



# Measurements of Thermal Noise in Optimized Coatings

Thermal Noise Interferometer

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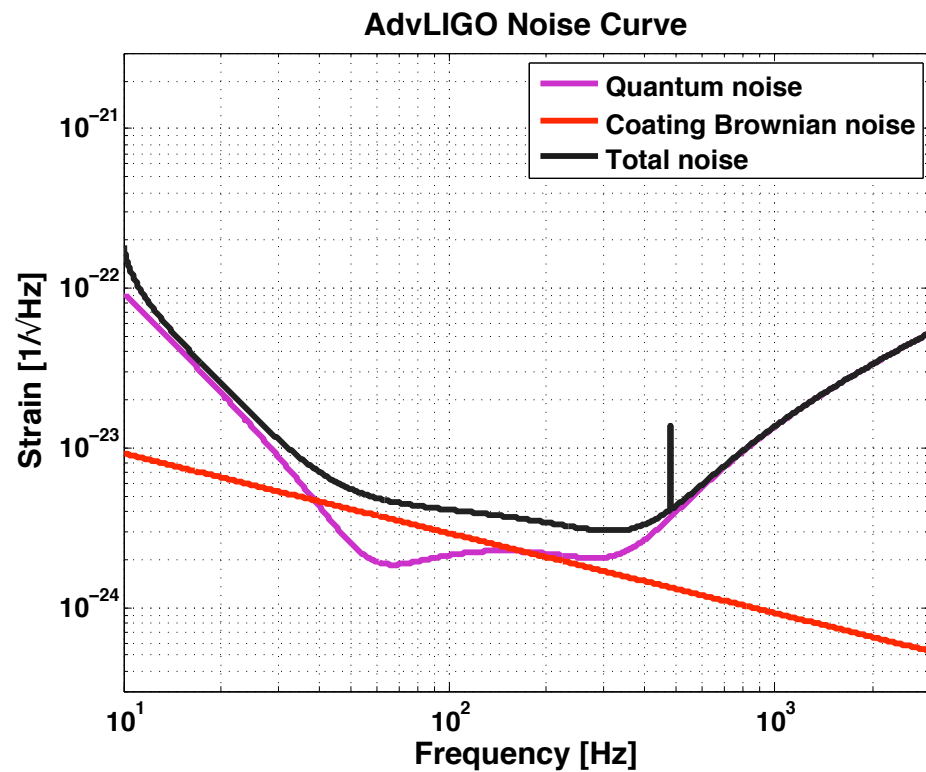
University of Sannio

