



Thermal lensing compensation for AIGO High Power Test Facility

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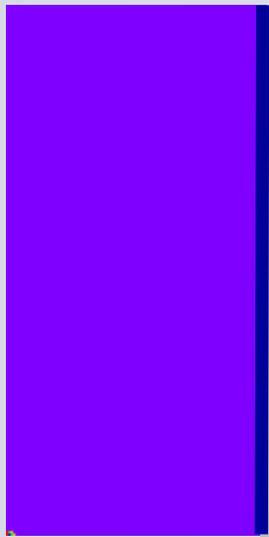


- Thermal lensing
- Influence on the performance of the interferometer
- How to compensate its effects

Thermal lensing (TL)



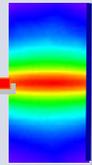
ITM temp. distrib.



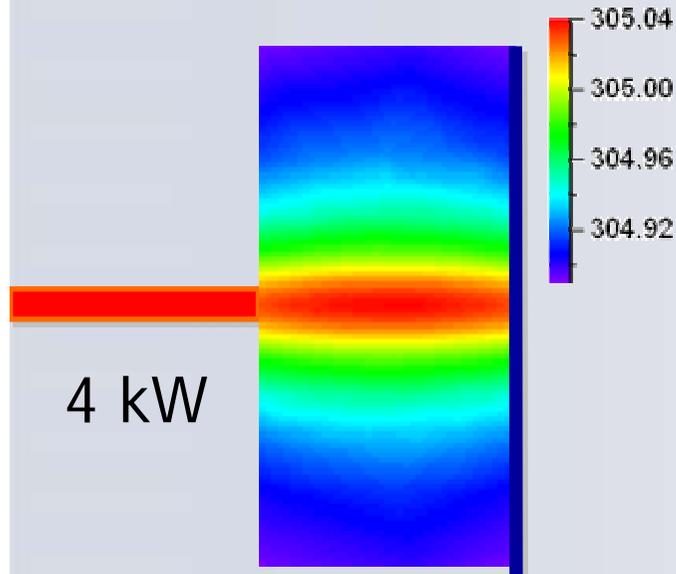
$$T_{ITM} = 300 K$$

Optical absorption
in the material

Thermal lensing (TL)



ITM temp. distrib.



4 kW

*ITM power absorbed
Substrate = 1W*

Optical absorption
in the material

+

High power laser
beam

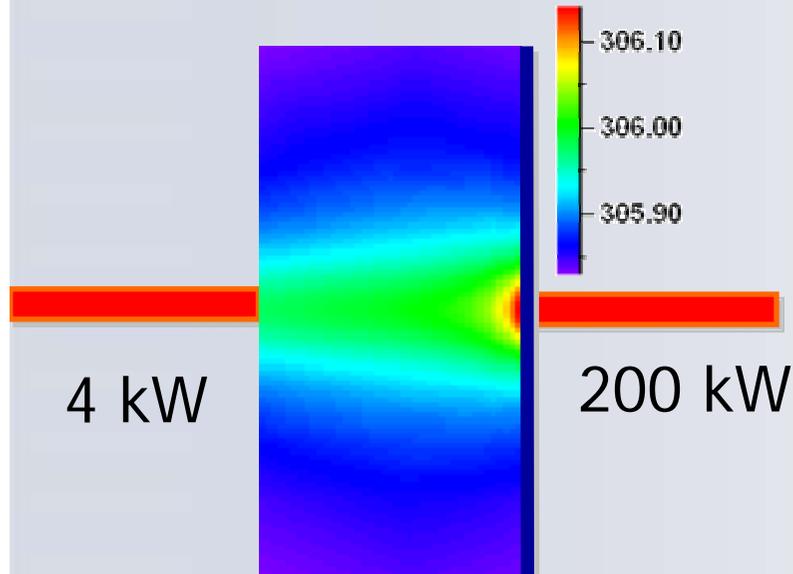


Non-uniform heating
of the optics

Thermal lensing (TL)



ITM temp. distrib.



