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The review of production drawings for the ALIGO ETM
Penultimate Mass: support notes

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Rev 00	22 nd February 2008	First draft, response required to action list in conclusions (R. Jones)
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1 Introduction

This document introduces the key features of the ALIGO ETM Penultimate Mass for review purposes.

Production drawings are based on drawings used for the ALIGO noise prototype^{1, 2} (NP-type). The drawing of the finished mass is to be used as the main source of manufacturing information, supported by the material selection and inspection information described in the associated specification.

The proposed changes to the form of the final ETM penultimate mass (as compared to the form of the NP-type penultimate mass) are as follows:

- **Change to the tolerance on wire groove position (use of symmetry tolerance, regardless of feature size, or RFS)**
- **Extension of wire grooves around full barrel of mass**
- **Extension of lambda/10 bond area on flat, and its associated specification.**

The following issues require clarification:

- Confirm approach to specifying flat length (versus width of mass, flat to flat)
- Size and positional tolerance required for shielded magnet recesses
- Quantity, size and position of reference
- Confirmation of wire sizes
- The ITM penultimate mass drawing, which is to be identical to the ETM penultimate mass, will be drafted once details of the ETM specification are confirmed.

***A list of actions has been tabulated in the conclusion. (These actions are also distributed throughout the text).**

2 Review documents (*numbers to be assigned)

D080117	ALIGO SUS ETM QUAD Penultimate Mass
E080090	ALIGO SUS ETM QUAD Penultimate Mass component specification

3 Format of production specification

¹ D050421-A ALIGO ETM NP-type Penultimate Mass

² E060235-00_DCN_NP-type Penultimate and Reaction Masses

Drawing³ to be used as main source of manufacturing information

No billet drawing provided

Specification⁴ supports drawing, with material selection information and inspection requirements

Key production requirements:

Precise knowledge of centre of mass position (for the bonding, and suspension in turn)

Wire grooves accurately positioned with respect to COM

Polish area must be appropriate for ear bonding (NOTE: existing NP-type ear footprint “D060555-02” can be represented within a 13mm x 22mm MIN.)

Shielded magnet recesses: position/size and shape to suit mating design.

4 List of main drawing features

- Diameter
- Thickness
- Chamfer size
- Flat length
- (Penultimate) Wire grooves
- Associated (penultimate) wire diameter
- Shielded magnet recesses
- Reference lines/markings
- Polishing

5 Discussion and clarification of features

5.1 Diameter: $\varnothing 340.0\text{mm} \pm 0.25\text{mm}$ (With cylindricity tolerance of 0.1mm)

Justification: Maintained in accordance with NP-type penultimate mass drawings (dimension and tolerance employed for both penultimate mass and test mass), where this specification was easily met in both cases.

ACTION 1-P (DONE): Confirmed by successful NP-type deliverable (Glasgow)

5.2 Thickness: $200.0\text{mm} \pm 0.5\text{mm}$

Justification: Maintained in accordance with NP-type penultimate mass drawings.

In a meeting between IGR representatives, material suppliers and the polishing company prior to the manufacture of NP-type masses concern was raised over this aspect of the drawing, with the

³ D080117 ALIGO SUS ETM QUAD Penultimate Mass

⁴ E080090-ALIGO SUS ETM QUAD Penultimate Mass component specification

polishers keen to minimize the amount of machining required. As a result, a large tolerance was placed on the feature in order to reduce the likelihood of this feature becoming a cost driver.

Following inspection of the NP-type masses, thickness was within specification in all cases, but always at the high end of the tolerance (E.g. mean thickness of D050421-002 = 200.42mm)

ACTION 2-P: Confirm thickness and tolerance (Drawing check, plus discussion with SUS colleagues)

Note: the thickness tolerance placed on the NP-type thermal compensator plate drawing (fused silica) was +/-0.1mm, so a reduction the tolerance may be an option.

5.3 Chamfer size: 2.0mm +/-0.2mm, x 45 degree +/- 5 degrees ALL ROUND

Justification: Maintained in accordance with NP-type penultimate mass drawings. This was not an inspected dimension.

ACTION 3-P (DONE): Confirmed by successful NP-type deliverable (Glasgow)

5.4 Flat Length: 2x, 95.0mm (SHARP TO SHARP)

Justification: Maintained in accordance with NP-type penultimate mass drawings *at this stage* (dimension and tolerance employed for both penultimate mass and test mass).

