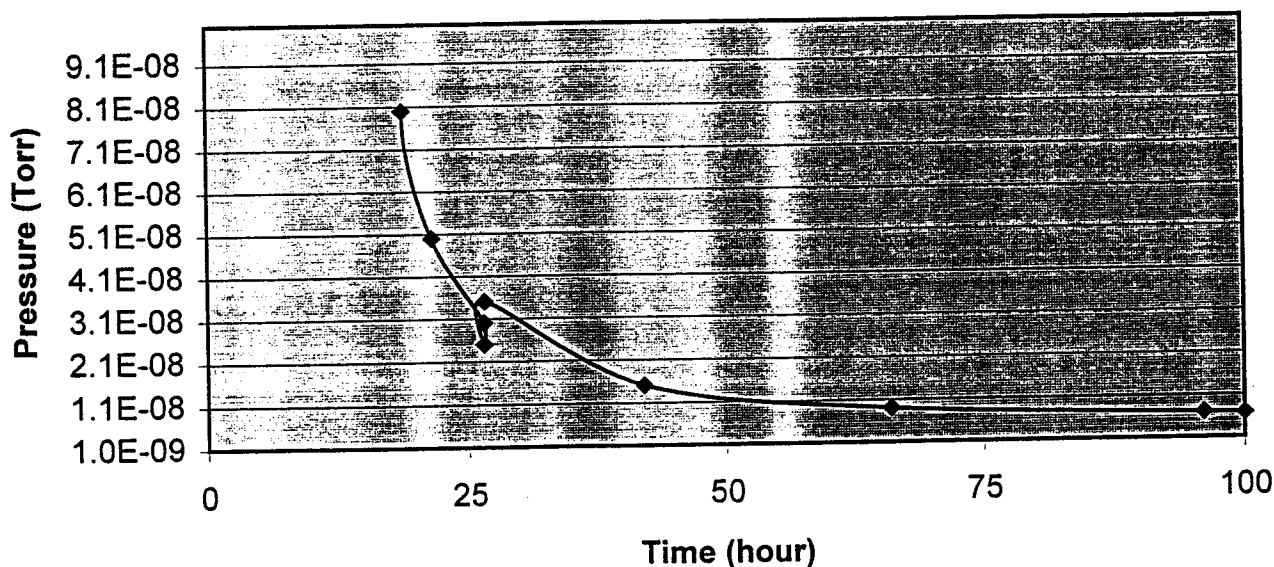
Left End Station Back-to-Air 100 Hour Pumpdown

04/02/98 1300 Start clean air purge with cryopump isolated by GV18  
 04/03/98 1300 End clean air purge  
 Start rough pumping system with QDP80  
 1700 P=0.49 Torr  
 Start turbo pumping system with STP2000C  
 04/04/98 745 P=8.0E-8 Torr  
 P(cryo)=4.0e-6 Torr  
 Fill Cryopump  
 830 Start 2500 l/s ion pump and close 14" gate valve  
 1000 Open GV18 (44" gate valve)  
 1030 P=5.0E-8 Torr  
 1530 Ion Pump (Voltage=3000V, Amperage=2.5E-4A)  
 P=3.0E-8 Torr  
 Open 14" gate valve  
 1531 P=2.5E-8 Torr  
 Close 10" gate valve to isolate STP2000C  
 1535 P=3.5E-8 Torr  
 Ion Pump (Voltage=3000V, Amperage=5.2E-4A)  
 4/5/98 700 P=1.5E-8 Torr  
 4/6/98 700 P=9.0E-9 Torr  
 4/7/98 1300 P=7.0E-9 Torr  
 1700 PT410=6.84E-9 Torr End of 100 hour test  
 PT424=6.69E-9 Torr

Graphical Data	
Time (hr)	Press (torr)
0	760
4	0.49
18.75	8.00E-08
21.5	5.00E-08
26.5	3.00E-08
26.52	2.50E-08
26.58	3.50E-08
42	1.50E-08
66	9.00E-09
96	7.00E-09
100	6.80E-09

Save all RGA data to WLEbta\_1.\*\*\*

**Left End Station 100 Hour Pumpdown**



# Partial Pressure Calculation

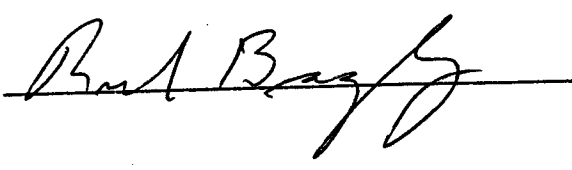
Demonstration of the Back-to-Air 100 hour pumpdown with respect to Partial Pressures

Date: 04/14/98  
 Test ID: WLEBTA (100 hr)  
 PSI Engineer: J. Flinn

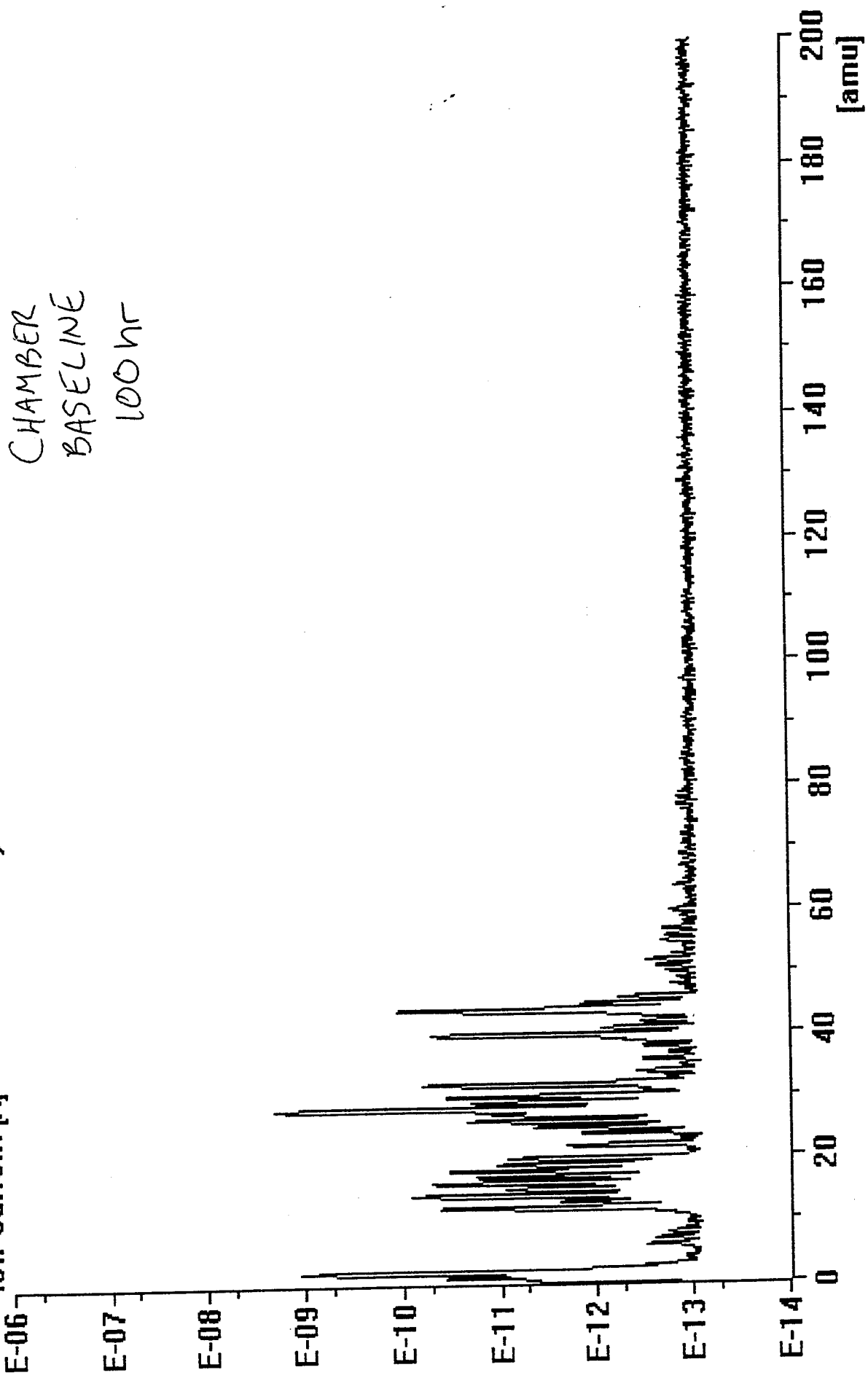
AMU	$F_{(amu)}$ transmission efficiency wrt N2	$E_{(amu)}$ ionization efficiency wrt N2	$S_{(p\_amu)}$ sensitivity (Torr/A)	$I_{(amu)}$ ion current (A)	$PP_{(amu)}$ (Torr)
2	-	-	2.87	1.14E-09	3.27E-09
16	0.57	1.60		4.85E-11	8.85E-11
18	0.64	1.12		3.40E-11	9.38E-11
28	-	-	3.87	1.98E-09	7.66E-09
44	1.57	1.42		1.11E-10	3.79E-10
all others	-	-	3.87	2.50E-10	9.68E-10