ITM power absorbed
Substrate = 1W
Coating = 0.2W

Optical absorption
in the material

+

High power laser
beam



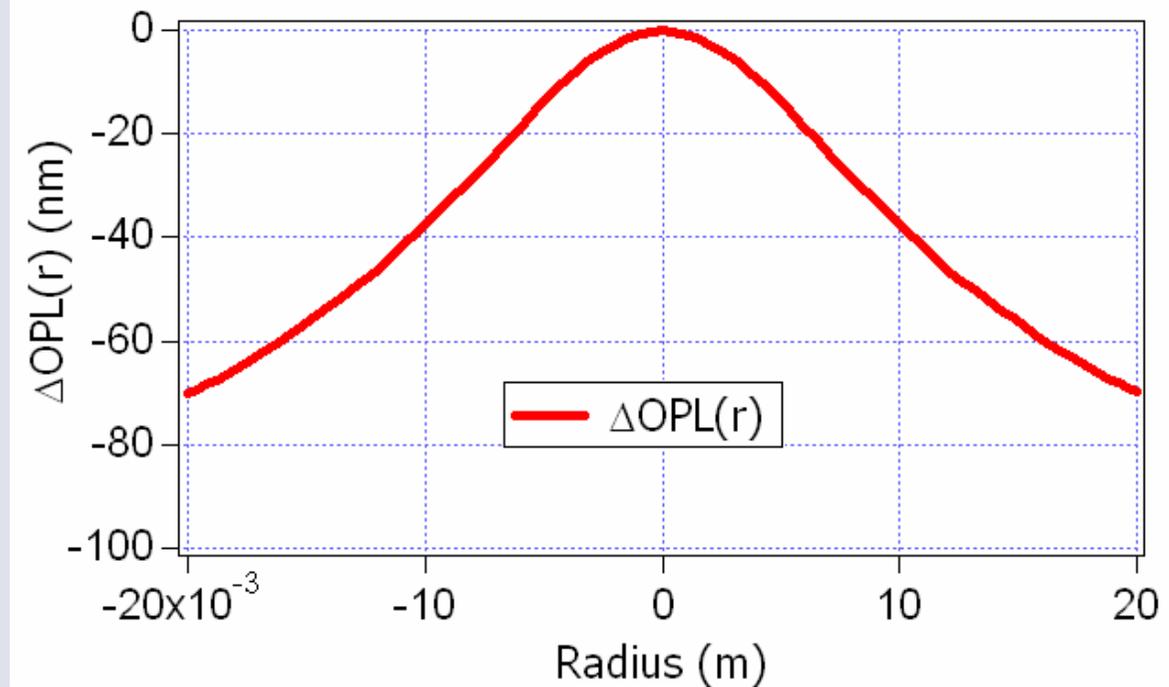
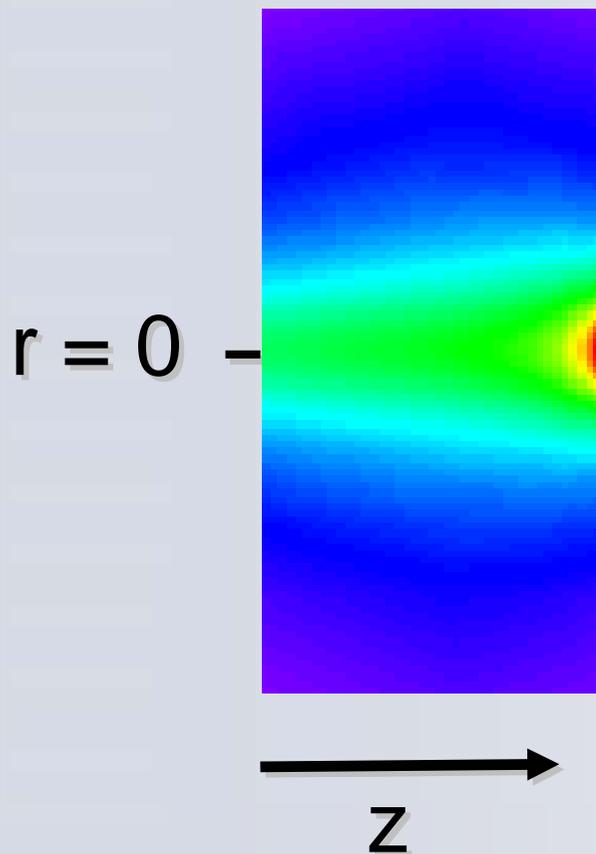
Non-uniform heating
of the optics

