
Stanford Gravitational Wave Group

Edge-Pumped Slab Amplifier Development

Bill Tulloch, Todd Rutherford, Eric K. Gustafson,
and Robert L. Byer

tulloch@loki.stanford.edu

LSC Working Group Meeting
University of Florida at Gainesville

March 5, 1999

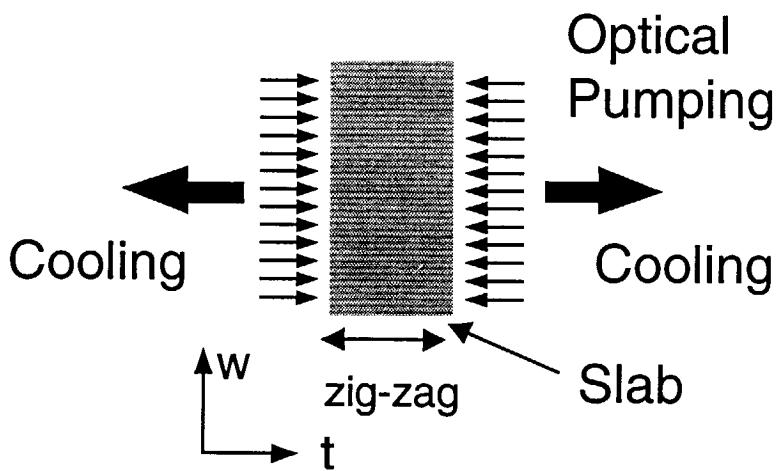
Stanford High Power Laser Lab

LIGO-G990022-34-M

Outline

- **Edge-pumped Slab Laser Development**
 - Edge-Pumping Geometry
 - 1:1 Slab Results
 - Slab Temperature - Thermal Population Loss
 - 3:1 Slab - Design and Preliminary Results
 - **Amplifier Research**
 - Predicted Amplifier Performance
 - Wavelength Temperature Tuning
 - **Summary and Conclusions**
 - **6 Month Research Plan for 10 W LIGO Master Oscillator**
-

Face-Pumping vs. Edge-Pumping

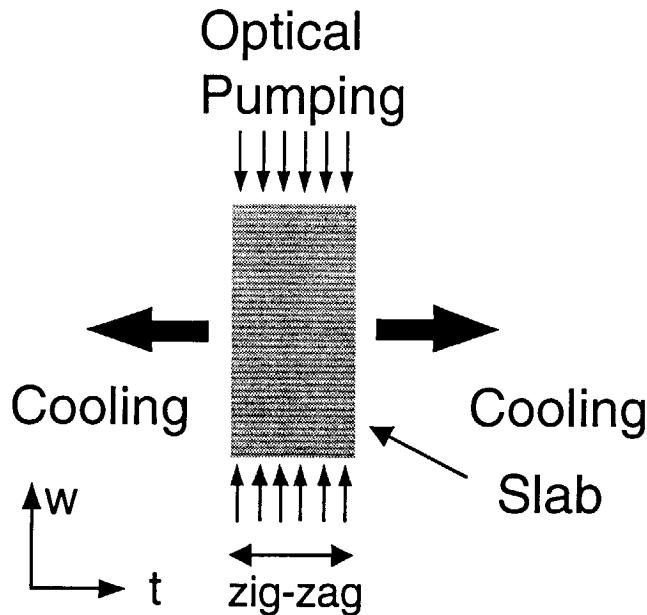


Face - Pumped

Cooling Face = Pumping Face

Stress Fracture $\propto (w/t)$

Pump Absorption depends on t



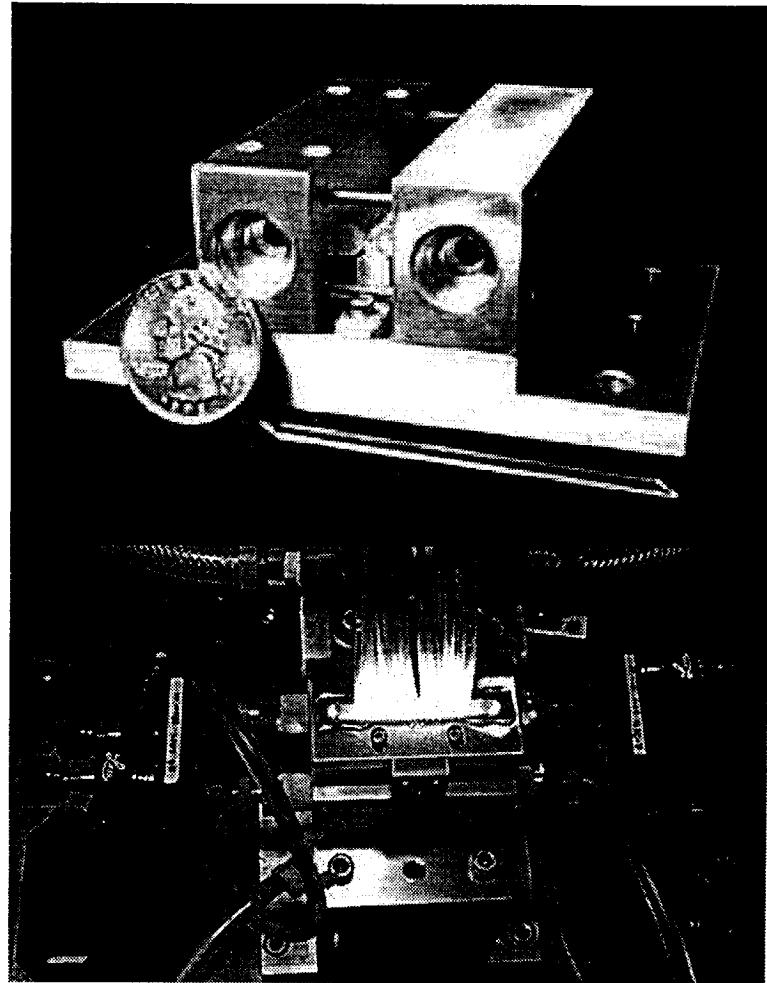
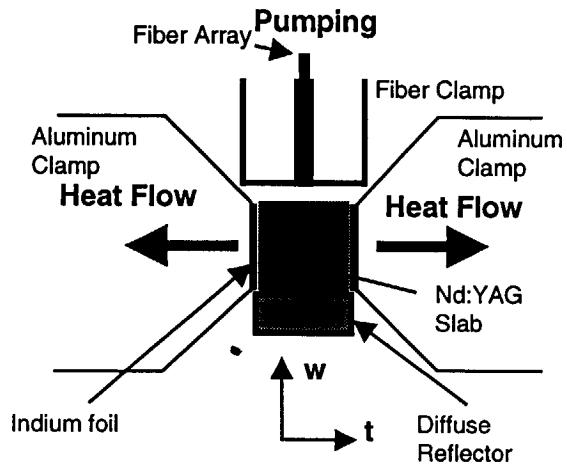
Edge - Pumped