Total Pressure = 1.25E-08

LIGO: \_\_\_\_\_

PSI: 

Ion Current [A] Cycle : 5



X: 19.69 Y: 8.427801E-08 C: 5

# Partial Pressure Calculation

Demonstration of the Back-to-Air 100 hour pumpdown with respect to Partial Pressures

Date: 04/14/98  
 Test ID: WLEBTA (115 hr)  
 PSI Engineer: J. Flinn

AMU	$F_{(amu)}$ transmission efficiency wrt N2	$E_{(amu)}$ ionization efficiency wrt N2	$S_{(p\_amu)}$ sensitivity (Torr/A)	$I_{(amu)}$ ion current (A)	$PP_{(amu)}$ (Torr)
2	-	-	2.87	9.61E-10	2.76E-09
16	0.57	1.60		3.88E-11	7.08E-11
18	0.64	1.12		2.61E-11	7.20E-11
28	-	-	3.87	1.59E-09	6.15E-09
44	1.57	1.42		9.49E-11	3.24E-10
all others	-	-	3.87	1.94E-10	7.51E-10

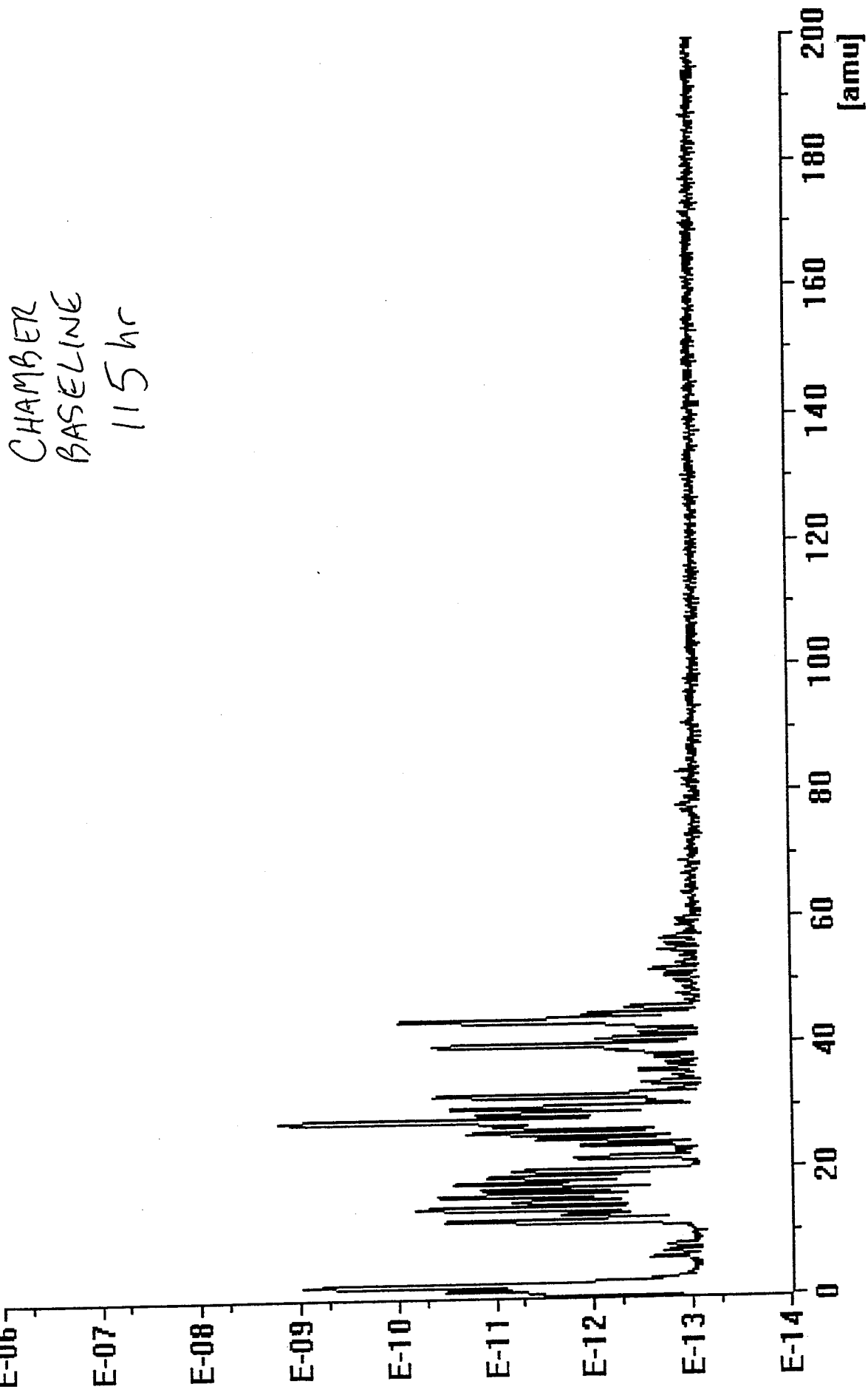
Total Pressure = 1.01E-08

LIGO: \_\_\_\_\_

PSI: Bruce Bayliss

Cycle : 7

Ion Current [A]



X: 63.28 Y: 4.422973E-09 C: 7

**LIGO VACUUM EQUIPMENT**  
**ACCEPTANCE TEST REPORT SUMMARY**

**LN<sub>2</sub> Consumption Test – Left End Station**

The LN<sub>2</sub> consumption test has been conducted per Acceptance Test Procedure V049-2-114. The duration between refills exceeded 100 days.

LIQUID NITROGEN CONSUMPTION TEST  
Ref. Spec. V049-2-208

Station WA. Left End Cryopump WCP7

Test Start Finish  
Date 5/6/98 5/16/98  
Time 7:00 11:00

Storage Tank WDW7  
14400 gallons total volume  
13700 gallons at full trycock  
13700 x 0.9 = 12330 usable gallons  
300 in.H2O level indication at full trycock  
45.67 gallons / in.H2O

Results

Starting level= 154 in.H2O  
Ending level= 131 in.H2O  
Duration= 244 Hours  
Liquid consumed= 1050.3 gallons  
Tank pressure= 15 psig  
Ave.consumption for test duration= 4.30 gal/hour  
Projected duration for usable gallons= 119.3 days

PSI *S. M. Evers* 5/16/98

LIGO *John Wouke*

**8.0 VACUUM EQUIPMENT PERFORMANCE VERIFICATION**

**8B. LEFT MID STATION**

The left end vacuum performance data is detailed in Acceptance Test Report V049-1-166.

All test results met or exceeded the requirements.

The following is a summary of that report:



## ACCEPTANCE TEST RESULTS SUMMARY

As shown in Section 3 the WA Left Mid Station has been successfully tested to meet the Acceptance Test Criteria with the following comments:

### System Leak Check

The system is believed to be leak tight to a level of  $2 \times 10^{-8}$  Torr-L/s Air. The minimum detectable leak from the RGA scan with the sensitivity obtained during the scan for the Left Mid station is about  $2 \times 10^{-8}$  Torr-liter/s. This was deduced based on mass 32 ion current. The Argon signal is not used because the pumping speed is not known accurately for Argon.

The RGA scans of just the calibration chamber, indicates that there is a leak in the calibration chamber between  $2 \times 10^{-10}$  to less than  $1 \times 10^{-9}$  Torr-liter/sec. The observed signal for mass 32 was almost  $6 \times 10^{-13}$  A with the RGA open to the main volume at an estimated conductance of 11 L/s (mass28). With the calibration chamber isolated the signal was  $9 \times 10^{-13}$  Amperes at an orifice speed of 3.7 L/s (mass28), with a calibrated sensitivity of 13 Torr/A the leak rate is estimated at  $2 \times 10^{-10}$  Torr-L/s. Helium leak checking of the RGA chamber indicates the chamber was tight to  $1 \times 10^{-9}$  Torr-L/s.