***Discussion point*:** What matters more, the width of the mass or the length of the flat?

A change in approach to specifying flat length may be worth considering. (Question for Garilynn: How is this being specified for the ETM optic?)

The accuracy of the current specification is reliant on the combined effect of:

- Accuracy of manufacture of the finished diameter (ø340.0mm +/-0.25mm)
- Accuracy of the flat length (95.0+/-0.1mm)

Table 1 describes the effect of the tolerance limits on the (flat to flat) width of the mass. (Numbers were produced using 2-D sketches in SolidWorks.)

Diameter ø (mm)	Flat length (mm) 94.9 (low end of tolerance)	Flat length (mm) 95.1 (high end of tolerance)
ø339.75 (low end of tolerance)	Mass width = 326.23mm	Mass width = <u>326.17</u> mm (LOWER LIMIT)
ø340.25 (high end of tolerance)	Mass width = <u>326.75</u> mm (UPPER LIMIT)	Mass width = 326.69mm

Table 1: SolidWorks assessment of mass width (within specification).

The width of the mass can change by up to a total of 0.58mm and still be within the existing specification.

Background: For both NP-type penultimate masses, the flat lengths were out of specification (undersized by 0.5mm in three of the four cases), but the measured diameters were very close to

ø340 (all within 0.1mm). The resulting (nominal) measured width⁵ of the each mass was still within the limits set by the cases above ($326.17\text{mm} < \text{Width (flat to flat)} < 326.75$).

Specifying the width of the mass⁶ (flat to flat when looking from surface ‘S3’) is an alternative worth considering. For a given range of finished diameters this would leave a clearly defined range of acceptable flat lengths. (I.e. the flat length will be appropriate if the width of the mass is within a chosen specification.)

ACTION 4-P: Discuss/confirm approach to this specification with SUS colleagues (Glasgow/SUS)

5.5 Wire Grooves: 6.0mm+/-0.1mm (symmetrical within 0.1 relative to datum C, regardless of feature size, RFS)

Justification: The NP-type drawing specified the wire grooves such that in the worst case, the COM could be 0.5mm from the suspension point which is undesirable⁷. Of the two masses provided for the NP-type, the grooves on the first mass exhibited position that were close to worst case, whereas the groove positions on the second mass (which will be used in the NP-type) were much improved.

The use of the symmetry positional tolerance should minimize the error in position regardless of the eventual thickness of the mass (RFS).

ACTION 5-P: To be confirmed following drawing check (Glasgow/RAL)

5.6 Wire diameters: ø 0.62mm (+/-0.1mm)

Justification: Maintained in accordance with NP-type penultimate mass drawings.

ACTION 6-P: Confirm that this is the correct wire diameter applicable to the ETM penultimate mass. (RAL)

5.7 Shielded magnet recesses: ø 10 mm hole depth 1.0mm (+/-0.1mm)

Justification: Maintained in accordance with NP-type penultimate mass drawings (specification agreed at UK project weekly meeting ALUK Weekly Project Meeting (07/07/06)

ACTION 7-P: Confirm that this specification is appropriate for mating components/bonding process. (RAL)

⁵ D050421-SN-001, measured width (flat to flat) = 326.6mm, D050421-SN-002, measured width (flat to flat) = 326.7mm (both taken from NP-type penultimate mass inspection documents)

⁶ D080117_ ALIGO SUS ETM QUAD Penultimate Mass

⁷ Email from I. Wilmut to R. Jones 25th January 2008 “RE: DCN for PM and ERM”

5.8 Reference Markings: 2 off along centre-line of each flat, 1 off @ 12 o'clock, 1 off @ 6 o'clock

Justification: Size and shape of marking on flats (used during bonding process) maintained in accordance with NP-type penultimate mass drawings, with the exception of a tightened tolerance on the width of the reference marking (change from 0.25mm +/-0.1, to 0.25mm +/-0.05).

Reference markings at 12 o'clock and 6 o'clock differ from NP-type penultimate mass drawings (where markings covered the full width of each the mass, top and bottom). Reduction in size of each marking should improve accuracy over their length.