TL characteristics



if $T \nearrow$, $n \nearrow$ ($\beta > 0$)

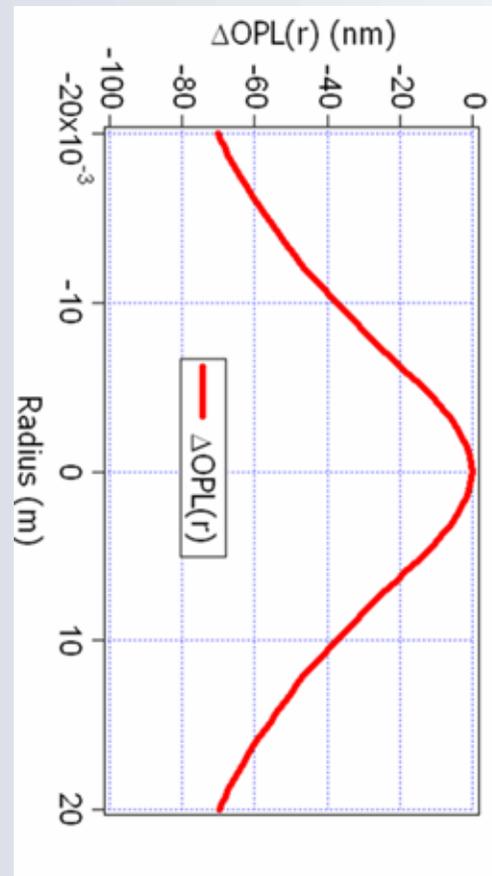
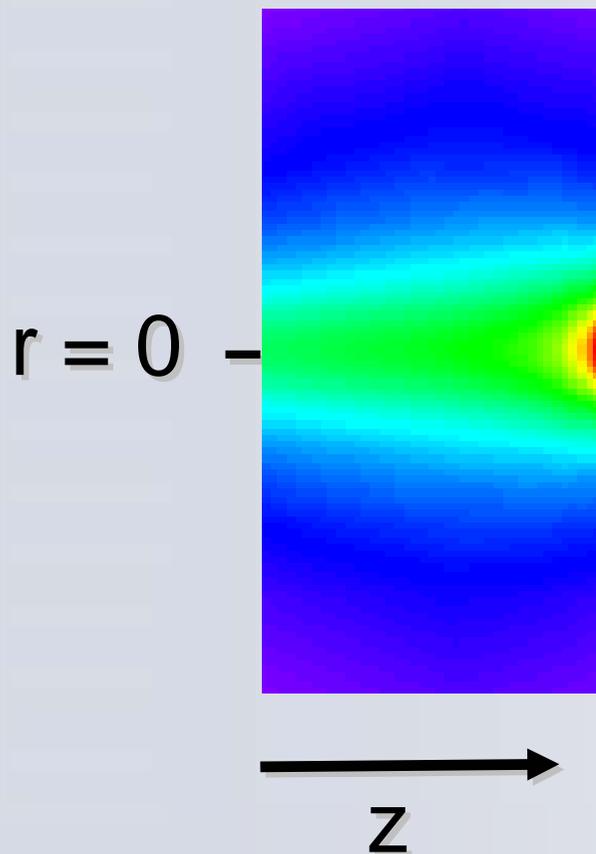
$$\Delta OPL(r) = \beta \int_0^L (T(r, z) - T(0, z)) dz$$