Cooling Face \neq Pumping Face

Stress Fracture $\propto (w/t)$

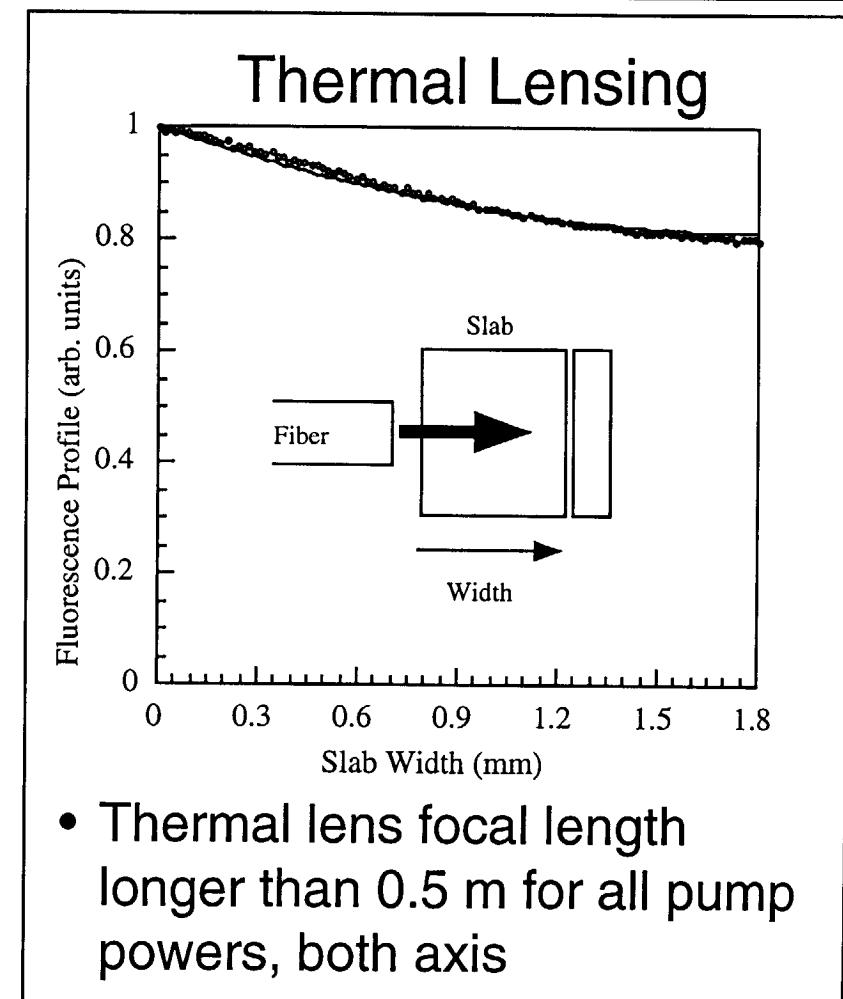
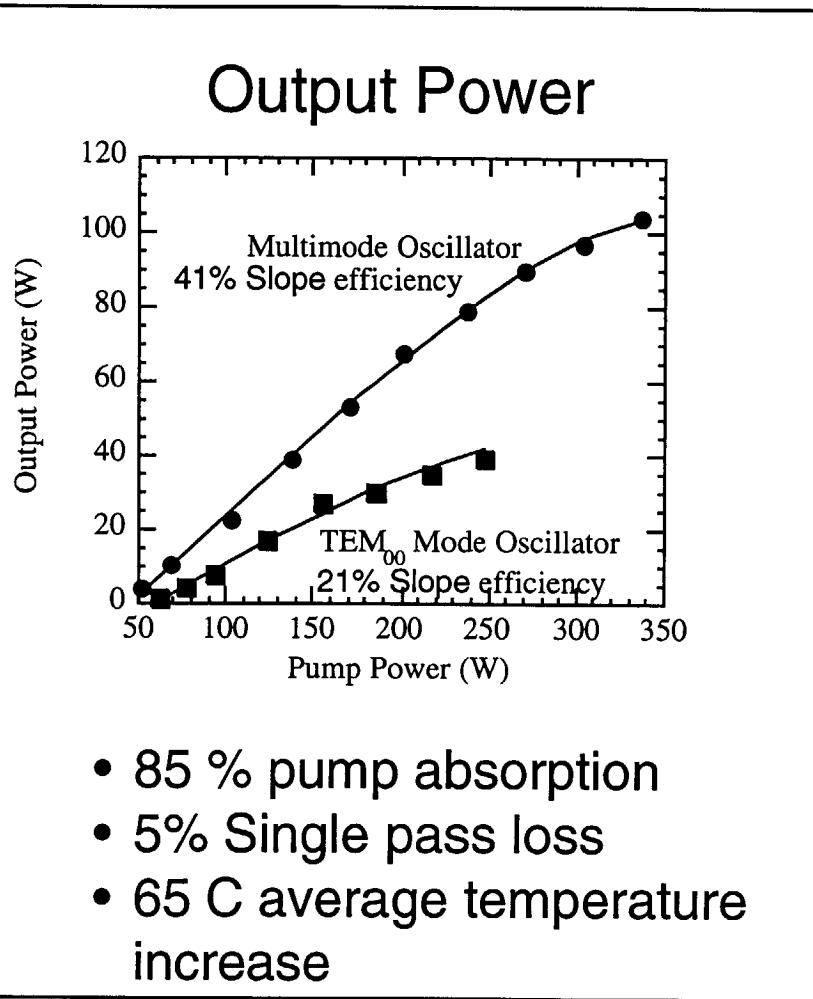
Pump Absorption depends on w