The addition of vertical reference markings to each flat signifying the centre of mass position (to aid the bonding process) was previously considered. However, through the combined effect of more accurate wire groove positions and more in depth inspection information, this was not thought necessary for the bonding process.

ACTION 8-P: Discuss/confirm with SUS colleagues (Glasgow/SUS)

5.9 Polishing: lambda/10 bond area changed to 60mm x 75mm centered on flat

Justification: NP-type penultimate mass drawings set the lambda/10 polish region to be biased towards the upper portion of the flat with a minimum clear aperture of 70mm x 55mm.

Note also that the NP-type ETM silica test mass specified a bond area of 100mm x 75mm centered on the flat. In each instance, the bond position is either located above the COM (in the case of the penultimate mass) or below (for the optic).

Changing to a bond area which is centered on the flat (combined with wire grooves around the full mass) adds value to each mass. In the event of a suspension failure causing damage to an ear or bond, the penultimate mass could be reworked/re-used by rotating through a period of 180 degrees.

Assessment of interferograms provided for the flats on the first delivered NP-type penultimate mass (D050421-001) required deliberation by IGR experts. There had been some difficulty in achieving the lambda/10 flatness at that time. However, the mass was deemed acceptable as it was proven that within the active area (APERTURE ZONE 1, in drawing D050421), any given area the size of an ear bond would meet the lambda/10 specification. Flats on the second NP-type penultimate mass (D050421-002) were significantly improved.

As a result of this experience a secondary specification could be desirable on the active bond area, in case there are problems in achieving the specification over the full area.

E.g.

SURFACE S1 AND S2:

SUPERPOLISH FLAT TO $\lambda/10$ PEAK TO VALLEY OVER APERTURE ZONE 1 (60mm x 75mm BOND AREA CENTERED ON FLAT).

ANY AREA, 15mm WIDE x 30mm DEEP WITHIN APERTURE ZONE 1, MUST BE AT LEAST FLAT TO $\lambda/10$ DURING INSPECTION.

ACTION 9-P: Confirm with SUS colleagues (Glasgow/SUS)

6 Conclusion

The proposed changes to the form of the ETM penultimate mass (as compared to the form of the Noise Prototype) are as follows:

- **Change to the tolerance on wire groove position (use of symmetry tolerance RFS)**
- **Extension of wire grooves around full barrel of mass**
- **Extension of lambda/10 bond area on flat, and its associated specification.**

Precise knowledge of centre of mass position shall be achieved by assessment of detailed inspection information.

All issues in the table below must be resolved before tender process can begin.

FEATURES	SIZE	Change from NP-type	ACTION No. / who	Confirmed
Diameter	ø340.0mm +/-0.25mm	None.	1-P/ Glasgow	Yes
Thickness	200.0mm +/-0.5mm	No change yet. (consider tolerance alteration)	2-P/ Glasgow /SUS	No*
Chamfer size	2.0mm +/-0.2mm, x 45 degree +/- 5 degrees ALL ROUND	None.	3-P/ Glasgow	Yes
Flat length	2x, 95.0mm (sharp to sharp)	No change yet! (DISCUSS)	4-P/ Glasgow/ SUS	No*
Wire Grooves	6.0mm+/-0.1mm (with 0.1 symmetrical tolerance)	Symmetric tolerance to reduce positional error. Reduction to radius at base of groove (from R0.3mm to R0.25mm MAX.)	5-P/ Glasgow/ RAL	No*
Associated wire diameters	ø 0.62mm	?	6-P/ RAL	No*
Shielded magnet recesses	ø 10 mm hole depth 1.0mm (+/- 0.1mm)	None.	7-P/ RAL	No*
Reference lines	2 off along centre-line of each flat, 1 off @ 12 o' clock, 1 off @ 6 o' clock	Reduced size of reference marks on barrel. (at 12 o'clock and 6 o'clock)	8-P/ Glasgow/ SUS	No*
Polishing	λ/10 bond area changed to 60mm x 75mm centered on flat	Increase bond area, symmetric about both central axes	9-P/ Glasgow/ SUS	No*

- It must also be confirmed (or otherwise) that the ITM penultimate mass is to be identical to the ETM penultimate mass (**ACTION: all to confirm**).

No reference has been made in this document to the need for transportation containers following manufacture.