The RGA was subsequently moved to a 2.5 inch metal valve (back-to air) on the main volume and the mass 32 signal dropped to  $1.5 \times 10^{-13}$  Amperes, just above the noise baseline. The corresponding detectable leak using the same RGA sensitivity is about  $2 \times 10^{-8}$  Torr liter/sec.

### System Bakeout

The bakeout ramp up and ramp down rates exceeded the specified rate. The design ramp rates were selected to minimize thermal stress and to keep input power requirements at reasonable levels. The actual ramp rates, although in excess of the acceptance criteria are still low and are not considered to be sufficient to cause thermal stresses, and are therefore acceptable.

The loss of the temperature data is unfortunate, but the subsequent excellent RGA scans after bakeout indicate that the system is clean and the bakeout was therefore effective.

LEFT MID STATION

**Ultimate Pressure Test**

The partial pressure measurements after bakeout readily exceeded the acceptance criteria and match very well with the LIGO goals indicating that the volume is clean and leak tight. A comparison table of the actual results vs. the LIGO is included for information.

AMU	LIGO Goals	Acceptance Test
	Partial Pressure	Partial Pressure
(Torr)	(Torr)	(Torr)
2	$5 \times 10^{-9}$	$6.2 \times 10^{-9}$
16	$2 \times 10^{-10}$	$1.0 \times 10^{-10}$
18	$5 \times 10^{-9}$	$5.2 \times 10^{-10}$
28	$1 \times 10^{-9}$	$9.7 \times 10^{-10}$
44	$2 \times 10^{-10}$	$2.6 \times 10^{-11}$
Other	$1.9 \times 10^{-9}$	$7.8 \times 10^{-11}$

**Backfill/100 Hour Pumpdown Test**

A comparison of the partial pressures before and after the backfill is shown below. As expected an approximate one-decade increase in N<sub>2</sub> and CO<sub>2</sub> pressures are observed. This is consistent with the prototype test program. Negligible increases are shown for H<sub>2</sub>O and CH<sub>4</sub> indicating that the clean air system is effective.

	After Bakeout	After Backfill & 100 hr Pumpdown
AMU	Partial Pressure	Partial Pressure
	(Torr)	(Torr)
2	$6.2 \times 10^{-9}$	$6.8 \times 10^{-9}$
16	$1.0 \times 10^{-10}$	$1.3 \times 10^{-10}$
18	$5.2 \times 10^{-10}$	$2.0 \times 10^{-10}$
28	$9.7 \times 10^{-10}$	$5.7 \times 10^{-9}$
44	$2.6 \times 10^{-11}$	$3.9 \times 10^{-10}$
Other	$7.8 \times 10^{-11}$	$8.5 \times 10^{-10}$

**LN2 Consumption**

This test was not performed and will be completed as part of the punch list.

LEFT MID STATION

**Noise/ Shock/Vibration**

The vacuum requirement contract only has a requirement for shock levels. Noise and vibration testing were connected for information only.

The large gates exceeded the specification requirement (approximately .03g Vs .01g specification requirement.)

LEFT MID STATION

**ACCEPTANCE TEST CRITERIA**

Item	Acceptance Criteria	Acceptance Results
Interface to CDS	Functional Checkout per V049-2-163	Checkout completed on 1/16/98
Clean Air System Test	Functional Checkout per V049-2-109 Dewpoint: <-60 C Particle Count: Class 100 @ .5 micrometer. Hydrocarbon Check:	Dewpoint: -75.3 C Particle Count: 0 Hydrocarbon Check: 0 PPM
Class 100 Cleanroom Test	Functional Checkout per V049-2-110 Particle Count: <100	Particle Count: <80.6
System Leak Check	Individual leaks greater than $1 \times 10^{-9}$ torr-L/s will be repaired.  Vacuum Check: Annulus: $P < 3 \times 10^{-4}$ torr 60 min for vessels and 30 min for spools and ate valves.  Main Volume: by RGA air signature. Maximum rate to be consistent with system requirements and RGA sensitivity.	All components comprising the isolatable volume were helium leak checked via evacuation and spray prior to bakeout.  All flange annuli checked and passed. Data recorded in site test logs.  The station is leak tight to sensitivity of RGA air signature. For the Left Mid Station this $< 2 \times 10^{-8}$ Torr-l/s.
System Bake-out	Functional Checkout per V049-2-112 Rev1 Bakeout: Ramp Rate: <1C/hour Uniformity: 150 C +/- 20C	The station was ramped from 19 C to 150 C over a period of 67 hours (2 C/hr) and held for 49 hours at 150C. Temperature data recorded in the bakeout cart data acquisition system was subsequently overwritten; therefore no temperature uniformity data is available. After the 48-hour hold, the temperature was ramped to 48 C over 48.5 hours (2.1C/hr) prior to shutting off the power.

LEFT MID STATION

Item	Acceptance Criteria	Acceptance Results																
Ultimate Pressure Test (After Bake-out)	Total Pressure: $<2 \times 10^{-8}$ torr Partial Pressure Measurements: Sum of all gasses other than H <sub>2</sub> and H <sub>2</sub> O: $<3 \times 10^{-9}$ torr	Total Pressure: $8.2 \times 10^{-9}$ torr Partial Pressure Measurements: Sum of all gasses other than H <sub>2</sub> and H <sub>2</sub> O: $1.4 \times 10^{-9}$ torr																
Backfill/100 Hr. Pumpdown Test	Roughing to $< 0.2$ torr in 15 hours Roughing to $5 \times 10^{-6}$ torr in 24 hours RGA scan after 100 hours for information only	Roughing to 0.2 torr in 5 hours Roughing to $2 \times 10^{-7}$ torr in 8 hours Partial pressures: <table style="margin-left: auto; margin-right: auto;"> <tr> <td style="padding-right: 20px;">AMU</td> <td>torr</td> </tr> <tr> <td>2</td> <td><math>7 \times 10^{-9}</math></td> </tr> <tr> <td>16</td> <td><math>1 \times 10^{-10}</math></td> </tr> <tr> <td>18</td> <td><math>2 \times 10^{-10}</math></td> </tr> <tr> <td>28</td> <td><math>6 \times 10^{-9}</math></td> </tr> <tr> <td>44</td> <td><math>4 \times 10^{-10}</math></td> </tr> <tr> <td>all others</td> <td><math>8 \times 10^{-10}</math></td> </tr> <tr> <td>Total</td> <td><math>1.4 \times 10^{-8}</math></td> </tr> </table>	AMU	torr	2	$7 \times 10^{-9}$	16	$1 \times 10^{-10}$	18	$2 \times 10^{-10}$	28	$6 \times 10^{-9}$	44	$4 \times 10^{-10}$	all others	$8 \times 10^{-10}$	Total	$1.4 \times 10^{-8}$
AMU	torr																	
2	$7 \times 10^{-9}$																	
16	$1 \times 10^{-10}$																	
18	$2 \times 10^{-10}$																	
28	$6 \times 10^{-9}$																	
44	$4 \times 10^{-10}$																	
all others	$8 \times 10^{-10}$																	
Total	$1.4 \times 10^{-8}$																	
LN <sub>2</sub> Consumption Test	LN2 consumption per V049-2-208 90 days without refill.	LN2 consumption test not performed. Test will be performed later as part of the punch list.																
Noise/Shock/Vibration Field Test	Per CAA Test Plan	See CAA Test Report in Section 5.9																

**LIGO VACUUM EQUIPMENT**  
**ACCEPTANCE TEST REPORT SUMMARY**

**Backfill/100 Hr. Pumpdown Test – Left Mid Station**

The backfill and 100 hr. pumpdown test was conducted per Acceptance Test Procedure V049-2-114.

The roughing and turbo pumping requirements met or exceeded the requirements.

The ultimate pressure and partial pressure results are detailed herein. This test was for demonstration purposes only.