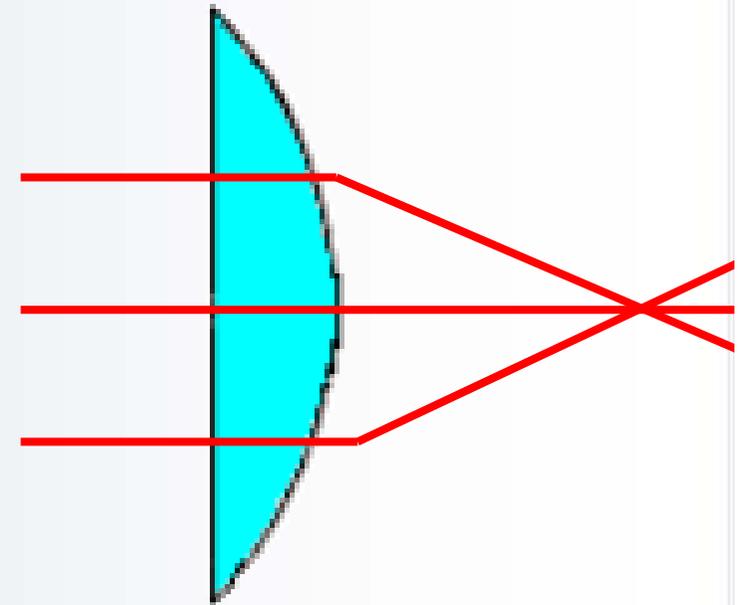


TL characteristics

$$\Delta OPL(r) = \beta \int_0^L (T(r, z) - T(0, z)) dz$$



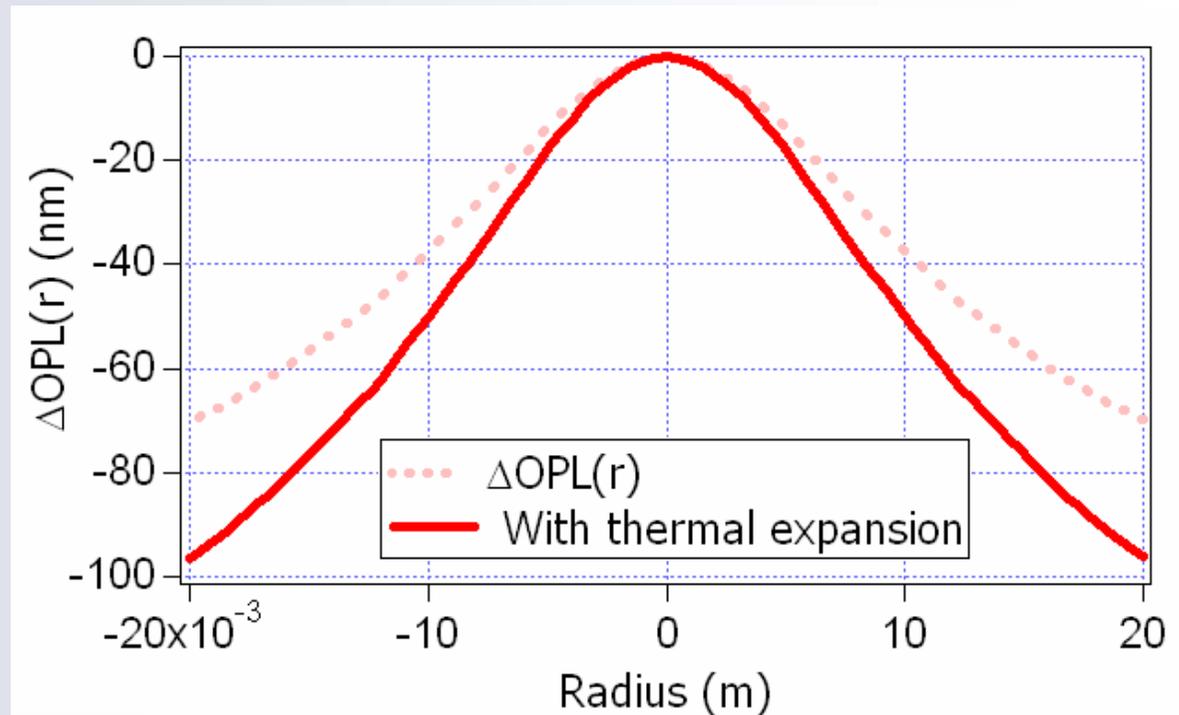
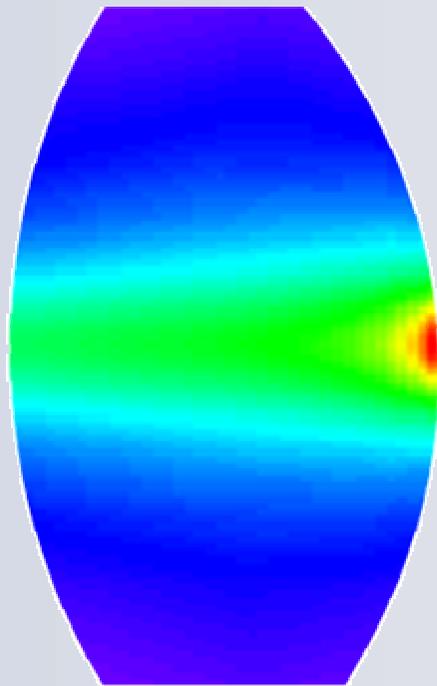
Equivalent to:



