

LASER INTERFEROMETER GRAVITATIONAL WAVE OBSERVATORY
-LIGO-
CALIFORNIA INSTITUTE OF TECHNOLOGY
MASSACHUSETTS INSTITUTE OF TECHNOLOGY

Technical Note LIGO-T040029- 00- R 2/26/2004

Encorporating coating anisotropy into coating thermal noise

Gregg Harry

This is an internal working note
of the LIGO Project.

California Institute of Technology

LIGO Project - MS 51-33

Pasadena CA 91125

Phone (626) 395-2129

Fax (626) 304-9834

E-mail: info@ligo.caltech.edu

Massachusetts Institute of Technology

LIGO Project - MS 20B-145

Cambridge, MA 01239

Phone (617) 253-4824

Fax (617) 253-7014

E-mail: info@ligo.mit.edu

WWW: <http://www.ligo.caltech.edu/>

Start with a description of an anisotropic multilayer coating from Hoff [1]:

$$\begin{aligned}
\epsilon_{rr} &= \sigma_{rr}/Y_{\parallel} - \sigma_{\parallel}\sigma_{\theta\theta}/Y_{\parallel} - \sigma_{\perp}\sigma_{zz}/Y_{\perp} \\
\epsilon_{\theta\theta} &= -\sigma_{\parallel}\sigma_{rr}/Y_{\parallel} + \sigma_{\theta\theta}/Y_{\parallel} - \sigma_{\perp}\sigma_{zz}/Y_{\perp} \\
\epsilon_{zz} &= -\sigma_{\perp}\sigma_{rr}/Y_{\perp} - \sigma_{\perp}\sigma_{\theta\theta}/Y_{\perp} + \sigma_{zz}/Y_{\perp}.
\end{aligned} \tag{1}$$

Here, Y_{\parallel} is the Young's modulus for stresses causing strains entirely within the plane parallel to the coating layers. Y_{\perp} is the Young's modulus for stresses causing strains perpendicular to the coating layers. There are two Poisson's ratios, σ_{\parallel} for stresses and strains both with the plane parallel to the coating layers, and σ_{\perp} for when either the stress or the strain is perpendicular to the coating layers.

The matrix in Eq. 1 can be inverted, to read

$$\begin{aligned}
\sigma_{rr} &= (\lambda_1 + 2\mu_1) \epsilon_{rr} + \lambda_1 \epsilon_{\theta\theta} + \lambda_2 \epsilon_{zz} \\
\sigma_{\theta\theta} &= \lambda_1 \epsilon_{rr} + (\lambda_1 + 2\mu_1) \epsilon_{\theta\theta} + \lambda_2 \epsilon_{zz} \\
\sigma_{zz} &= \lambda_2 \epsilon_{rr} + \lambda_2 \epsilon_{\theta\theta} + (\lambda_2 + 2\mu_2) \epsilon_{zz},
\end{aligned} \tag{2}$$

where

$$\lambda_1 = -Y_{\parallel} (\sigma_{\perp}^2 Y_{\parallel} + \sigma_{\parallel} Y_{\perp}) / ((\sigma_{\parallel} + 1) (2\sigma_{\perp}^2 Y_{\parallel} - (1 - \sigma_{\parallel}) Y_{\perp})), \tag{3}$$

$$\mu_1 = Y_{\parallel} / (2(1 + \sigma_{\parallel})), \tag{4}$$

$$\lambda_2 = \sigma_{\perp} Y_{\parallel} Y_{\perp} / (-2\sigma_{\perp}^2 Y_{\parallel} + (1 - \sigma_{\parallel}) Y_{\perp}), \tag{5}$$

$$\mu_2 = Y_{\perp} (\sigma_{\perp} Y_{\parallel} - (1 - \sigma_{\parallel}) Y_{\perp}) / (2(2\sigma_{\perp}^2 Y_{\parallel} - (1 - \sigma_{\parallel}) Y_{\perp})). \tag{6}$$

Equation 2 is the anisotropic equivalent of Gretarsson's equation A2 in ref. [2]. Following the same procedure as in that reference, the equivalent of Gretarsson's equation A4 is found;

$$\begin{aligned}
\epsilon'_{rr} &= \epsilon_{rr} \\
\epsilon'_{\theta\theta} &= \epsilon_{\theta\theta} \\
\epsilon'_{zz} &= (\lambda - \lambda_2) / (\lambda_2 + 2\mu_2) (\epsilon_{rr} + \epsilon_{\theta\theta}) + (\lambda + 2\mu) / (\lambda_2 + 2\mu_2) \epsilon_{zz} \\
\epsilon'_{rz} &= \epsilon_{rz} \\
\sigma'_{rr} &= (\lambda_1 + 2\mu_1) \epsilon_{rr} + \lambda_1 \epsilon_{\theta\theta} + \lambda_2 \epsilon'_{zz} \\
\sigma'_{\theta\theta} &= \lambda_1 \epsilon_{rr} + (\lambda_1 + 2\mu_2) \epsilon_{\theta\theta} + \lambda_2 \epsilon'_{zz} \\
\sigma'_{zz} &= \sigma_{zz} \\
\sigma'_{rz} &= \sigma_{rz}.
\end{aligned} \tag{7}$$

Here, all the parameters without numerical subscripts refer to values in the substrate.