Edge-Pumped, Conduction-Cooled Slab Laser Design



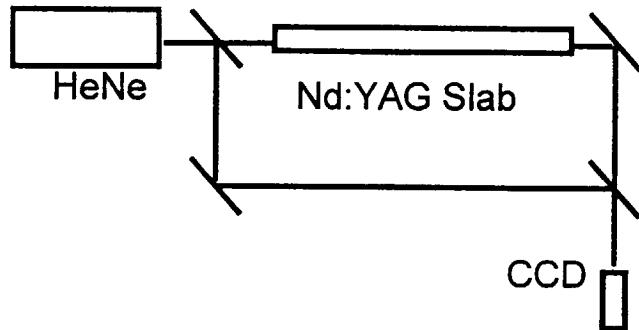
Advantages	Disadvantages
<ul style="list-style-type: none">• Conduction-cooled• Separate pumping and cooling interfaces• Pump absorption and thermal characteristics both proportional to w	<ul style="list-style-type: none">• TIR interface is also conduction cooling interface• Small thermal gradient in pumping direction

1:1 Slab Laser Results



Slab Average Temperature

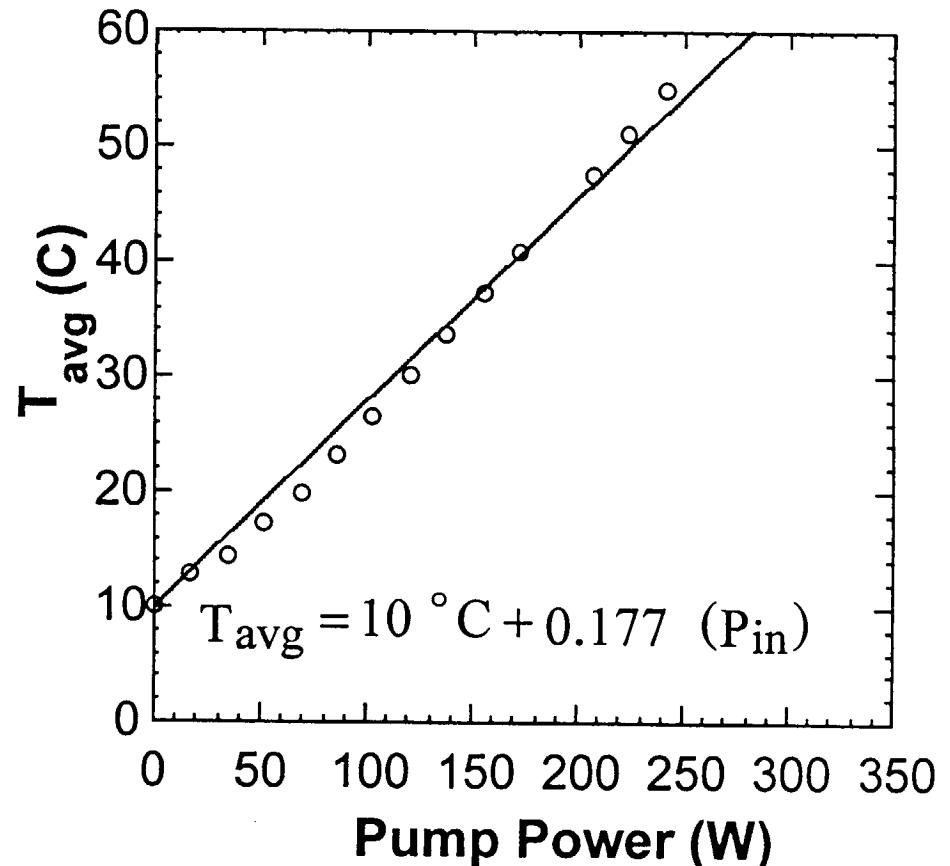
Average Temperature Measurement



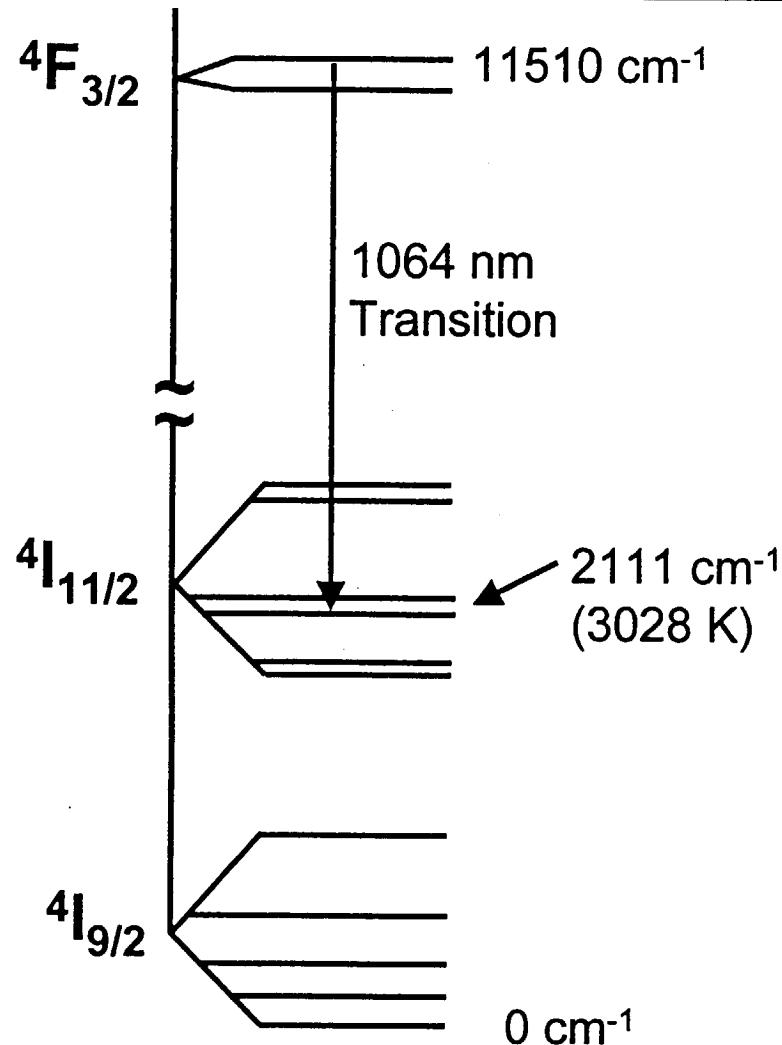