TL characteristics



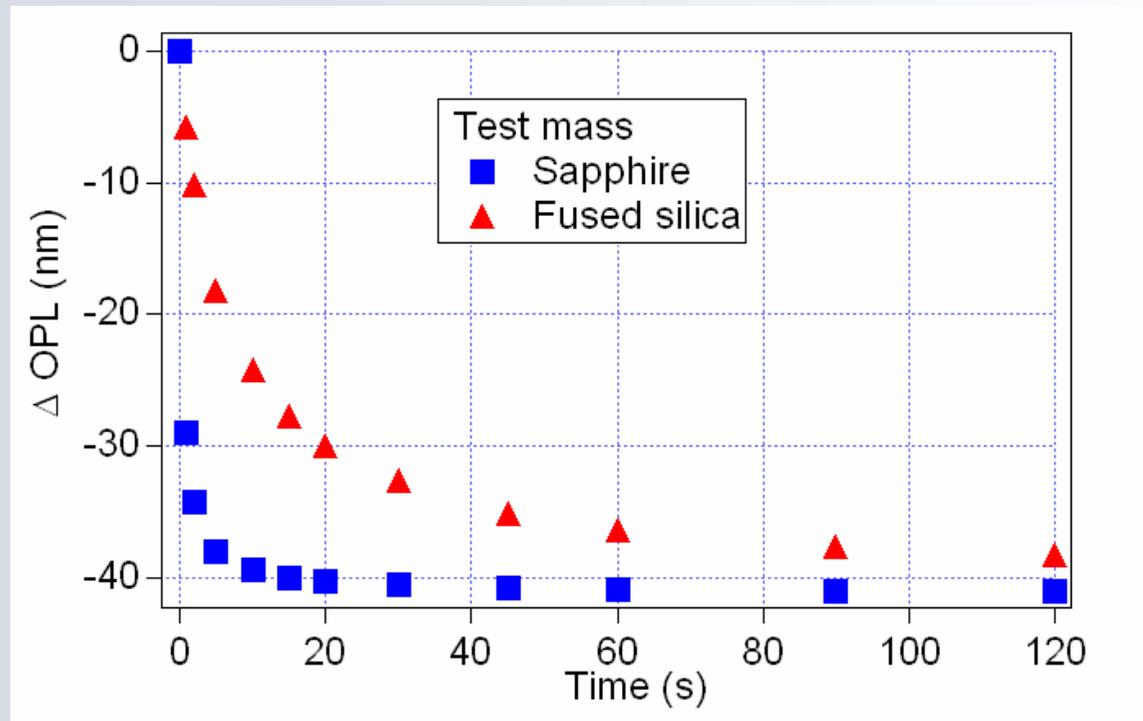
$$\Delta OPL(r) = \beta \int_0^{L+\Delta L(r)} (T(r, z) - T(0, z)) dz$$



TL characteristics



$$\Delta OPL = \beta \int_0^L (T(w, z) - T(0, z)) dz$$



- Same TL magnitude for fused silica and sapphire

- Short TL time constant (< 1 minute)