Following the method of Gretarsson as in [2] with the changes noted above for an anisotropic modulus, the effective loss angle ϕ_{readout} for thermal noise calculations in an interferometer can be found.

$$\phi_{\text{readout}} = \phi_{\text{substrate}} + d / (\sqrt{\pi} w Y_{\perp})$$

$$\begin{aligned}
& \left(\left(Y / (1 - \sigma_{\perp}^2) - 2\sigma_{\perp}^2 Y Y_{\parallel} / (Y_{\perp} (1 - \sigma^2) (1 - \sigma_{\parallel})) \right) \right) \phi_{\perp} \\
& + Y_{\parallel} \sigma_{\perp} (1 - 2\sigma) / \left((1 - \sigma_{\parallel}) (1 - \sigma) \right) (\phi_{\parallel} - \phi_{\perp}) \\
& + Y_{\parallel} Y_{\perp} (1 + \sigma) (1 - 2\sigma)^2 / \left(Y (1 - \sigma_{\parallel}^2) (1 - \sigma) \right) \phi_{\parallel}.
\end{aligned} \tag{8}$$

This is to be compared to equation 20 in reference [2].

The limit of Eq. 8 where all the Poisson ratios are small, $\sigma_{\parallel} = \sigma_{\perp} = \sigma = 0$, gives

$$\phi_{\text{readout}} = \phi_{\text{substrate}} + d / (\sqrt{\pi} w) \left(Y / Y_{\perp} \phi_{\perp} + Y_{\parallel} / Y \phi_{\parallel} \right). \tag{9}$$

The limit when $Y_{\parallel} = Y_{\perp} = Y'$ and $\sigma_{\parallel} = \sigma_{\perp} = \sigma'$, ie when the coating is assumed isotropic except in its loss angles, Eq. 8 reproduces Eq. 21 in reference [2].

The values for Y_{\perp} , Y_{\parallel} , ϕ_{\perp} and ϕ_{\parallel} can be calculated from the values of the isotropic materials that make up the layers of the coating. For a coating of two layers,

$$Y_{\perp} = (d_1 + d_2) / (d_1 / Y_1 + d_2 / Y_2), \tag{10}$$

$$Y_{\parallel} = (Y_1 d_1 + Y_2 d_2) / (d_1 + d_2), \tag{11}$$

$$\phi_{\perp} = Y_{\perp} (\phi_1 d_1 / Y_1 + \phi_2 d_2 / Y_2) / (d_1 + d_2), \tag{12}$$

$$\phi_{\parallel} = (Y_1 \phi_1 d_1 + Y_2 \phi_2 d_2) / [Y_{\parallel} (d_1 + d_2)], \tag{13}$$

where d_1 and d_2 are the total thicknesses, Y_1 and Y_2 are the isotropic Young's moduli, and ϕ_1 and ϕ_2 are the isotropic loss angles of the two materials that make up the coating.

To use the full formula in Eq. 8, values for the Poisson ratios are needed. The Poisson ratio connecting stress in the z direction with strains in the plane of the coating, $\theta - r$, σ_{\perp} can be found from

$$\sigma_{\perp} = (\sigma_1 Y_1 d_1 + \sigma_2 Y_2 d_2) / (Y_1 d_1 + Y_2 d_2). \tag{14}$$

The equivalent formula for σ_{\parallel} is more complicated. The value for σ_{\parallel} can be found by numerically solving

$$\lambda_1 = (\sigma_1 Y_1 d_1 / ((1 + \sigma_1) (1 - 2\sigma_1)) + \sigma_2 Y_2 d_2 / ((1 + \sigma_2) (1 - 2\sigma_2))) / (d_1 + d_2). \tag{15}$$

For $\text{SiO}_2/\text{Ta}_2\text{O}_5$ coatings in the appropriate ratios to make an HR coating for 1.062 μm light, these values are

$$\sigma_{\perp} = 0.19, \tag{16}$$

$$\sigma_{\parallel} = 0.21. \tag{17}$$

References

- [1] N. J. Hoff in *Engineering Laminates*, ed. A. G. H. Hoff (John Wiley and Sons, New York, 1949).
- [2] G. M. Harry, A. M. Gretarsson, P. R. Saulson, S. E. Kittleberger, S. D. Penn, W. J. Startin, S. Rowan, M. M. Fejer, D. R. M. Crooks, G. Cagnoli, J. Hough, and N. Nakagawa, *Class. Quantum Grav.* **19**(2003)897.