$$T_{\text{avg}} = T_c + \Delta T$$

$$\Delta T = \frac{\lambda \# \text{Fringes}}{\Delta \text{OPL} \left(\alpha(T), \frac{dn(T)}{dT} \right)}$$

$$\Delta T = P_{\text{in}} \eta_{\text{heat}} [\theta_{\text{LaserHead}} + \theta_{\text{Coolant}}]$$



Thermal Population Absorption Loss

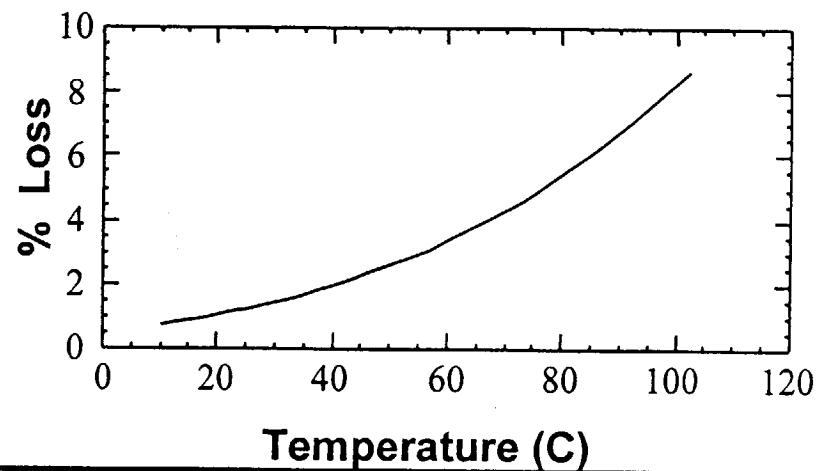


Boltzman Population Distribution

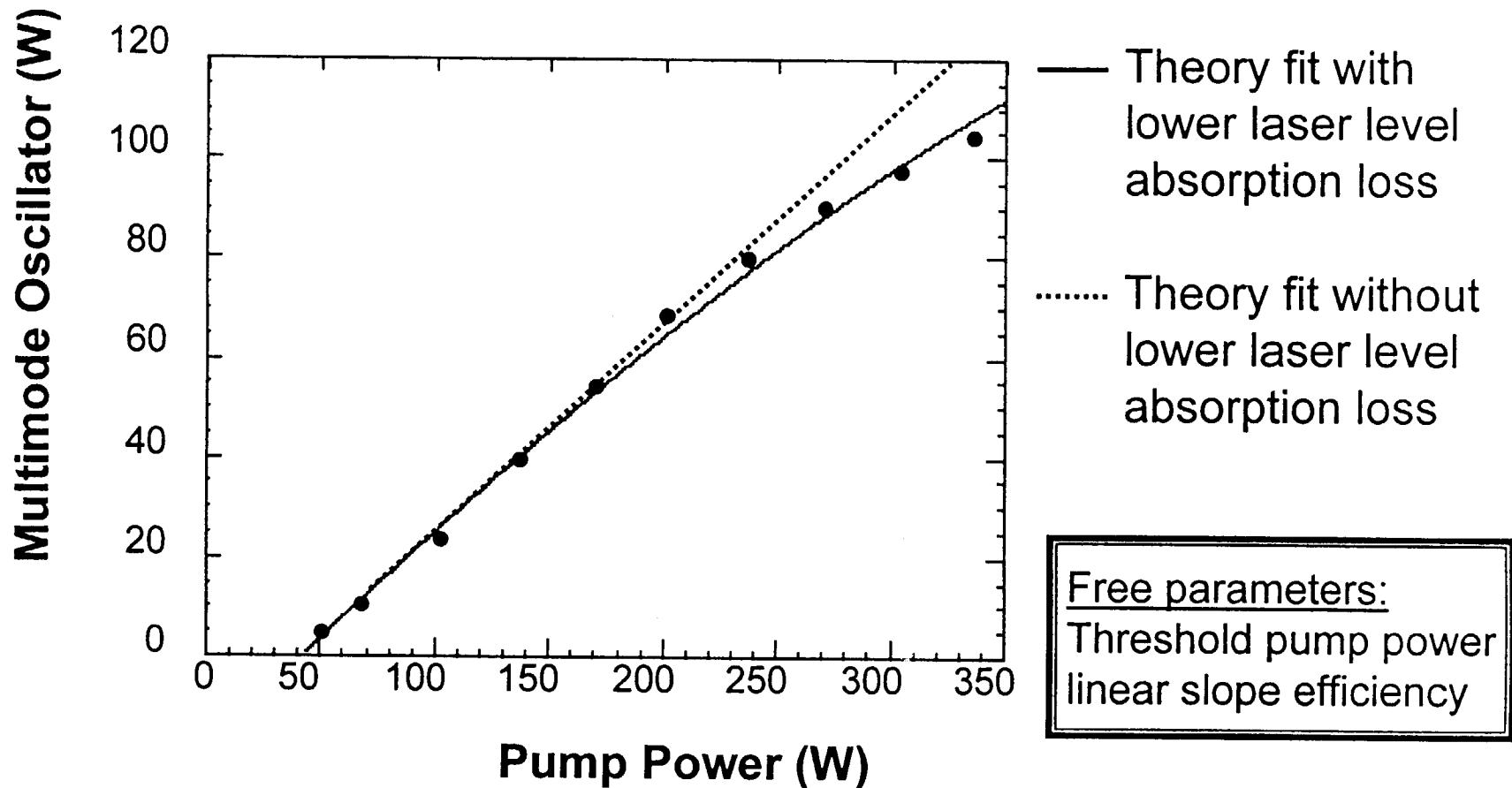
$$f_1 = \frac{N_{2111}}{N_{\text{total}}} = \frac{\exp\left(\frac{-\Delta E_{2111}}{kT}\right)}{\sum_i \exp\left(\frac{-\Delta E_i}{kT}\right)}$$