Innocenzo Pinto, Vincenzo Pierro, Maria Principe



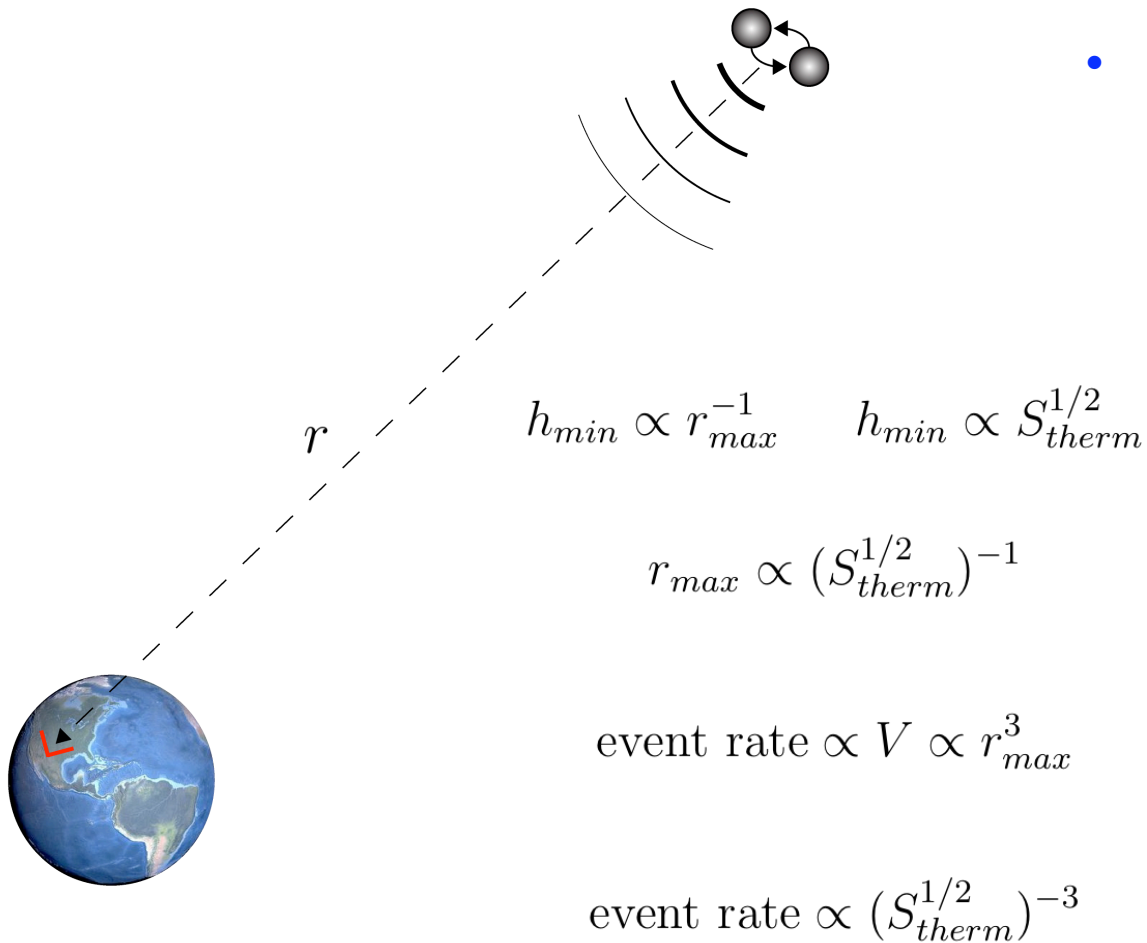
## Advanced LIGO Noise Floor

- Coating thermal noise will limit sensitivity around 100 Hz
- Reductions in coating noise lead directly to improvements in sensitivity



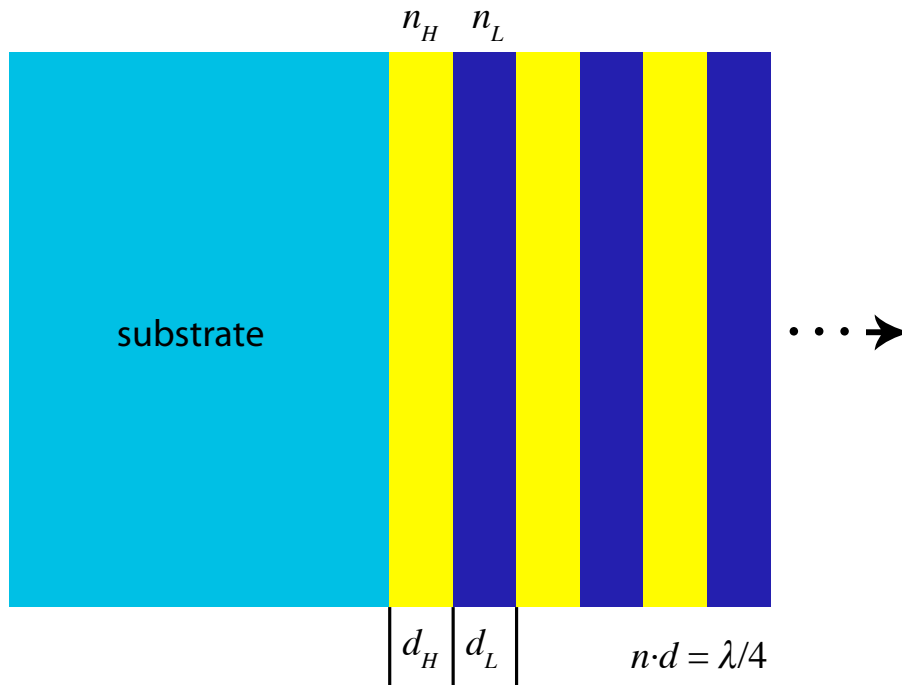


## Lower Noise Floor Means More Events



- Small improvement in thermal noise floor means big gain in event rate

## Standard Multilayer Dielectric Coatings



- Alternating layers of high and low index materials
- Quarter wavelength optical thickness for best reflectivity
- Silica low-index, tantala high-index for good performance at 1064nm
- Thermal noise arises from internal friction in the coatings