# Partial Pressure Calculation

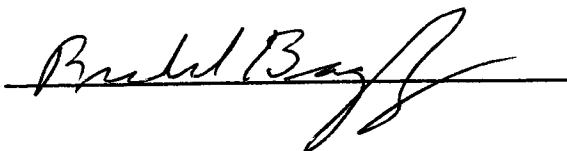
Demonstration of the Back-to-Air 100 hour pumpdown with respect to Partial Pressures

Date: 05/05/98  
 Test ID: WLMBTA (100 hr)  
 PSI Engineer: J. Flinn

AMU	$F$ (amu) transmission efficiency wrt N <sub>2</sub>	$E$ (amu) ionization efficiency wrt N <sub>2</sub>	$S$ (p_amu) sensitivity (Torr/A)	$I$ (amu) ion current (A)	$PP$ (amu) (Torr)
2	-	-	4.66	1.45E-09	6.76E-09
16	0.57	1.60		4.85E-11	1.25E-10
18	0.64	1.12		5.25E-11	2.04E-10
28	-	-	5.45	1.05E-09	5.72E-09
44	1.57	1.42		8.10E-11	3.89E-10
all others	-	-	5.45	1.55E-10	8.45E-10

Total Pressure =	1.40E-08
------------------	----------

LIGO: \_\_\_\_\_

PSI: 

Left Mid Station Back-to-Air 100 Hour Pumpdown

04/28/98 800 Start clean air purge with cryopumps isolated by GV10, GV11  
Ion pump running and 14" valve closed

04/29/98 800 End clean air purge  
800 Start rough pumping system with QDP80  
1300 P=0.2 Torr  
Start turbo pumping system with STP2000C  
1600 P=2.0e-7 Torr - Turbo tripped out (Emergency Operation, 5 hour shutdown)

04/30/98 700 Restart turbopump  
830 Fill Cryopump WCP3 (WCP4 will remain isolated  
from the 100 hour pumpdown test)  
Open GV11 (44" gate valve) to WCP3  
1300 P=2.0E-8 Torr at turbo  
PT245= 1.8E-8 Torr  
1345 Ion Pump (Voltage=3000V, Amperage=1.8E-5A)  
1350 Open 14" gate valve  
Close 10" gate valve to isolate STP2000C  
1355 PT245=1.08E-8 Torr  
Ion Pump (Voltage=3000V, Amperage=1.6E-4A)

05/01/98 700 PT245=9.0E-9 Torr

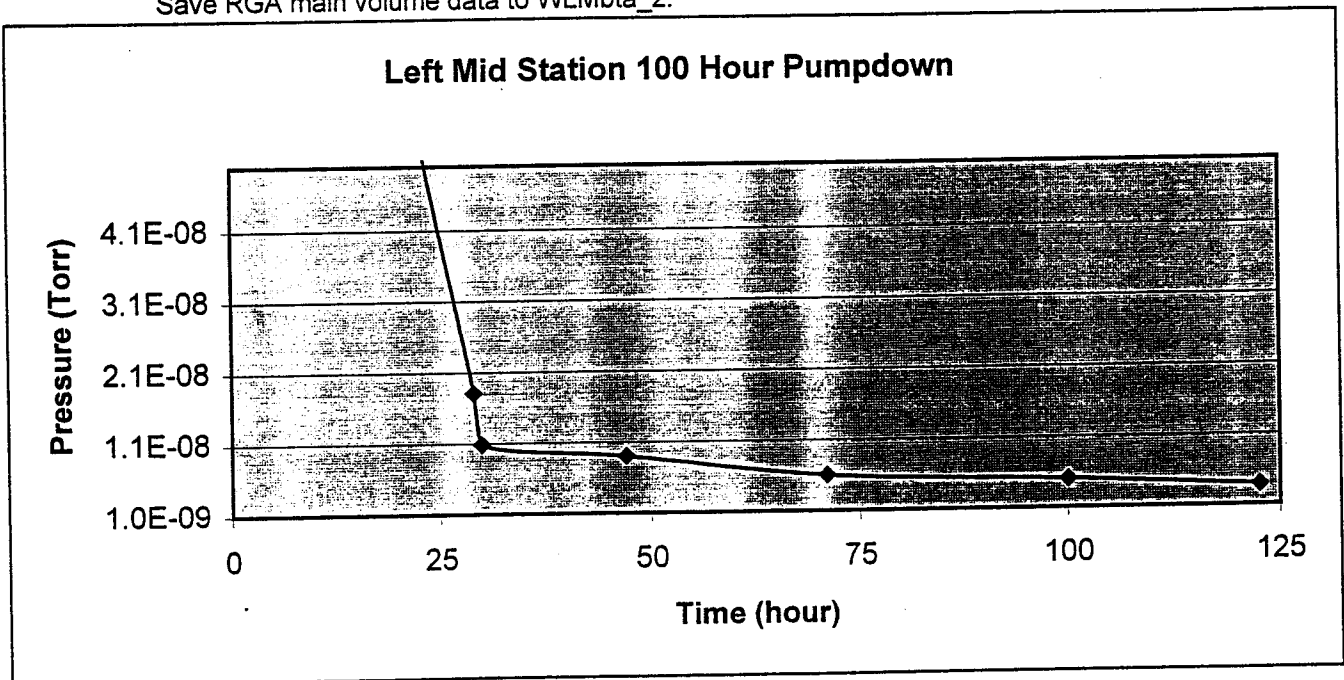
05/02/98 700 PT245=6.0E-9 Torr  
Ion Pump (Voltage=3000V, Amperage=1.0E-4A)

05/03/98 1200 PT245=5.0E-9 Torr End of 100 hour test  
Ion Pump (Voltage=3000V, Amperage=9.0E-5A)

05/04/98 1030 PT245=3.9E-9 Torr  
Ion Pump (Voltage=3000V, Amperage=7.0E-5A)

Graphical Data	
Time (hr)	Press (torr)
0	760
5	0.2
8	2.00E-07
29	1.80E-08
29.92	1.08E-08
47	9.00E-09
71	6.00E-09
100	5.00E-09
122.5	3.90E-09

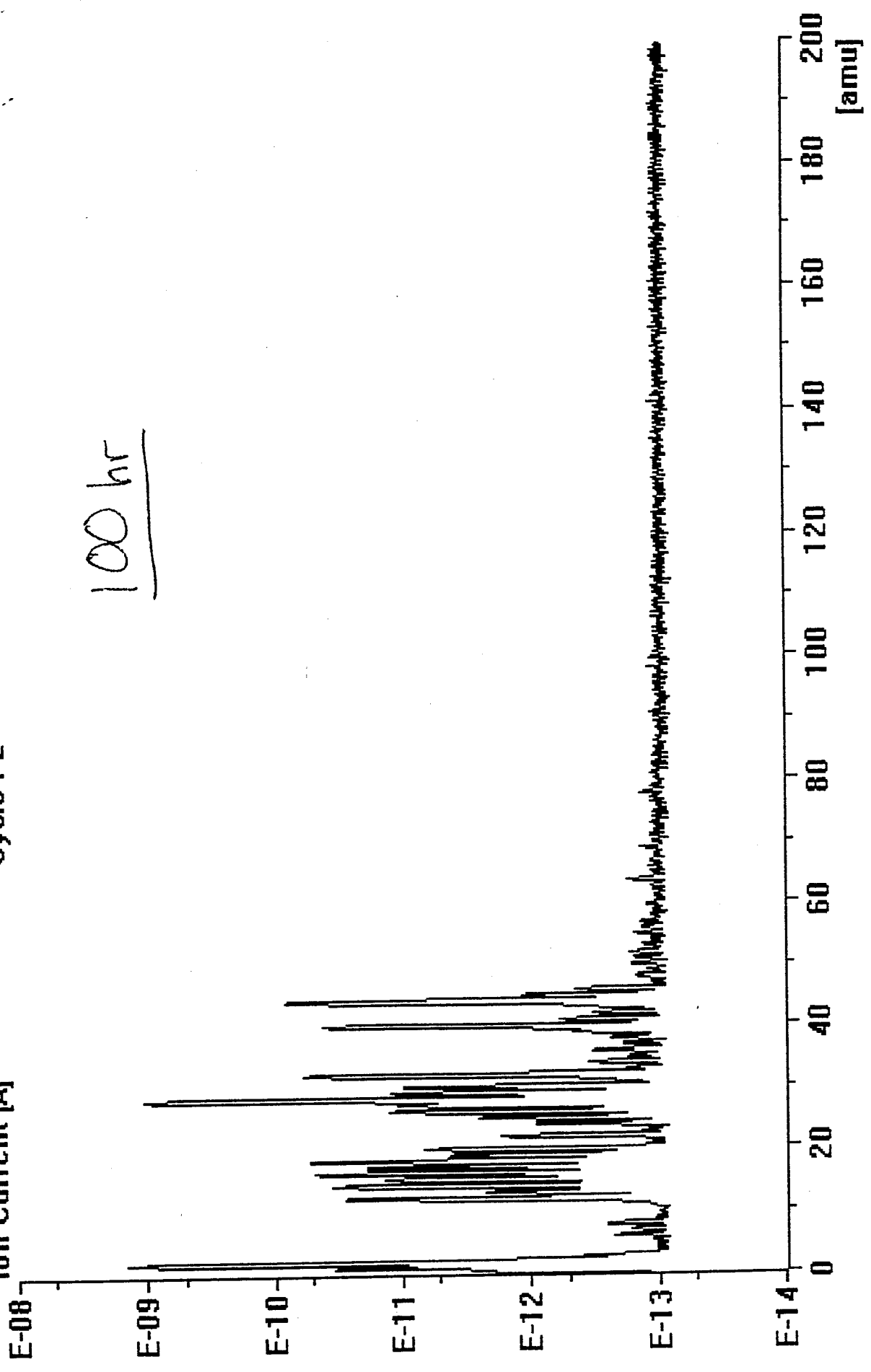
Save RGA calibration data to WLMbta\_1.\*\*\*  
Save RGA main volume data to WLMbta\_2.\*\*\*