Single-Pass Percent Loss

$$L_{\text{abs}} = 1 - \exp(-\sigma N_{\text{total}} f_{11})$$



Laser Oscillator Model - Thermal Absorption Loss

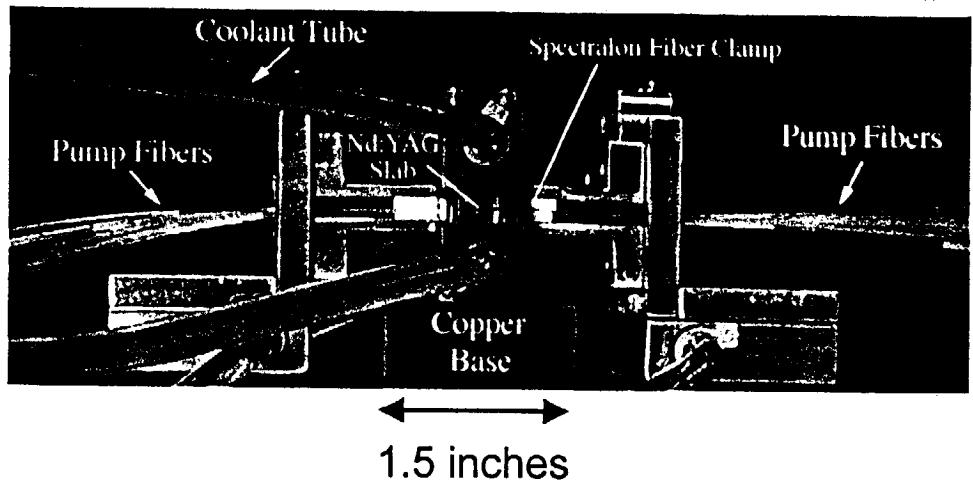
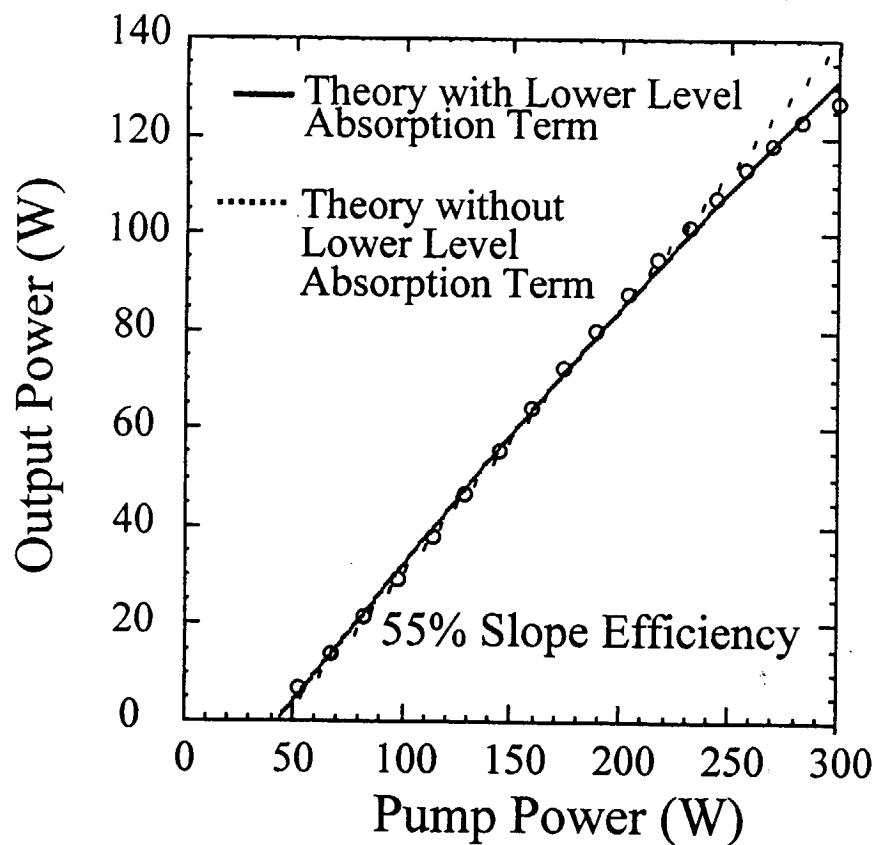


Edge-Pumped Laser Design Improvements

Problem	Primary Effect	Solutions
• High loss at TIR	• Lowers slope efficiency	• “Super-polished” slabs, • Fewer TIRs
• High average temperature (> 60 C)	• Increased slab loss due lower laser level absorption • Master Oscillator Power Amplifier gain mismatch	• Reduce laser head thermal resistance • Increase slab aspect (w/t), • - 40 C coolant, • Improve metal-coolant heat transfer
• One-sided pumping	• Asymmetric thermal profile in non zig-zag plane	• Two-sided pumping

