

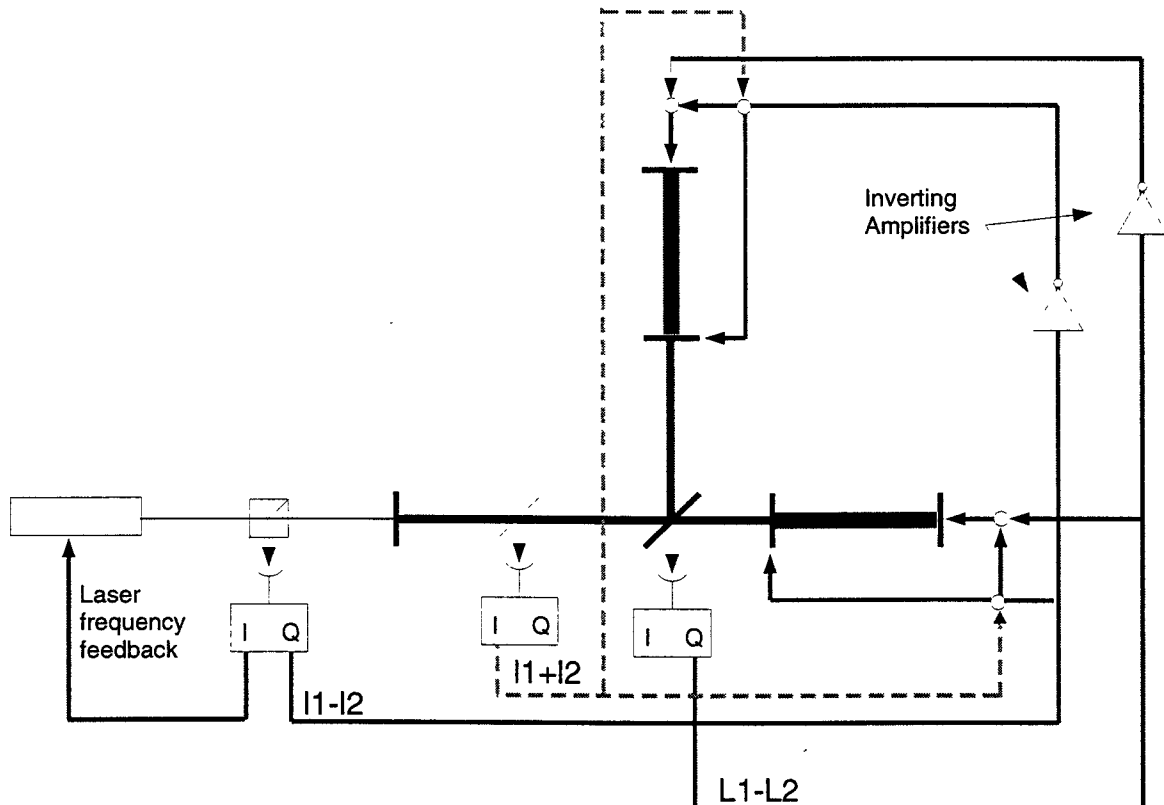
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# Conceptual Design Part 1: Control System Design

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# Baseline Configuration



- Actuate only the test masses (design driven by SUS)
- Sensing as shown in figure

# Alternative Configurations

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- Actuation (baseline is the 4 test masses)
  - ›› End test masses, beamsplitter, and recycling mirror
    - Minimizes number of signal paths
  - ›› In-board test masses, beamsplitter, and recycling mirror
    - High bandwidth signals would not be transmitted over 4 km
- Sensing
  - ›› I1+I2 sensed with non-resonant sidebands
    - Eliminates set of beam reducer optics in beam splitter chamber
  - ›› I1-I2 sensed at recycling cavity pick-off
    - Loop more robust to changes in the losses of the cavity mirrors

# Length Sensing Matrix

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$$\begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \end{bmatrix} \approx \begin{bmatrix} a_1 & \varepsilon_1 & 0 & 0 \\ \varepsilon_2 & a_2 & 0 & 0 \\ 0 & 0 & a_3 & \varepsilon_3 \\ 0 & 0 & \varepsilon_4 & a_4 \end{bmatrix} \begin{bmatrix} L_1 + L_2 \\ l_1 + l_2 \\ L_1 - L_2 \\ l_1 - l_2 \end{bmatrix}$$