Ion Current [A] Cycle : 2

100 hr



# Partial Pressure Calculation

Demonstration of the Back-to-Air 100 hour pumpdown with respect to Partial Pressures

Date: 05/05/98  
 Test ID: WLMBTA (100 hr)  
 PSI Engineer: J. Flinn

AMU	$F$ (amu) transmission efficiency wrt N2	$E$ (amu) ionization efficiency wrt N2	$S$ (p_amu) sensitivity (Torr/A)	$I$ (amu) ion current (A)	$PP$ (amu) (Torr)
2	-	-	4.66	1.45E-09	6.76E-09
16	0.57	1.60		4.85E-11	1.25E-10
18	0.64	1.12		5.25E-11	2.04E-10
28	-	-	5.45	1.05E-09	5.72E-09
44	1.57	1.42		8.10E-11	3.89E-10
all others	-	-	5.45	1.55E-10	8.45E-10

Total Pressure = 1.40E-08

LIGO: \_\_\_\_\_

PSI: Bruce Bayl

# Partial Pressure Calculation

Demonstration of the Back-to-Air 100 hour pumpdown with respect to Partial Pressures

Date: 05/05/98  
 Test ID: WLMBTA (123 hr)  
 PSI Engineer: J. Flinn

AMU	$F$ (amu) transmission efficiency wrt N2	$E$ (amu) ionization efficiency wrt N2	$S$ (p_amu) sensitivity (Torr/A)	$I$ (amu) ion current (A)	$PP$ (amu) (Torr)
2	-	-	4.66	1.14E-09	5.31E-09
16	0.57	1.60		3.40E-11	8.73E-11
18	0.64	1.12		3.68E-11	1.43E-10
28	-	-	5.45	8.00E-10	4.36E-09
44	1.57	1.42		5.00E-11	2.40E-10
all others	-	-	5.45	1.20E-10	6.54E-10

Total Pressure =	1.08E-08
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LIGO: \_\_\_\_\_

PSI: Bud Bay

**LIGO VACUUM EQUIPMENT**  
**ACCEPTANCE TEST REPORT SUMMARY**

**Ultimate Pressure Test (After Bake-out) – Left Mid Station**

The ultimate pressure test was conducted per Acceptance Test Procedure V049-2-114.

All test results met or exceeded the requirements.

# Partial Pressure Calculation

Acceptance of the Bakeout with respect to Air Signature and Partial Pressures

Date: 03/18/98  
 Test ID: WLMRGA  
 PSI Engineer: J. Flinn

AMU	$F_{(amu)}$ transmission efficiency wrt N2	$E_{(amu)}$ ionization efficiency wrt N2	$S_{(p\_amu)}$ sensitivity (Torr/A)	$I_{(amu)}$ ion current (A)	$PP_{(amu)}$ (Torr)
2	-	-	9.75	6.39E-10	6.23E-09
16	0.57	1.60		1.69E-11	1.04E-10
18	0.64	1.12		5.64E-11	5.24E-10
28	-	-	13.03	7.44E-11	9.69E-10
44	1.57	1.42		2.27E-11	2.61E-10
all others	-	-	13.03	6.00E-12	7.82E-11

		<u>LIGO Contract Limits</u>	<u>Actual</u>	<u>Pass</u>
Primary Criteria -	Total Pressure:	2.00E-08 Torr	8.17E-09 Torr	Yes
Secondary Criteria -	Others except H2 & H2O:	3.00E-09 Torr	1.41E-09 Torr	N/A

LIGO: John Worder

PSI: Paul Bayly

### Minimum Detectable Air Leak due to RGA Sensitivity at Left Mid Station

Ion current for mass 32 is  $1.5 \times 10^{-13}$  A. We will assume that no  $O_2$  is consumed or produced and that the signal is due to an air leak.

Use the standard composition of atmospheric air (~80%  $N_2$ , ~20%  $O_2$ ). This concludes that the mass 28 ion current contribution is  $6.0 \times 10^{-13}$  A. The sum is then  $7.5 \times 10^{-13}$  A.

We also must assume that the calibration factors have not changed since the RGA was moved. The sensitivity for  $N_2$  is 13 Torr/A. Therefore,

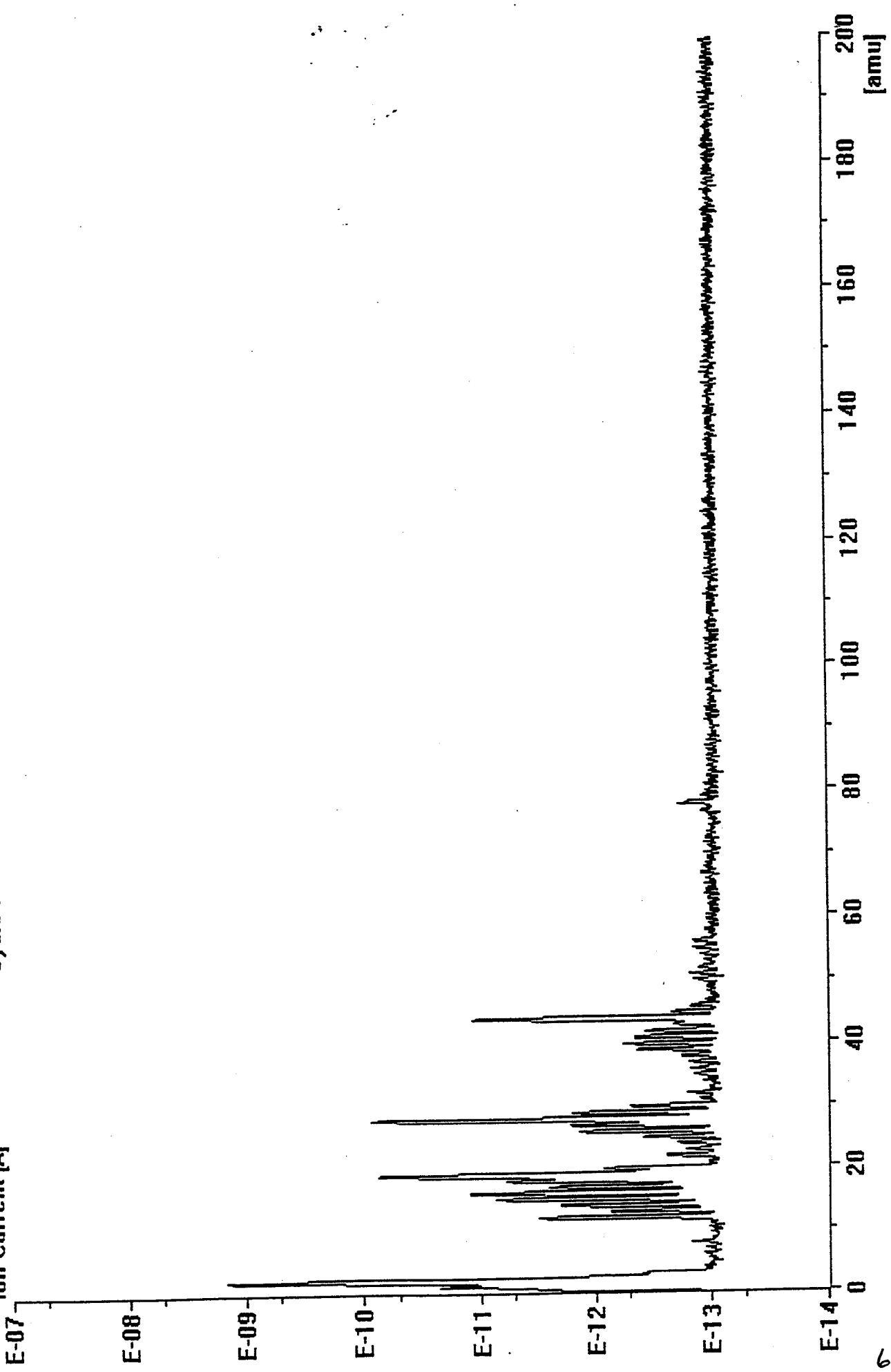
$$PP_{Air} = S_{N_2} \cdot IC_{N_2} = (13 \text{ Torr / A}) \cdot (7.5 \times 10^{-13} \text{ A}) = 9.75 \times 10^{-12} \text{ Torr}$$