Test mass TL effects

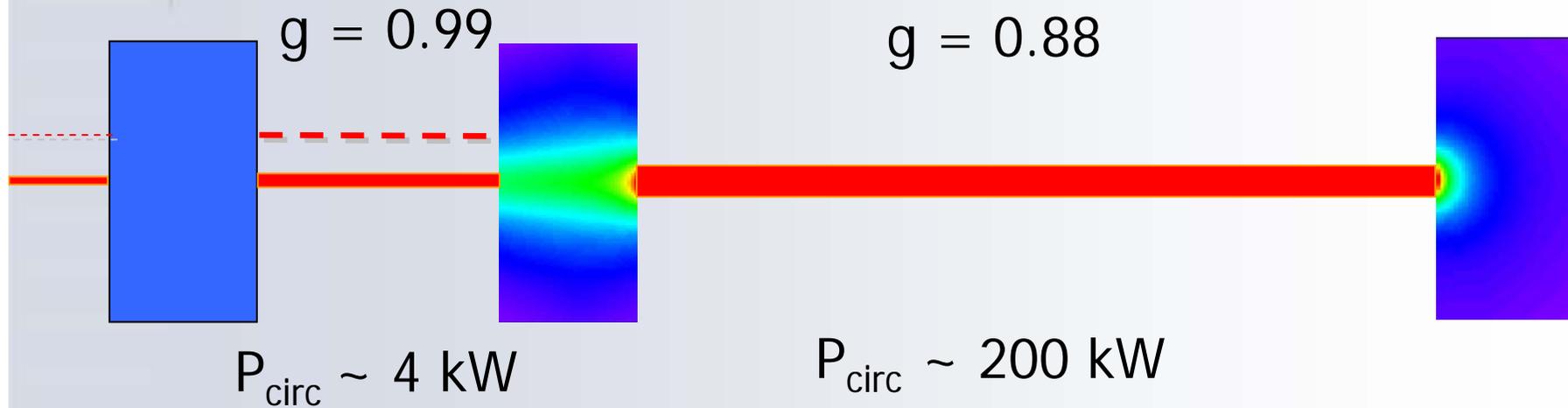


- Test mass acts like a convergent lens (focal length \sim km)
- Non spherical lens \Rightarrow higher mode conversion (< 0.5 %)
- Change the mirror radius of curvature (change in sagitta \sim nm)

Cavity TL effects

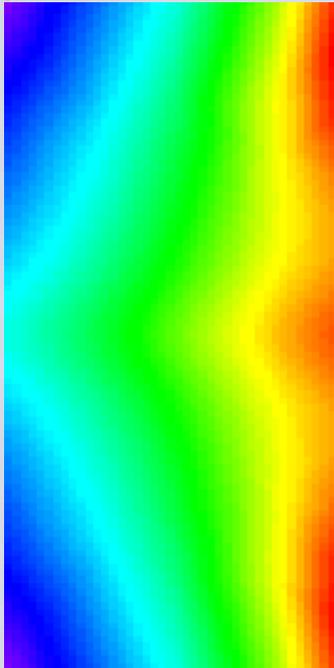


Gingin Test 3



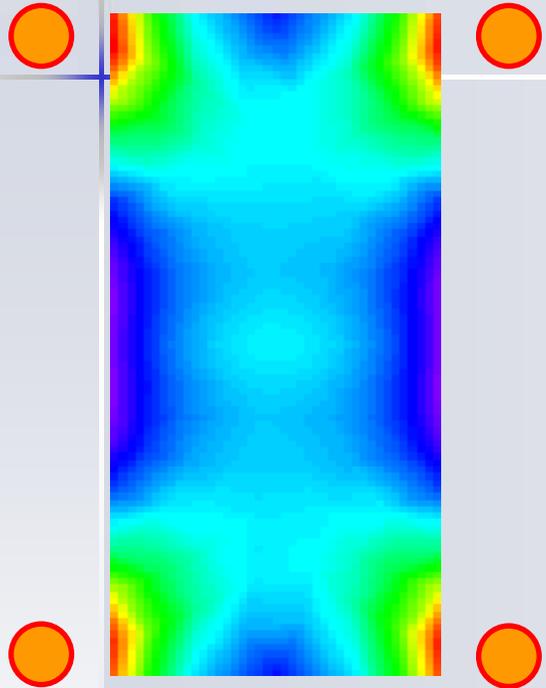
- Change the cavity modes
- Decrease in the circulating power
 - 3% for the carrier in the arm
 - 17% for the sidebands