- V1, V3, and V4 loops are fairly uncoupled:

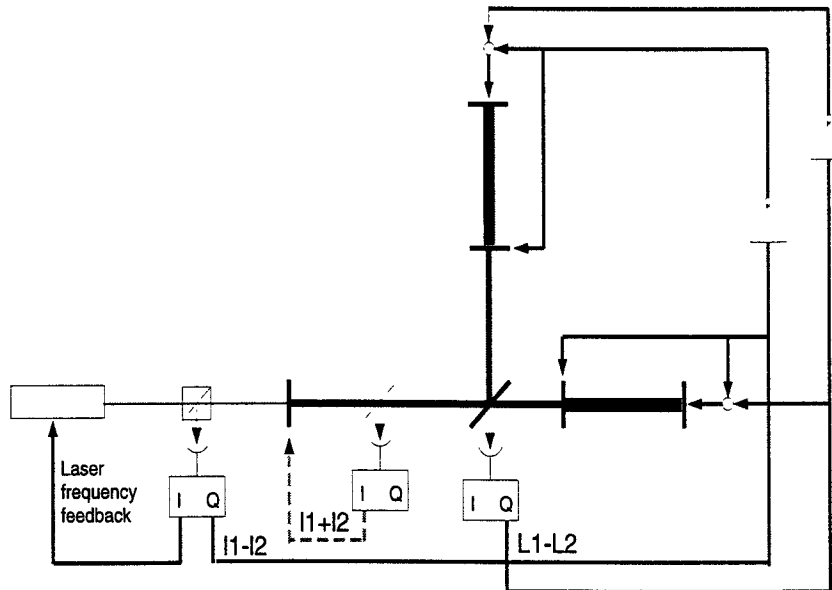
$$\frac{\varepsilon_n}{a_n} \sim 0.01 - 0.001$$

- V2 loop has large  $L_1+L_2$  and small  $l_1+l_2$  piece:

$$\frac{\varepsilon_2}{a_2} \gg 1$$

- Loop gain of  $(L_1+L_2)$  loop must be  $>$  than  $(l_1+l_2)$  loop by at least  $\varepsilon_2/a_2$  to provide adequate decoupling