The published 2500 l/s ion pump pumping speed for  $N_2$  at  $1 \times 10^{-8}$  Torr is 2200 l/s. This leads to the finding that the minimum detectable leak (MDL) is

$$MDL = (9.75 \times 10^{-12} \text{ Torr}) \cdot (2200 \text{ l / s}) = 2.1 \times 10^{-8} \text{ Torr - l / s}$$

Cycle : 6

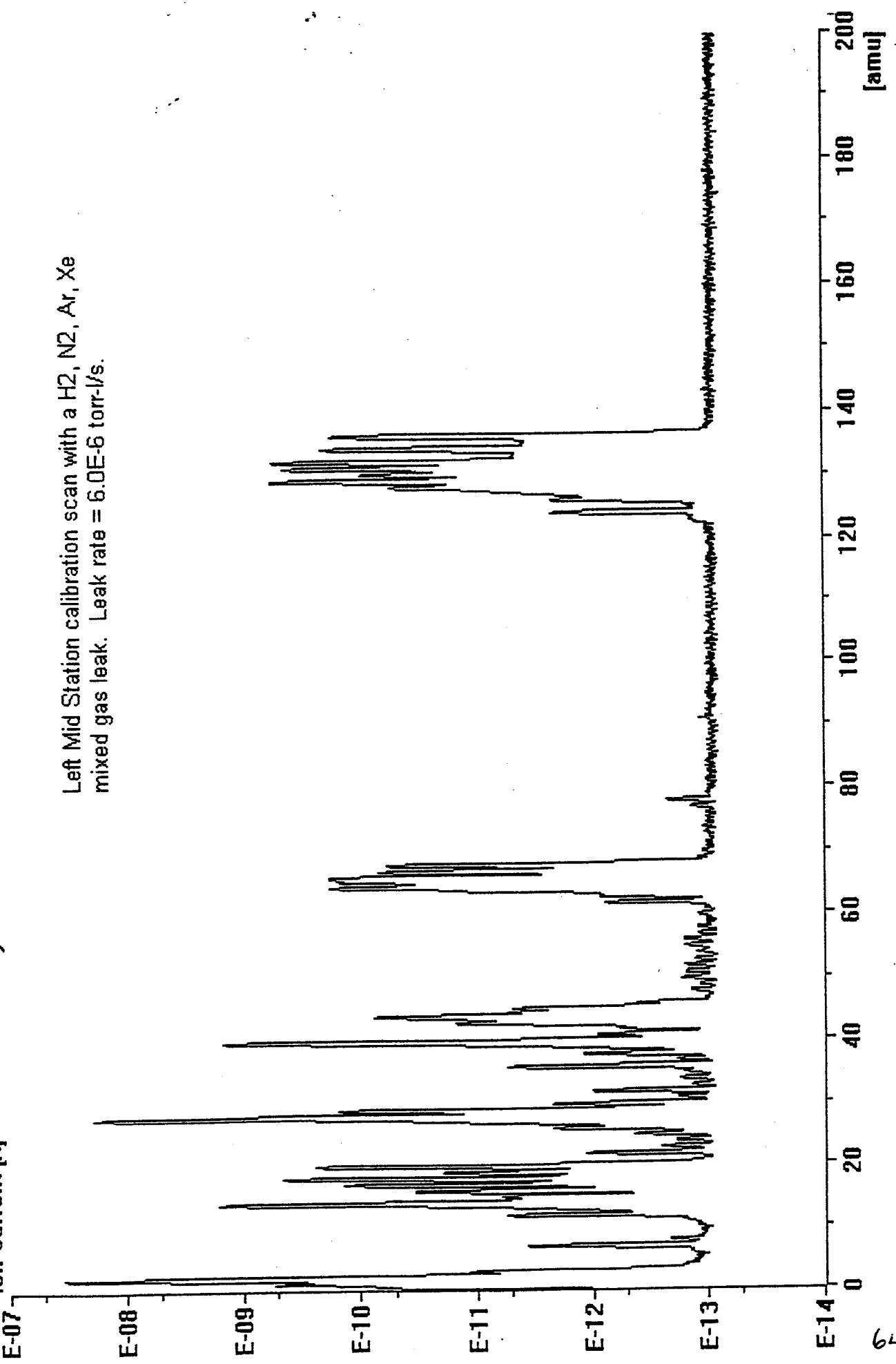
Ion Current [A]



Cycle : 7

Ion Current [A]

Left Mid Station calibration scan with a H2, N2, Ar, Xe mixed gas leak. Leak rate = 6.0E-6 torr-l/s.





**LIGO VACUUM EQUIPMENT**  
**ACCEPTANCE TEST REPORT SUMMARY**

**LN<sub>2</sub> Consumption Test – Left Mid Station**

The LN<sub>2</sub> consumption test will be conducted per Acceptance Test Procedure V049-2-114.

It is presently a punch list item.

**LIGO VACUUM EQUIPMENT**  
**ACCEPTANCE TEST REPORT SUMMARY**

**Noise/Shock/Vibration Field Test – Left Mid Station**

The noise/shock/vibration field testing was conducted by Cambridge Acoustical Associates (approximately .03g vs. .01g specification requirements).

SAMPLE  
1 OF 8

**VIBRATION, NOISE, SHOCK MEASUREMENTS OF THE PSI VACUUM  
EQUIPMENT AT THE LIGO END AND MID STATION  
HANFORD, WA**

**Prepared By:  
Kyle Martini**

**June 1998**

**Test Report  
U-2379-8001**

**Prepared for:  
Process Systems International, Inc.  
20 Walkup Drive  
Westborough, MA 01581-5003  
PSI Purchase Order 554-386-00**

**Cambridge Acoustical Associates, Inc.  
A Department of Engineering Technologies  
84 Sherman Street  
Cambridge, MA 02140-3261**

## I. INTRODUCTION AND SUMMARY

The first phase of the LIGO commission test for vibration, noise, and shock has been completed at the Hanford, WA end- and mid- stations. Acoustic and vibration measurements were recorded on or near the chambers in these facilities with individual PSI vacuum equipment operating and the facility in a "quiet mode". Background measurements were also recorded. In addition manual and motorized valves were open and closed while shock measurements were recorded on the valve and on the chambers.

The results of the measurements are summarized as follows:

A. The background vibration levels, "quiet mode" (see Section II.A.2), are significantly higher than the LIGO vacuum equipment specification, and typically fluctuates about the higher LIGO building vibration specification. When measuring the vibration levels due to the operation of the vacuum equipment, the background vibration dominates much of the frequency range.

B. Operating the ion pump does not measurably increase the vibration levels.

C. Excitation frequencies of the molecular turbopump are 48 and 54 Hz due to the pump's controller, 280 Hz of unknown origin, and its spin frequency of 450 Hz and higher harmonics. A broadband resonance of the beamsplitter at 300 Hz amplified the 280 Hz excitation frequency. The vibration isolation system designed for the turbopump was short circuited during measurements to prevent the bellows from collapsing. This transmitted higher vibration than expected.

D. The excitation caused by boiling in the cryopump is broadband and tends to increase the overall level of vibration. Controlling the boil process is essential in minimizing vibration. During our measurements, we varied the operation of the cryopump (see Sections II.A.4.d and III.A.5) and significantly changed the levels of vibration. At the lower frequencies there is a 10 dB reduction in level across the beam manifold bellows between the cryopump and the beamsplitter. Overall reduction in the

resonance response to the broadband excitation of cryopump as well as the background noise could be achieved by increasing the effective loss factor of the structure.