Heating ring



- ■ Due to the sapphire high thermal conductivity, the compensation is more difficult than for silica
- More difficult for small beam radius
-

Heating ring



- Due to the sapphire high thermal conductivity, the compensation is more difficult than for silica
- More difficult for small beam radius

ITM temp. distrib.

$$T_{ITM} = 400 \text{ K}$$

$$P_{ring} = 60 \text{ W}$$

- Use of 2 heating rings ?

Not practical for Gingin on sapphire TM!

Compensation plate



Compensate the TL on an external silica plate

Heating ring



FS Plate

- Diameter same as the TM
- Thickness optimized (~ 10 mm)

Advantage:

TM remains intact

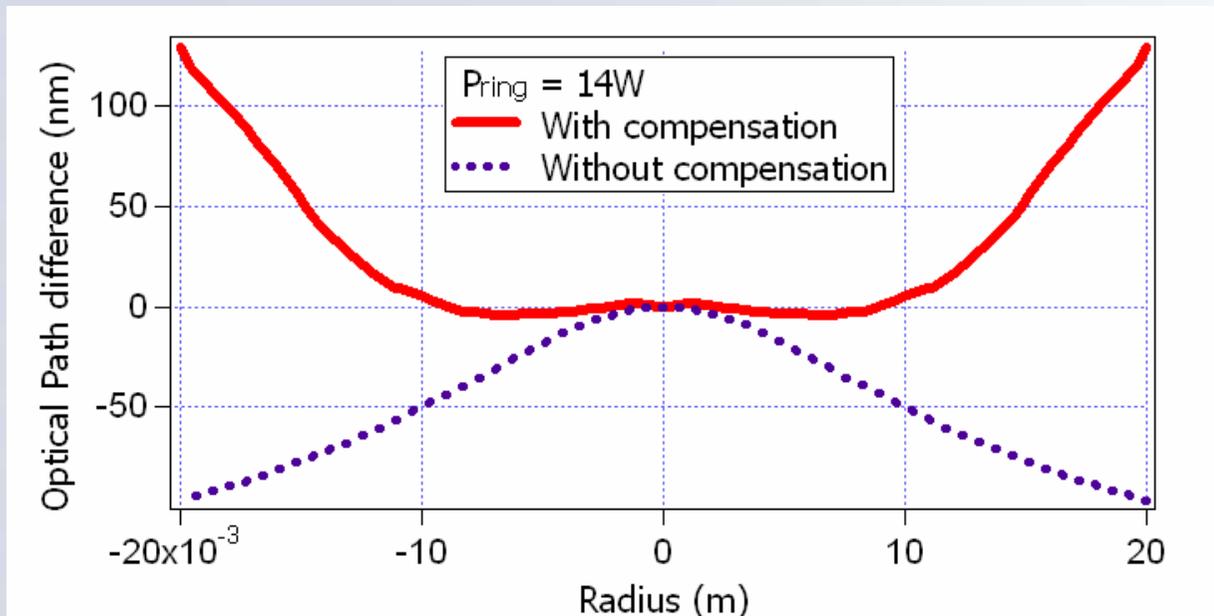
Drawback:

Object inside the cavity

For Gingin...