Preliminary Results*

3:1 Nd:YAG Multimode Oscillator Results



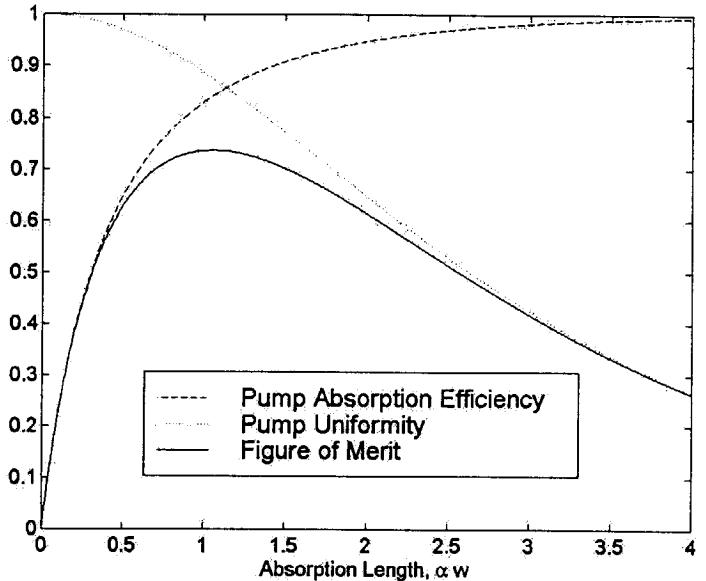
95% Pump Absorption Efficiency

- Nd:YAG Slab
 - 1% Doped Nd:YAG
 - 1.5 x 4.5 x 38.9 mm w/ Brewster end faces
 - SiO₂ Coating for low loss TIR
 - 1.5 % single-pass loss

Preliminary Results*

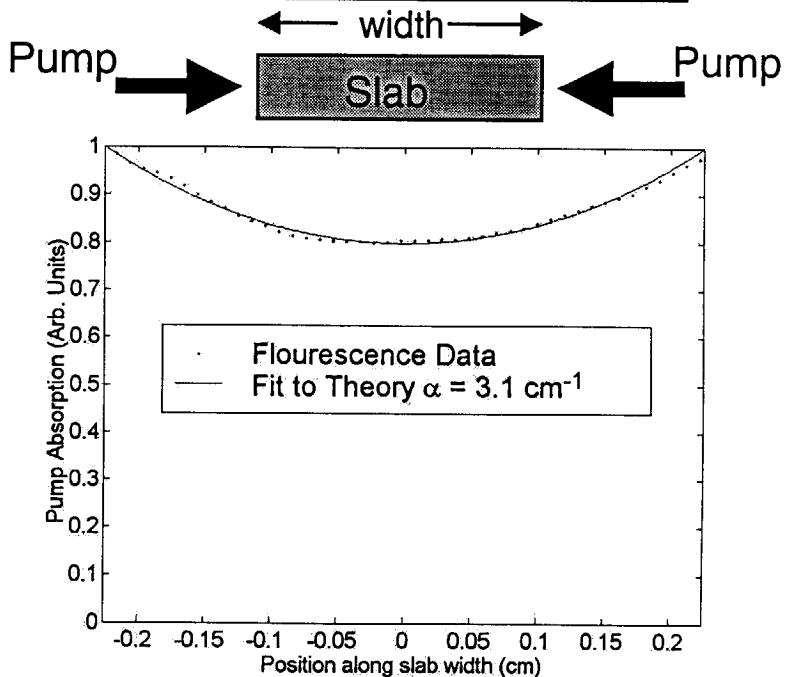
3:1 Nd:YAG Thermal Lensing Results

Pumping Uniformity



- Design Point : $\alpha w = 1.35$
- 4.5 mm Slab Width
- 3.0 cm^{-1} Absorption Coefficient, α ,

Fluorescence Profile

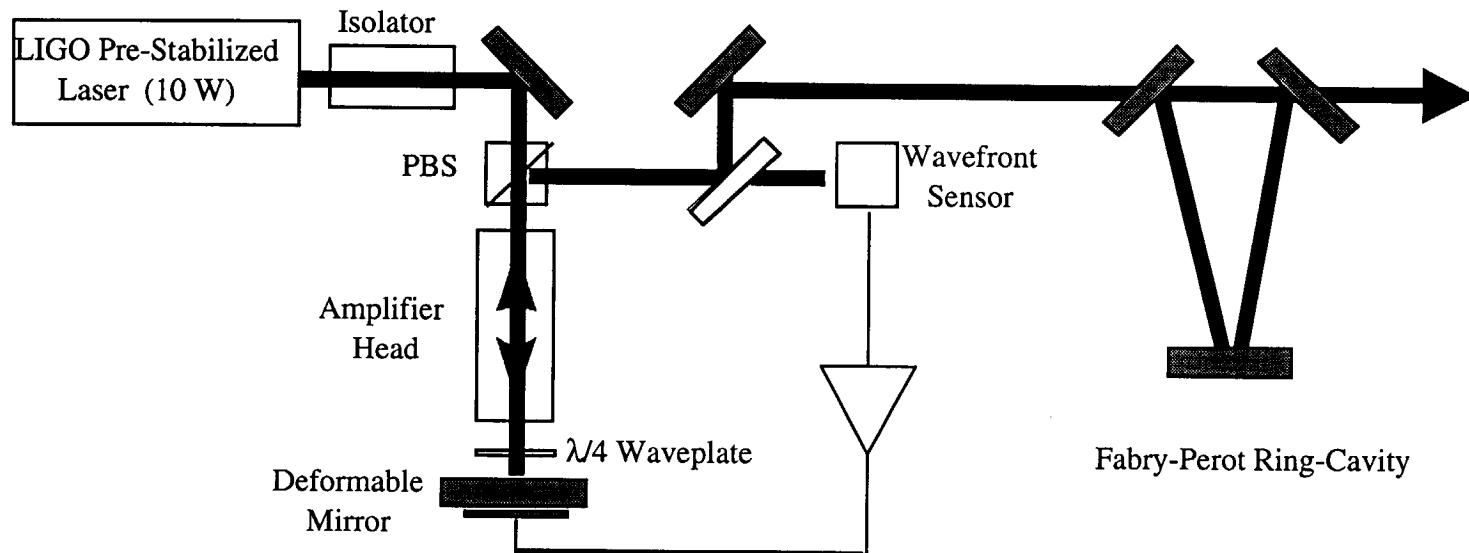


Measured Thermal Lens (full pump)