E. The noise measured during the operation of the turbopump did not meet the LIGO's noise specification above 125 Hz, as expected. A properly installed noise enclosure around the pump and its controller would reduce the noise level to the rooms background level, which also does not meet specification above 125 Hz.

F. Shock measurements on the beamsplitter chamber, when the manual valves were opened or closed, met or slightly exceeded LIGO's revised shock specification, with the exception of the 14" ion pump valve in the mid station. When the spring loaded mechanism released during opening of this valve, the specification was exceeded by a factor of 2.7. Levels on the valve body were significantly higher for all valves.

G. When operating the large gate valves, the levels on the chamber were 3-4 times greater than the specification. Levels on the large gate valve's body were not as high as for the manual valves.

H. The results at the mid-station overall are similar to the end-station, with narrow band variation.





Fig. 5

LIGO PROJECT / WASHINGTON / END STATION  
Noise levels in Vacuum Equipment Space

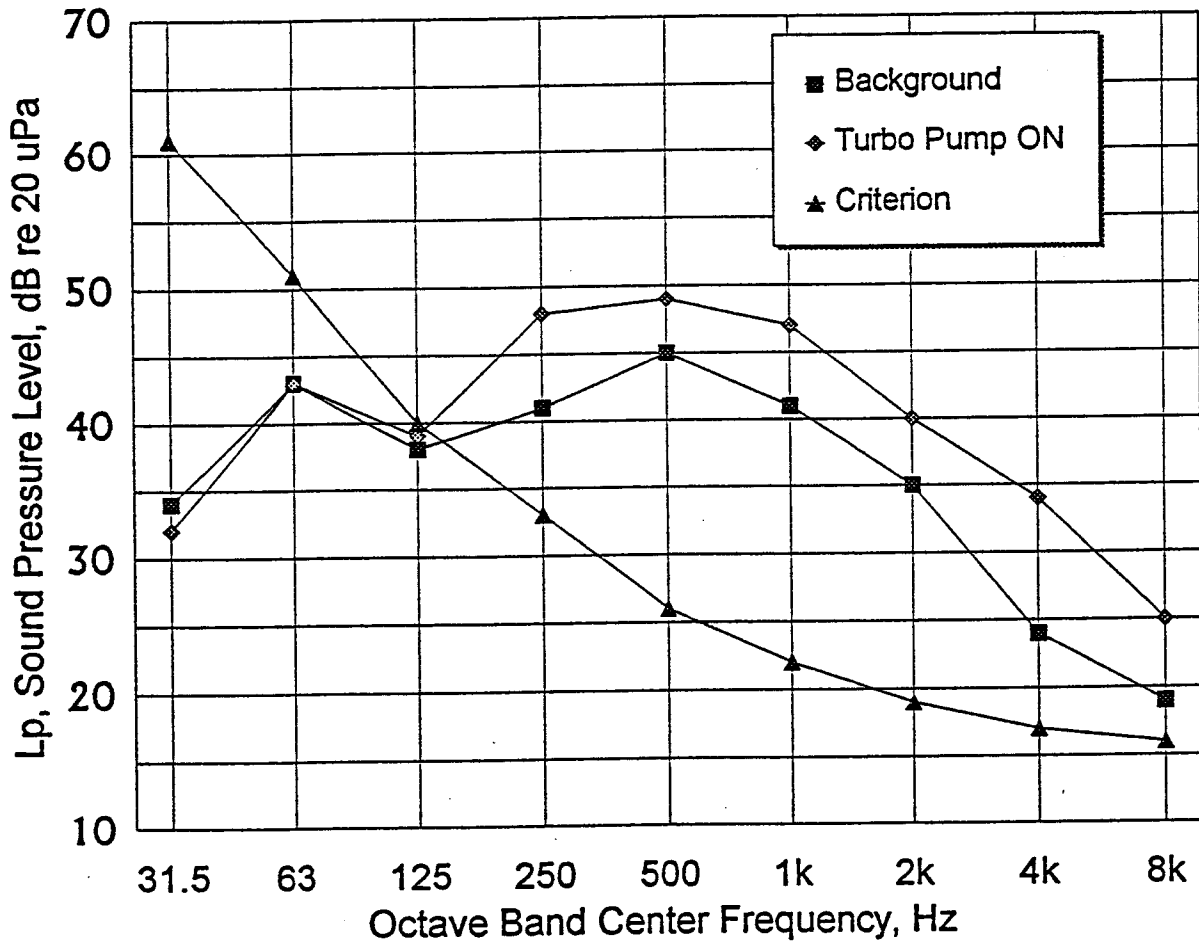
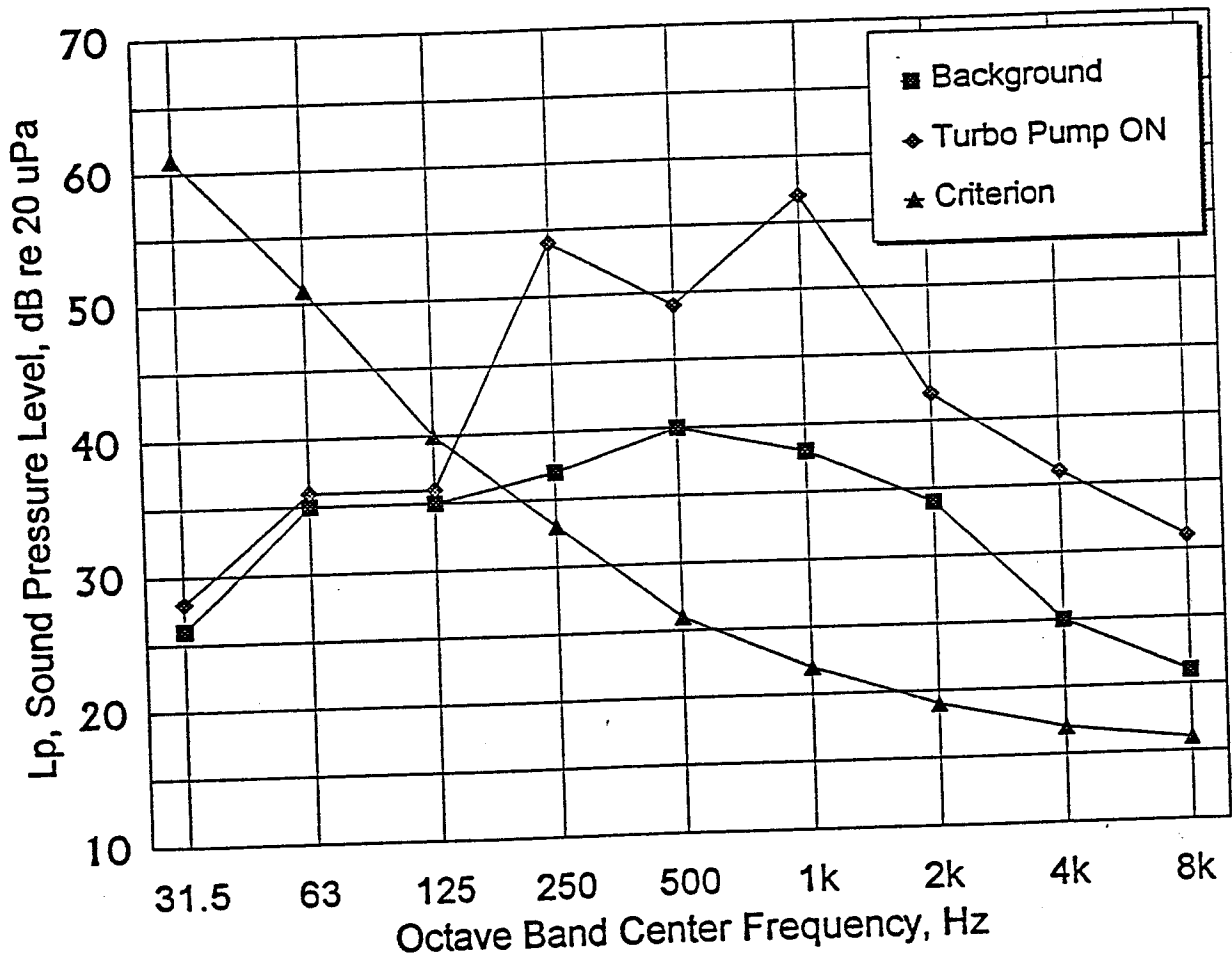
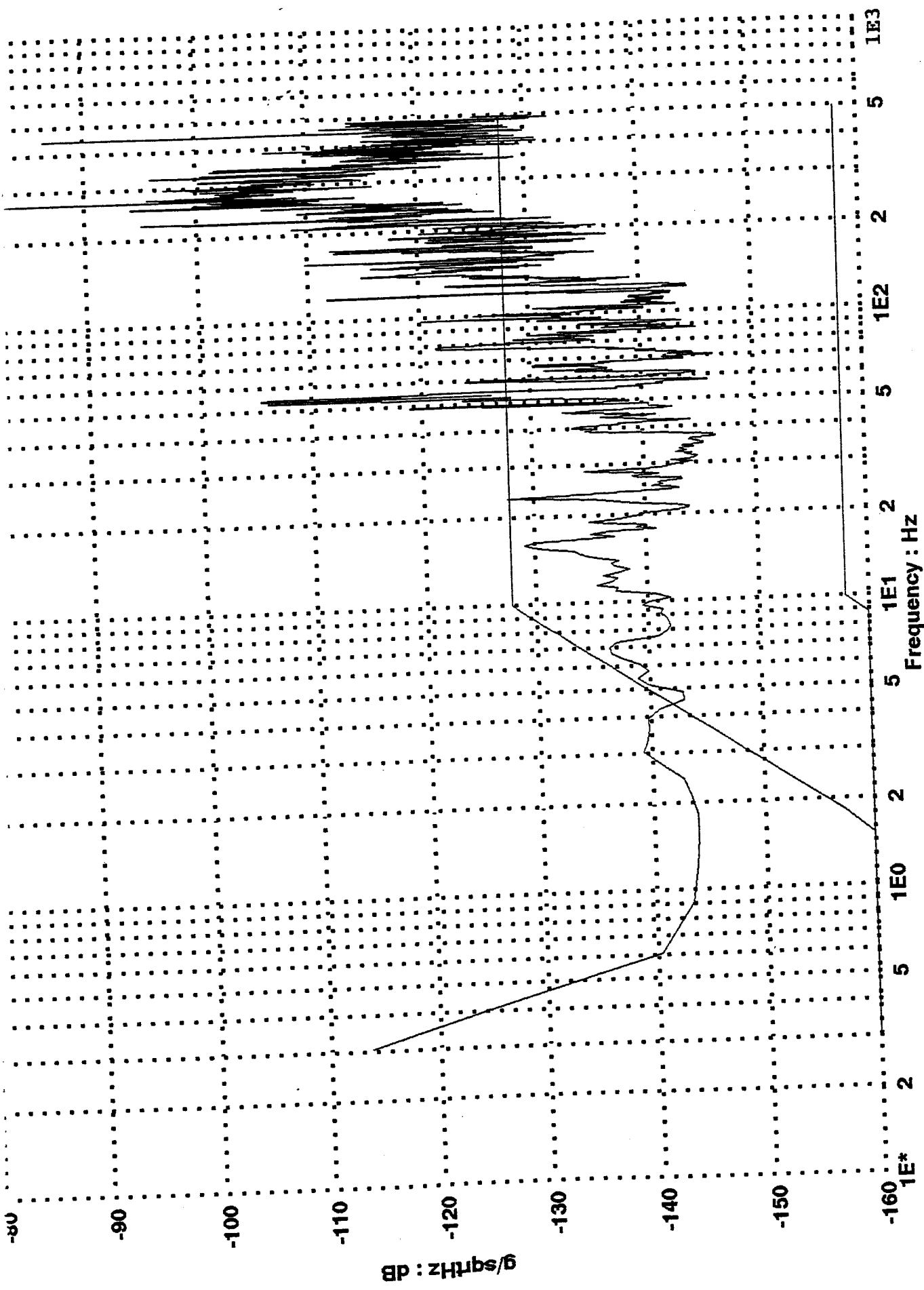