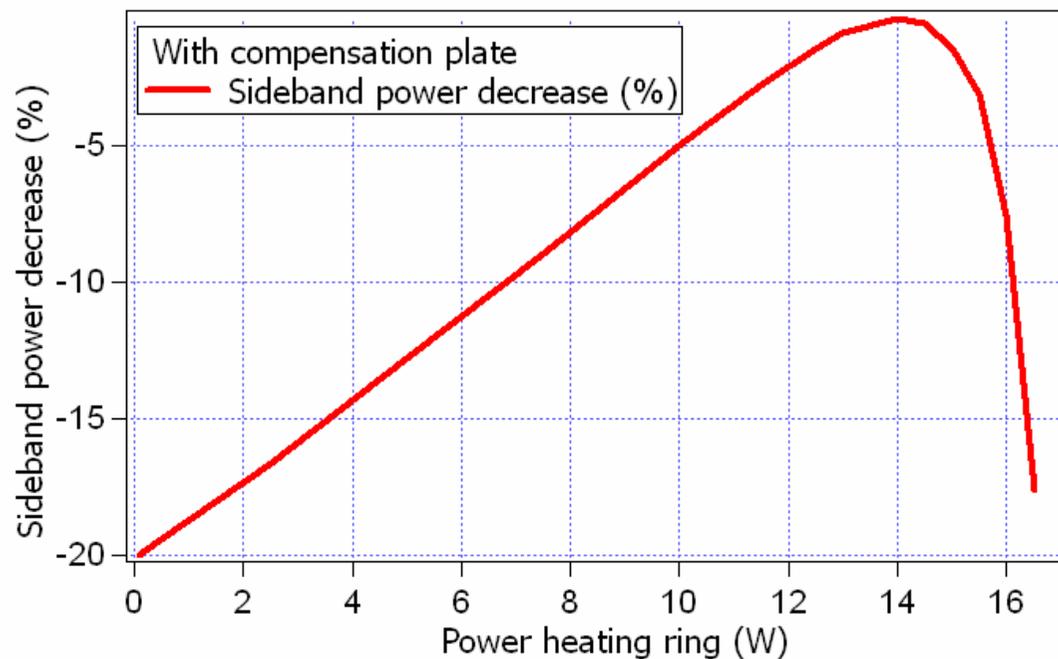
Gingin Test 3



$$P_{\text{ring}} = 14 \text{ W}$$

$$T_{\text{plate}} = 340 \text{ K}$$

For Gingin...

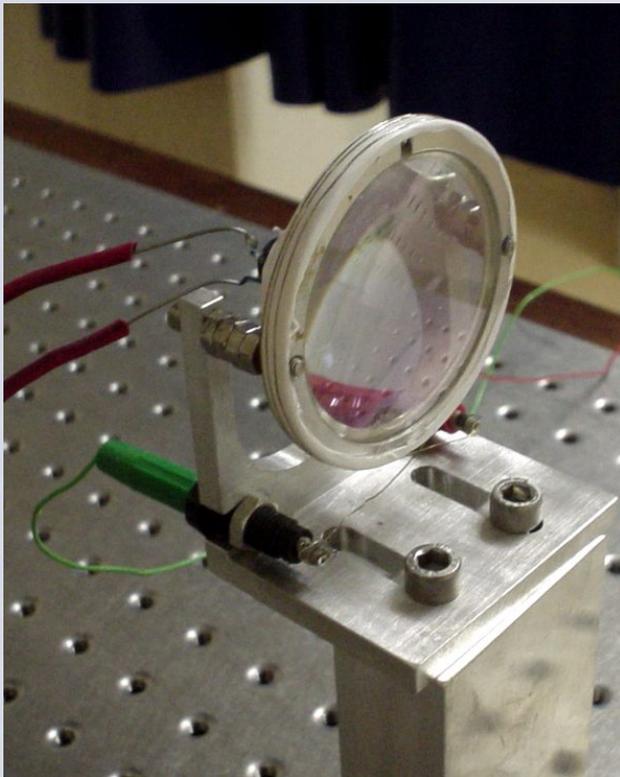


- No change in arm circulating power
- Restoration of the sideband gain

Experiments



Experiments required to validate the simulations



- 50 mm diameter plate
- Heating by conduction
- Using a Mach-Zehnder interferometer

First result:
thermo-optic coefficient

Further work



The main issues remain:
Quantification of the noise added by the plate

- Suspension requirement ?
- Influence of the AR coating ?
- Control accuracy ?

- Strong thermal lensing in AIGO
- Compensation plate essential
- Need more research

Regarding the thermal lensing:

Be alert not alarmed !

Special thanks to ACIGA and LIGO people