# Test Case Detection Mode Design

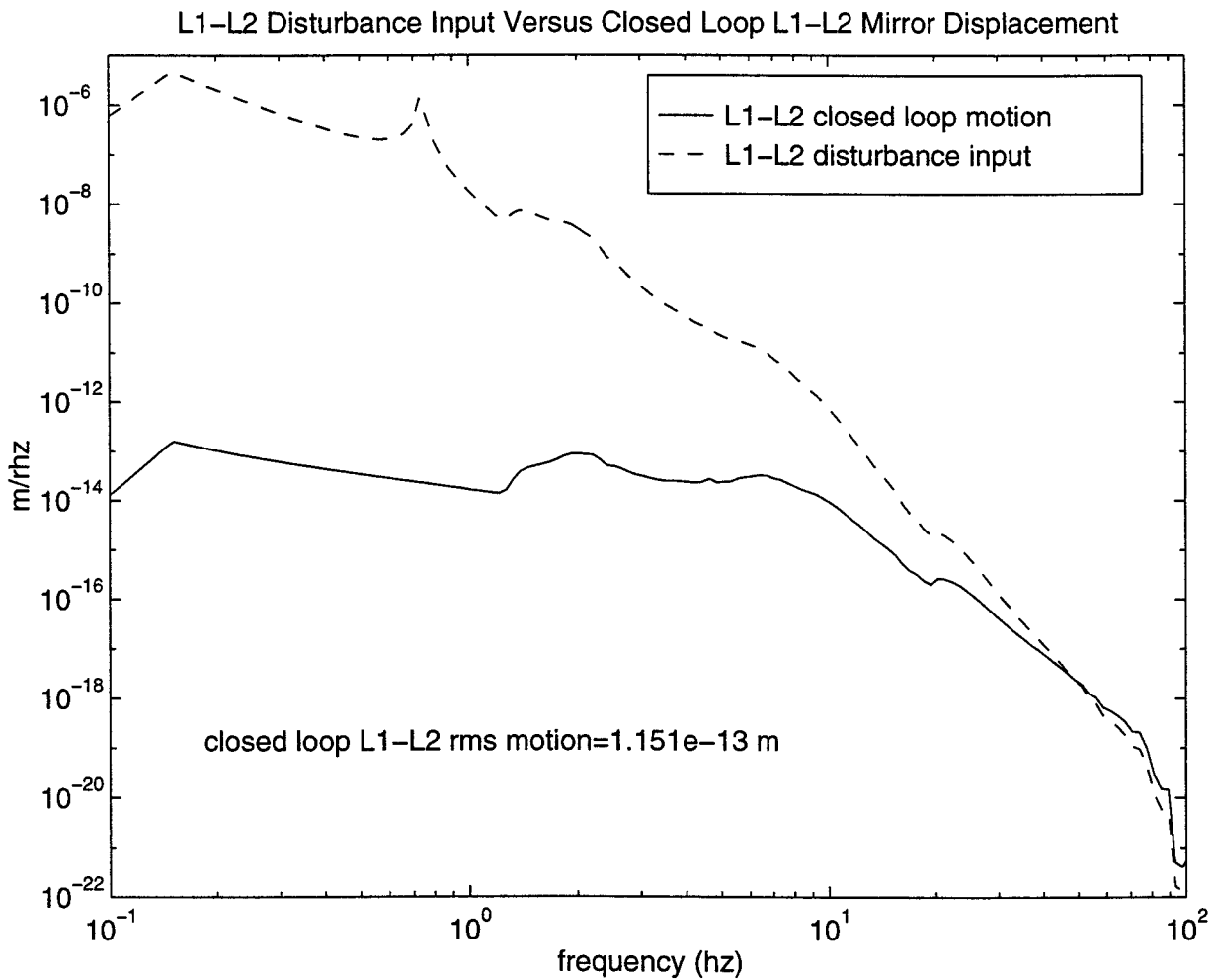


- Low frequency design driver ( $<10$  Hz):
  - ›› Reduction of RMS motion (mainly at microseismic peak)
  - ›› Loop gain ratio requirement of  $(L1+L2)$  and  $(l1+l2)$  loops
- Mid-frequency design driver ( $10 < f < 100$  Hz)
  - ›› Shot noise feedthrough of  $l_1-l_2$  loop into gravity wave band
  - ›› Loop gain ratio requirement of  $(L1+L2)$  and  $(l1+l2)$  loops
- High frequency design driver ( $f > 100$  Hz)
  - ›› loop gain attenuation so test mass resonances don't ring
  - ›› frequency noise suppression