Fig. 6

LIGO PROJECT / WASHINGTON / MID STATION  
Noise levels in Vacuum Equipment Space





DF: 0.31 Hz T-Lo: 0.ms T-Hi: 3277.ms FFT: 4096 Wind:HANN Sm: 0.  
E1-14 4/20/98 End Station: BS noz G, circ. dir., turbo. source

## **9.0 SYSTEM DOCUMENTATION**

The left end station vacuum equipment design and performance is detailed by the following documentation:

- As-built Drawings
- Quality Documentation
- Acceptance Test Reports
- Operating and Maintenance Manuals

## **10.0 DISPOSITION OF EQUIPMENT**

All deliverable equipment will be installed in each station when it is accepted by LIGO.

The common equipment (bake-out blankets, cart, etc.) will be turned over to LIGO with the last LA site building.

Caltech did not furnish any equipment to PSI as part of this building installation and commissioning.

## **11.0 EQUIPMENT WARRANTY**

Vacuum equipment warranty periods are based on when LIGO took possession of the equipment. The warranty period for the early deliverables (Washington beam tube valves, Washington beam tube pumps, etc.) has expired.

The warranty period for each piece of equipment in each building will be detailed in a separate document provided after LIGO accepts or takes possession of each building.

**12.0 OPEN PUNCH LIST ITEMS**

*Meeting Handout*

**13.0 GNB VALVE MODIFICATIONS/STATUS**

*Meeting Handout*

**ATTACHMENT I**

**V049-1-169**

**As-built Drawings**

[See Separate "B" Size Package]



**ATTACHMENT II**

**V049-1-169**

**End Item Documentation Package**

[Table of Contents Only]

 LIGO PROJECT  
MAJOR COMPONENT  
END ITEM DOCUMENTATION PACKAGE  
FOR WASHINGTON LEFT MID STATION

<i>TAG NO.</i>	<i>SER. NO.</i>
WBSC6	07
WCP3	01
WCP4	01
WA1A	01
WA7B1	01
WA14A	01
WBE4A	01
WBE4B	02

GNB GATE VALVES

WGV 12	003
WGV 09	004
WGV 10	010
WGV 18	016

PSI DOCUMENTATION NO. V049-1-171 Rev.0  
VOLUME 1

 LIGO PROJECT  
MAJOR COMPONENT  
END ITEM DOCUMENTATION PACKAGE  
FOR WASHINGTON LEFT MID STATION

<i>TAG NO.</i>	<i>SER. NO.</i>
WBSC6	07
WCP3	01
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GNB GATE VALVES

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PSI DOCUMENTATION NO. V049-1-171 Rev.0  
VOLUME 2

 LIGO PROJECT  
MAJOR COMPONENT  
END ITEM DOCUMENTATION PACKAGE  
FOR WASHINGTON LEFT END STATION

<i>TAG NO.</i>		<i>SER. NO.</i>
WBSC10		01
WBE4C		03
WCP7		02
WA1B		02
WA7B		02
	GNB GATE VALVES	
WGV 17		008
WGV 11		009

PSI Documentation No. V049-1-170 Rev.0  
VOLUME 1

 **LIGO PROJECT**  
**MAJOR COMPONENT**  
**END ITEM DOCUMENTATION PACKAGE**  
**FOR WASHINGTON LEFT END STATION**

<i>TAG NO.</i>		<i>SER. NO.</i>
WBSC10		01
WBE4C		03
WCP7		02
WA1B		02
WA7B		02
	<b>GNB GATE VALVES</b>	
WGV 17		008
WGV 11		009

PSI Documentation No. V049-1-170 Rev.0  
VOLUME 2

## **ATTACHMENT III**

**V049-1-169**

### **Washington Site Contractor QA Data**

1. Left Arm Alignment
2. Left Arm Testing (Pressure Testing)
3. Left Arm Welding Inspection/X-ray



**PROCESS SYSTEMS INTERNATIONAL, INC.**

20 Walkup Drive, Westborough, MA 01581

⚡ **LIGO PROJECT**  
**SUB-VENDOR QA DOCUMENTATION DATA**

**TABLE OF CONTENTS**

**A&N CORP**  
**EDWARDS HIGH VACUUM INTL.**  
Varian (conflats, ion pumps, small gate valves)  
**EDWARDS ENGINEERING ( chillers)**  
FIBA Ambient Air Vaporizers  
**PROCESS ENGINEERING INC. (LN2 storage tanks)**  
**BADGER METER CRYOVAVLES**  
J. ROYAL ( viton o-rings )  
MERIDEN ( rotometers )  
ROSEMONT ( level & pressure trans. )  
LINDCO (relief valves, burst disk)  
CVI (vj piping)

PSI DOC. NO. V049-1-180