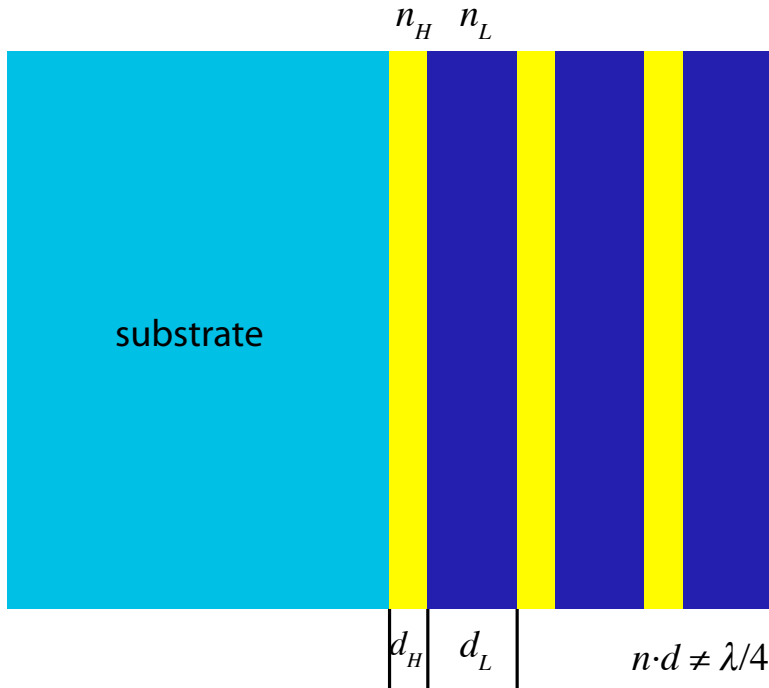
$$S_x(f) = \frac{2k_B T}{\pi^{3/2} f} \frac{(1 - \sigma^2)}{wY} \phi_{eff}$$

$$\phi_{eff} \propto (L_L + \gamma \cdot L_H)$$

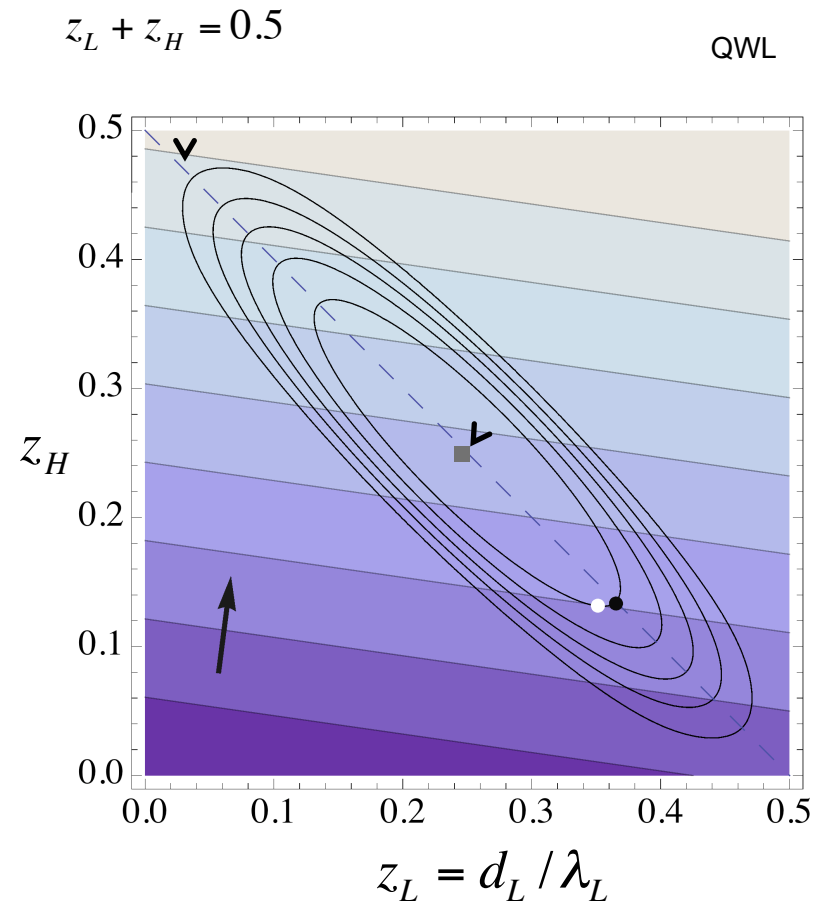
$$\gamma \propto \frac{Y_H \phi_H}{Y_L \phi_L}$$

# Optimized Coatings

- Tantala is more lossy than silica
- Reduce the amount of tantala in the coating



- Optimum coating is still a stack of identical “doublets”
- Simplify things by making the doublets  $\lambda/2$  thick