# Loop Gains and RMS Motion

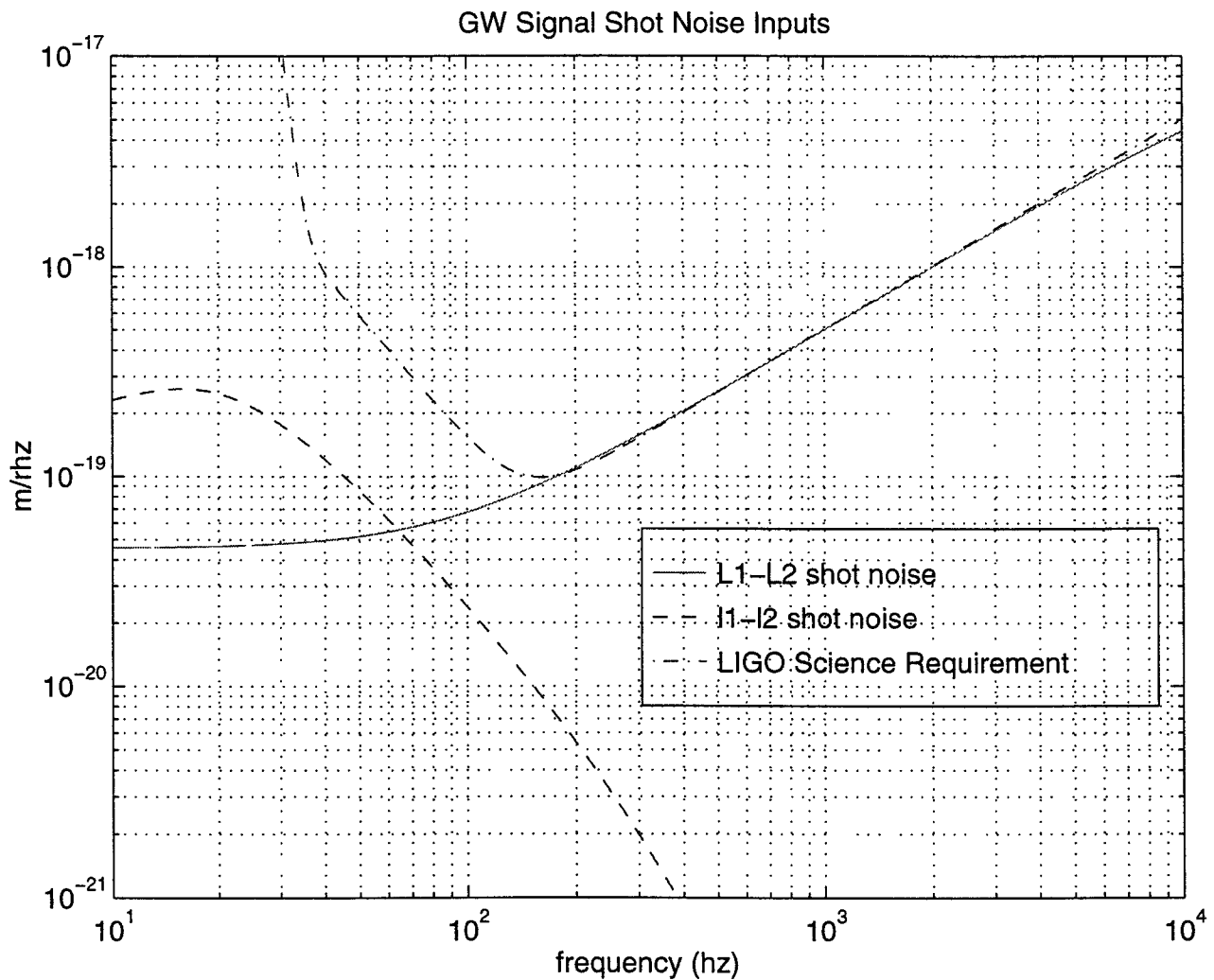
	<i>Laser loop</i>	$l_1+l_2$ loop	$L_1-L_2$ loop	$l_1-l_2$ loop
Loop Gain at 1 Hz	$10^6$	$3 \times 10^3$	$3 \times 10^6$	$2 \times 10^3$
Unity Gain Frequency in Hz	$10^4$	55	140	22
Phase Margin	$45^\circ$	$46^\circ$	$36^\circ$	$40^\circ$
Gain Margin	8	3	4	7
Gain at 8 kHz	$\sim 1$	$2 \times 10^{-8}$	$10^{-5}$	$10^{-8}$
RMS Requirement (mrms)	$2.5 \times 10^{-12}$ (equivalent)	$1.6 \times 10^{-10}$	$10^{-12}$	$1.3 \times 10^{-10}$
RMS Motion (mrms)	$8 \times 10^{-13}$ (equivalent)	$1.2 \times 10^{-11}$	$1.15 \times 10^{-13}$	$1.5 \times 10^{-10}$

# Example Plot of Closed Loop Motion (L1-L2 Loop)



- Disturbance Input: Livingston spectrum filtered through baseline stack and suspension design