$$\begin{aligned} f_{\text{width}} &= -42 \text{ cm} \\ f_{\text{thickness}} &= 52 \text{ cm} \end{aligned}$$

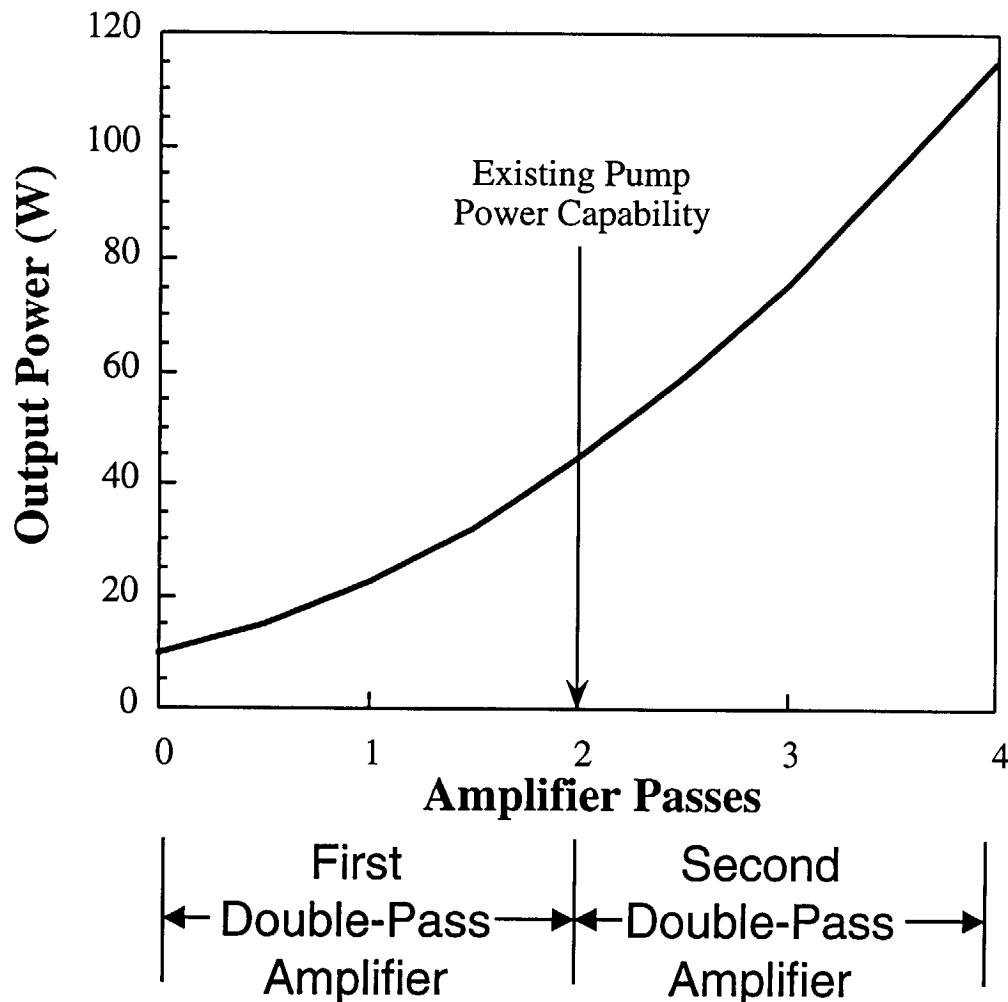
Stanford's LIGO II MOPA Amplifier Module Design

High Power Master-Oscillator Power-Amplifier



- Modular, easy to scale
- Coherence Control
- Spatial Mode Control
- Soft Failure Mode
- **Amplifier Power Noise**
- Extraction Efficiency
- Mode Distortion

