# **Digital Filter Noise**

# Why does the textbook tell us not to use direct form 2?

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## Introduction

- Read ref1, in particular chapter 6
- z-transform to go from s-domain to zdomain

$$H(s) = G \frac{s^{2} + B_{1}s + B_{2}}{s^{2} + A_{1}s + A_{2}} \rightarrow H(z) = g \frac{1 + b_{1}z^{-1} + b_{2}z^{-2}}{1 + a_{1}z^{-1} + a_{2}z^{-2}}$$

 Once you have the z-domain coefficient, your filter equation is

$$y_n = g(x_n + b_1 x_{n-1} + b_2 x_{n-2}) - a_1 y_{n-1} - a_2 y_{n-2}$$

## "Direct Form 1" Implementation

- Direct implementation of equation for y<sub>n</sub>
- The TF is performed in two steps

$$H(f) = g \times H_{zeros}(f) \times H_{poles}(f)$$



"Direct Form 2" Implementation

- Rearrange DF1 to get DF2
  - Equivalent computation
  - Uses less memory



$$H_{poles}(f_s/4) \approx 1$$

$$H_{zeros}(f_s/4) \approx 1$$

# Direct Form 2 Fixed Point Noise Analysis

- With fixed point numbers, the quantization noise analysis is relatively easy (ref 1)
- Noise added at each multiplication



## Direct Form 2 Fixed Point Noise Analysis

The output noise power density is

$$N_{OUT}(f) = N_{Quant} \left( \frac{1}{2} |H(f)|^2 + 2 \right)$$



where

 $N_{Quant} = \frac{2^{-2B}}{12f_s}$ 

and B is the number of bits after the decimal point and fs the sample frequency. For example, with B=64 and  $f_s = 16384$  Hz,

$$n_{Quant} = \sqrt{N_{Quant}} = \frac{2^{-B}}{\sqrt{12f_s}} \cong \frac{10^{-22}}{\sqrt{Hz}}$$

# Direct Form 2 Floating Point Noise Analysis

- With floating point numbers, things are more complicated
  - Noise added at multiplications and additions
  - Noise depends on the signal



## Direct Form 2 Floating Point Noise Analysis

$$N_{OUT}(f) = N_{Quant} \left( \sum_{input} A_i^2 |H(f)|^2 + \sum_{output} A_j^2 \right)$$



Where  $A_i$  is the floating point multiplier used in each operation.  $N_{Quant}$  is as before, with B the number of bits in the mantissa. For example, a signal between 8 and 16, expressed in double precision, would have

$$A \times n_{Quant} = 8 \frac{2^{-53}}{\sqrt{12f_s}} \cong \frac{2 \times 10^{-18}}{\sqrt{Hz}}$$

for  $f_s = 16384$  Hz as before.

## Direct Form 2 Noise Analysis: Example 1

- Input signal white (BW = 8kHz)
- 2 poles and 2 zeros 1Hz
  - Roughly:  $a_1 = -2 + \epsilon$ ,  $a_2 = 1 \epsilon$ ,  $b_0 = 1$ ,  $b_1 = a_1$ ,  $b_2 = a_2$



All of the operations involve the signal filtered by the poles. The amplitude spectral density is about  $10^7$  in DC. Taking A<sub>MID</sub> to be the RMS of this signal,

$$n_{OUT}(f) = \sqrt{8A_{MID}^2 N_{Quant}} \cong \frac{6 \times 10^{-12}}{\sqrt{Hz}}$$

as compared to

$$n_{IN}(f) = \sqrt{A_{IN}^2 N_{Quant}} \cong \frac{2 \times 10^{-15}}{\sqrt{Hz}}$$

## Direct Form 2 Noise Analysis: Example 2

- Input signal pink
  - RMS dominated by low-frequency signal
  - typical of LIGO signals
  - Assume RMS of input  $A_{IN} = 1$ DF2 OUT  $n_{IN}(f) = \sqrt{A_{IN}^2 N_{Quant}} \approx \frac{2 \times 10^{-19}}{\sqrt{H_7}}$



which makes the unchanged output noise seem very large

$$n_{OUT}(f) = \sqrt{8A_{MID}^2 N_{Quant}} \cong \frac{6 \times 10^{-12}}{\sqrt{Hz}}$$

# **Biquad Form**

- Biquad form avoids large internal values
  - A null filter (as in previous example) leads to no added noise
  - Requires one additional summation



$$a_{11} = -a_1 - 1$$

$$a_{12} = -a_2 - a_1 - 1$$

$$c_1 = b_1 - a_1$$

$$c_2 = b_2 - a_2 + b_1 - a_1$$

The "biquad" form is a particular state-space arrangement which minimizes flops. Its layout is very similar to the analog biquad filter.

# Biquad Form Noise Analysis

 For non-null filters, the internal signal RMS is similar to the output RMS, so

 $N_{OUT}(f) \approx 8N_{Quant} \max\left(A_{input}^2, A_{output}^2\right)$ 



# DF2 vs. BQF Empirical Results

- High and low frequency input
- 4<sup>th</sup> order notch
  - -fp=fz=1Hz
  - -Qp=1
  - Qz=1e6

 $x_{input} = \sin(2\pi \times t) + 10^{-9} \sin(2\pi \times t \times f_s / 4)$ 



# DF2 vs. BQF Empirical Results

- Output noise roughly as expected in both cases
- Biquad reveals quant noise not well modeled by white noise

$$x_{input} = \sin(2\pi \times t) + 10^{-9} \sin(2\pi \times t \times f_s / 4)$$



# Conclusion

- Direct Form 2, used by LIGO, is not a good choice for low-noise filtering
- Noise in floating point DSP has been studied extensively for high-quality audio applications
- Many low-noise implementations are available
  - State-space second-order sections are general
  - Noise optimized forms usually involve more flops
- For a very modest increase in computational time, we can improved noise performance by many orders of magnitude

### References

- 1. <u>Discrete-Time Signal Processing</u> Oppenheim and Schafer, 2<sup>nd</sup> Ed 1999
- "Floating-point roundoff noise analysis of second-order state-spacedigital filter structures" Smith, L.M.; Bormar, B.W.; Joseph, R.D.; Yang, G.C.-J. Circuits and Systems II: Analog and Digital Signal Processing, <u>IEEE Transactions on</u> <u>Volume 39, Issue 2, Feb 1992 Page(s):90 – 98</u>

# A LIGO Signal

- Strain
  - RMS dominated
     by 18Hz peak
  - Added 160dB
     band-stop around
     150Hz
- A notch at 1Hz induces noise in the stop-band



## Low-Noise Form

- Proposed form avoids large internal values
  - A null filter (as in previous example) leads to no added noise
  - Requires no additional flops



$$d_n = b_n - a_n$$

# Low-Noise Form Noise Analysis

$$N_{OUT}(f) = N_{Quant} \left( A_{input}^2 \left| H(f) \right|^2 + \sum_{loop} A_i^2 \left| H_{poles}(f) \right|^2 + A_{output}^2 \right)$$



For non-null filters, the internal signal RMS is similar to the output RMS, so

$$N_{OUT}(f) \approx N_{Quant} A_{output}^2 \left( 2 + 6 \left| H_{poles}(f) \right|^2 \right)$$

which is similar to DF2 below the pole frequency, but lower above that frequency.

# DF2 vs. BQF Empirical Results

- High and low frequency input
- 4<sup>th</sup> order notch
  - -fp=fz=1Hz
  - -Qp=1

-Qz=1e6





## DF2 vs. LNF Empirical Results

 Output noise close to expected in both cases