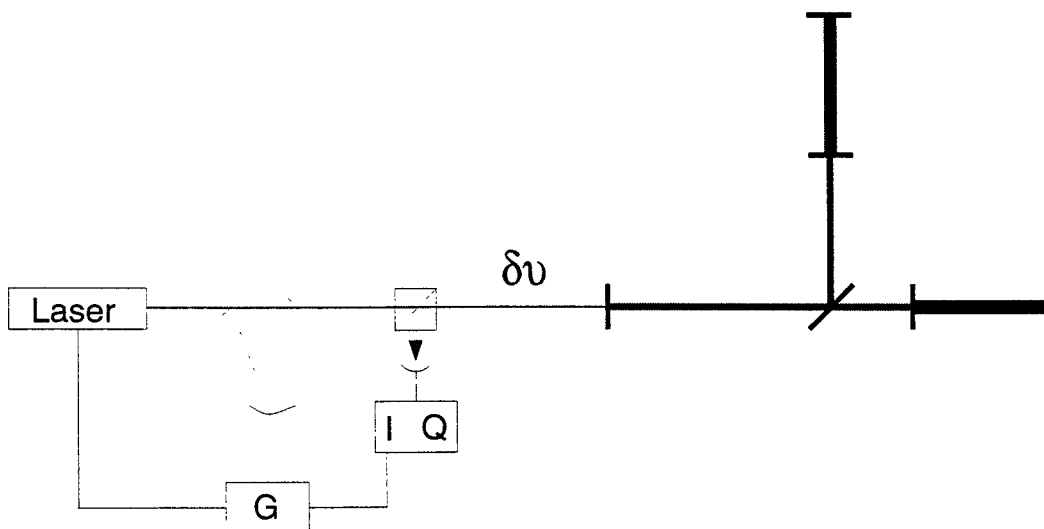
# Shot Noise Performance for Auxiliary Length Control Servos



- Michelson I1-I2 shot noise ~16% of LIGO sensitivity between 40-140 Hz



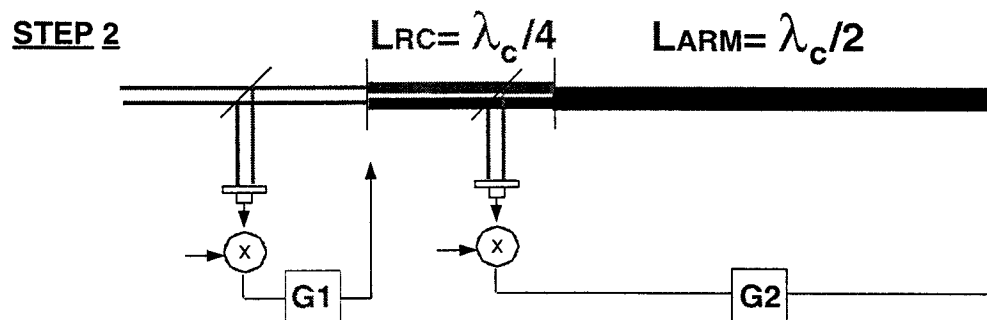
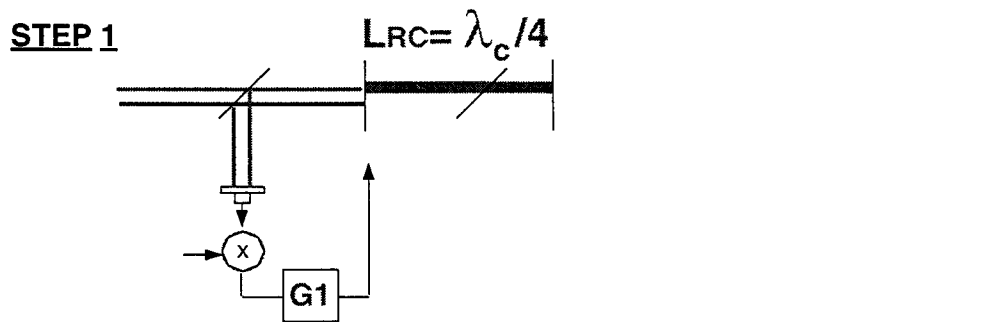
# Frequency Noise Suppression



	<b>f = 100 Hz</b>	<b>f = 10 kHz</b>
<b>δν Requirement</b>	$10^{-7} \text{ Hz/Hz}^{1/2}$	$4 \times 10^{-6} \text{ Hz/Hz}^{1/2}$
<b>δν from IFO Shot Noise</b>	$10^{-7} \text{ Hz/Hz}^{1/2}$	$3.3 \times 10^{-6} \text{ Hz/Hz}^{1/2}$
<b>δν with IFO Feedback "Off"</b>	$10^{-4} \text{ Hz/Hz}^{1/2}$ (MC thermal noise)	$10^{-5} \text{ Hz/Hz}^{1/2}$ (MC thermal noise and shot noise)
<b>δν with IFO Feedback "On"</b>	$5 \times 10^{-9} \text{ Hz/Hz}^{1/2}$ (loop gain= $2 \times 10^4$ )	$10^{-5} \text{ Hz/Hz}^{1/2}$ (loop gain=1)