Predicted Amplifier Power

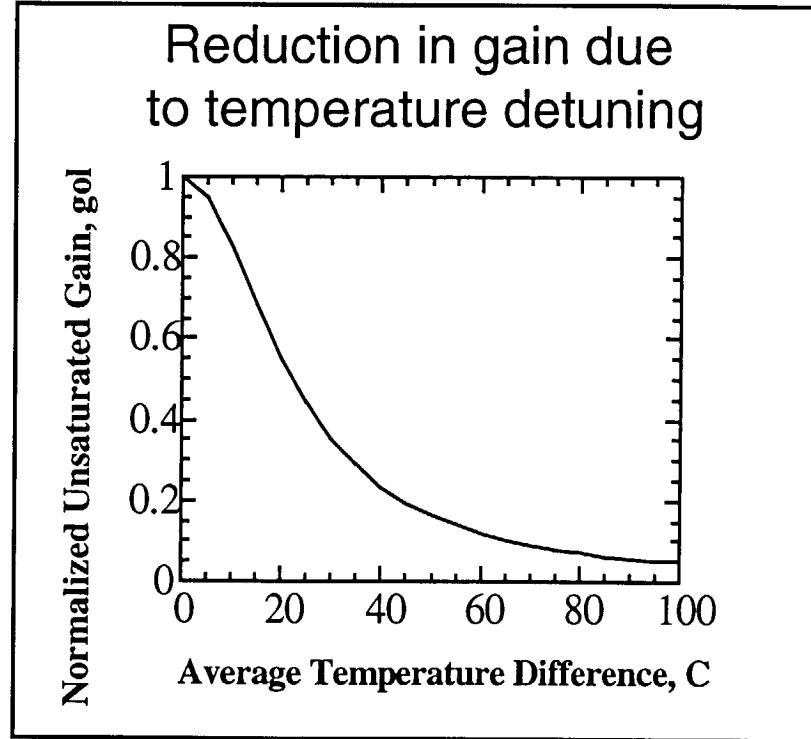
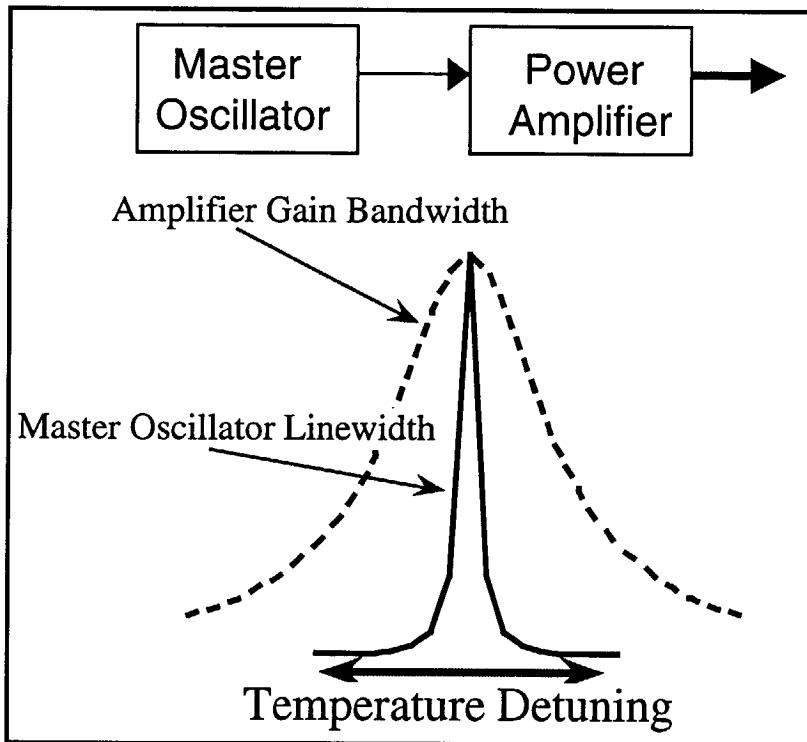


Master Oscillator
- 10 W LIGO Laser

Amplifier
- Edge-Pumped
- Conduction-Cooled
- Double-Pass
- 300 W Fiber-Coupled
Laser Diode Arrays

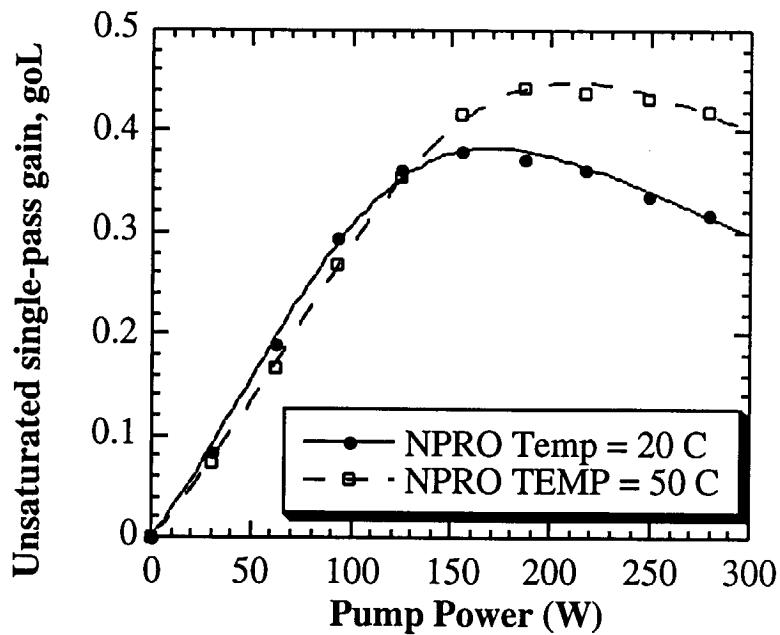
Average Temperature Amplifier Detuning

Wavelength Temperature Tuning 4.5×10^{-3} nm/C
Amplifier Gain Linewidth 0.2 nm



Temperature Detuning in Single-Pass Amplifier

Unsaturated single-pass gain
as a function of master oscillator (NPRO) temperature



Gain rollover due to
master oscillator and
power amplifier
temperature detuning!

Summary and Conclusions

- **Conduction-cooled, edge-pumped slab multimode oscillator**
 - Slope efficiency has increased from 30 % to 55% since 6/98
 - Output power has increased from 40 W to 127 W since 6/98
- **Average Temperature Effects**
 - Thermal population absorption loss
 - Oscillator/amplifier wavelength detuning
- **Ready for 40 W MOPA System Characterization**

High Power Laser Research Proposal

- **Phase 1 - 40 W MOPA System Characterization**
 - Power Scaling (1 month)
 - Amplitude Noise - Saturated Amplifier (1.5 months)
 - Frequency Noise - Free Running (2 weeks)
 - Spatial Beam Control (3 weeks)
 - Beam Wiggle, Spatial Beam Distortion
 - 40 W Mode Cleaner (3 weeks)
 - Second Harmonic Generation - LBO, PPLT, PPLN (2 weeks)
 - Thermal Distortions in System Components (2 weeks)
 - Modulators, isolators, etc.
 - **Phase 2**
 - 100 W MOPA - Diode Budget Dependent
 - Adaptive Optics MOPA Demonstration
-