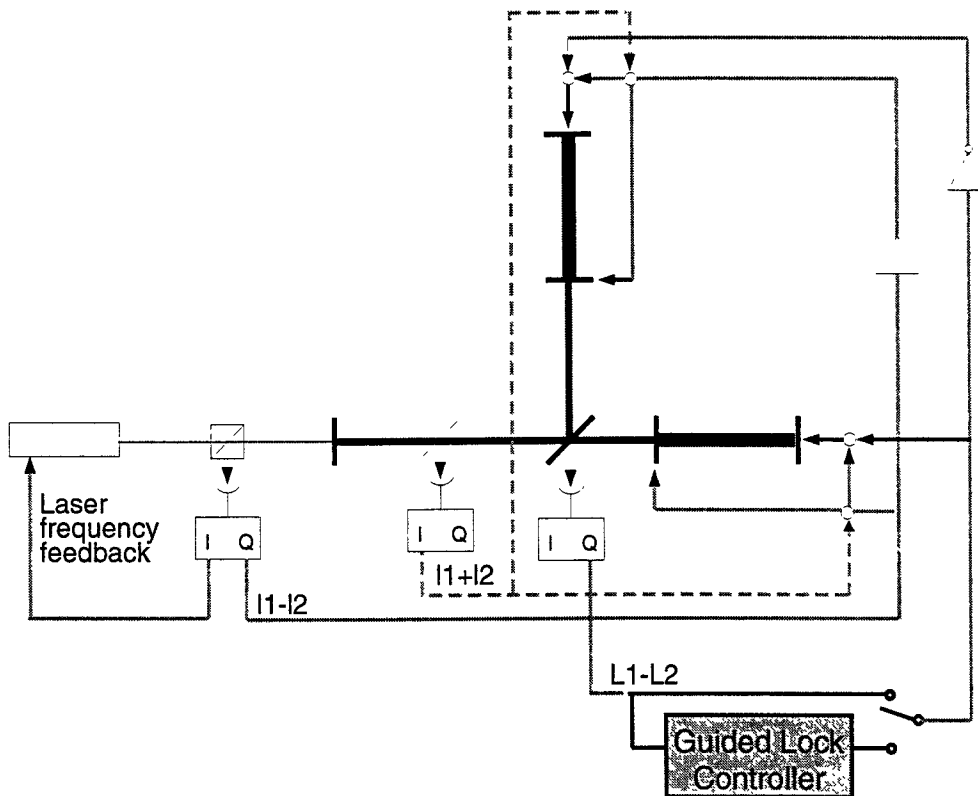
# Concept for Acquisition Mode

- Concept based on coupled cavity acquisition model
  - ›› cavities lock in natural sequence (sidebands first)
  - ›› Threshold velocity is high for recycling cavity (broad fringe)
  - ›› Threshold velocity lower for arm cavity acquisition unless bandwidth is very high (i.e. laser loop)



# Concept for Acquisition Mode (cont.)

- Projected locking behavior for recycling
  - ››  $I_1 - I_2$  and  $I_1 + I_2$  have high threshold velocity (broad fringes)
  - ››  $L_1 + L_2$  has high threshold velocity (high BW servo)
  - ››  $L_1 - L_2$  loop has low threshold velocity (~same as 40m)
- Resulting configuration similar to Detection mode but with “Guided Lock” in  $L_1 - L_2$  loop



# Concept for Acquisition Mode (contd.)

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- Other differences from Detection Mode

- ›› Reduced low frequency gains (important for RMS reduction not acquisition)
- ›› Increased bandwidths (bandwidths important, not gain)
- ›› Unconditionally stable filters (get more gain and phase margin so believe acquisition will be more robust)
- ›› Switching system between Acquisition and Detection modes servos based on 40m switching design

# Issues To Be Resolved

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- Final decision on Detection mode configuration
- Completion of Acquisition Model to verify threshold velocities and conceptual design
- Systems engineering approach to resolve laser frequency noise issues