## Optimization Strategy

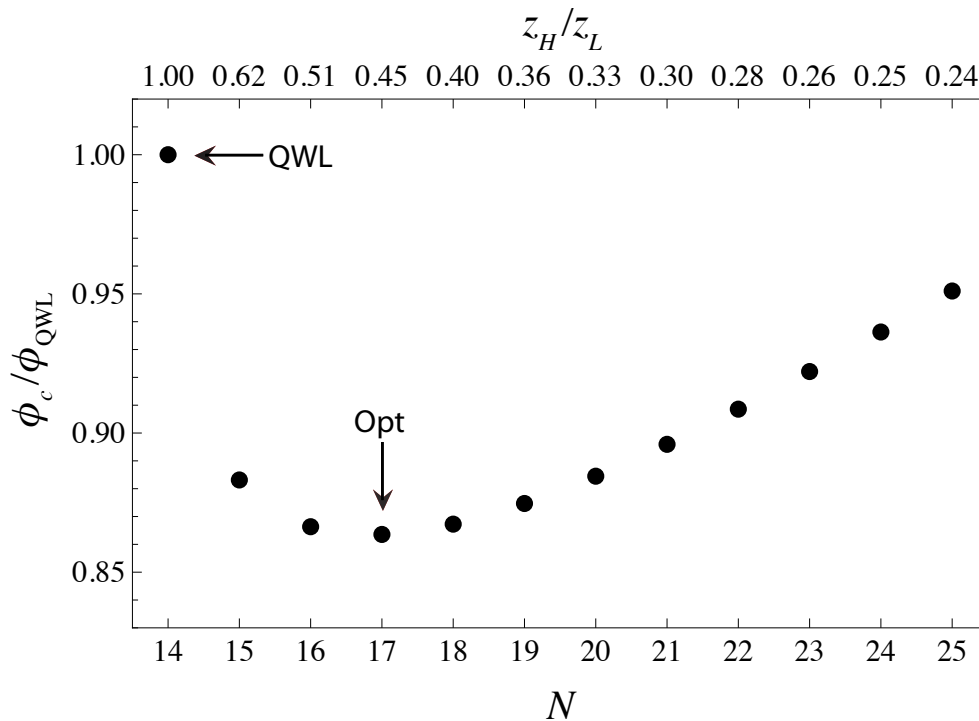
$$\tau(N_d, z_H) = \tau_{QWL}$$

$$\phi_{eff} = b_L L_L + b_H L_H$$

$$b_{L,H} = \frac{\lambda_0}{\pi w} \frac{\phi_{L,H}}{n_{L,H}} \left( \frac{Y_{L,H}}{Y_s} + \frac{Y_s}{Y_{L,H}} \right)$$

$$\gamma = b_H / b_L = [5, 10]$$

- Start from QWL design of  $N_{QWL}$  doublets and transmission  $\tau_{QWL}$
- Add one doublet and adjust layer thickness (keeping  $z_H + z_L = 0.5$ ) until  $\tau_{QWL}$  is recovered
- Calculate new  $\phi_{eff}$
- Repeat until minimum noise design is found

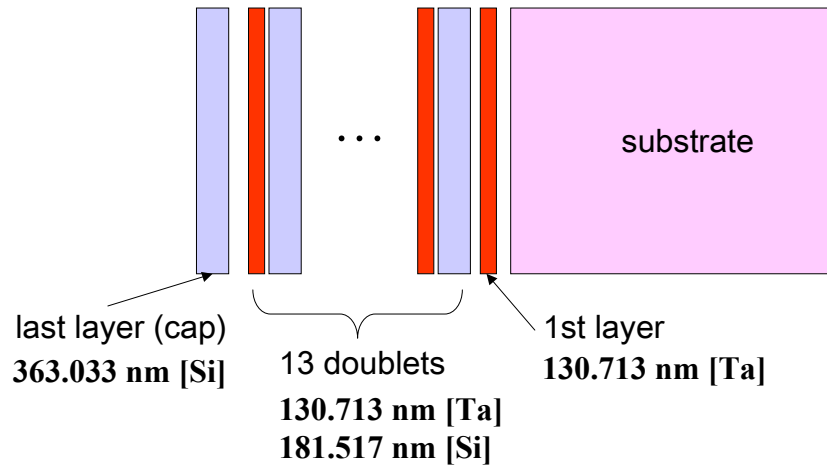




# Final Design

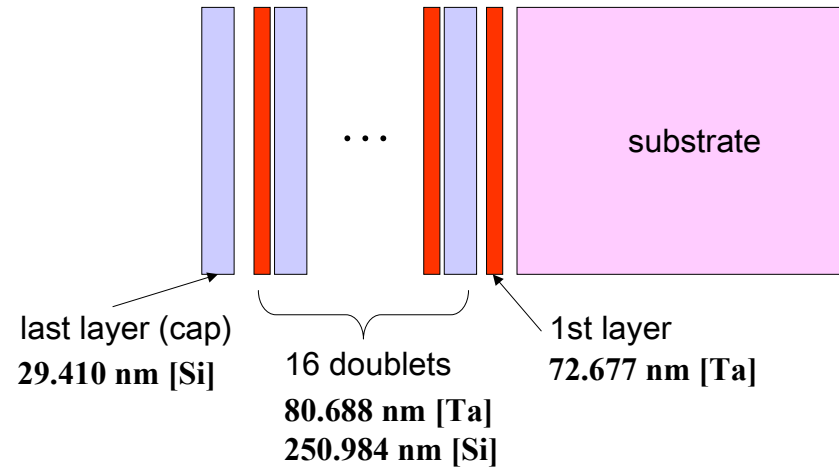
Reference QWL

Silica  
 Tantala



Optimized Prototype

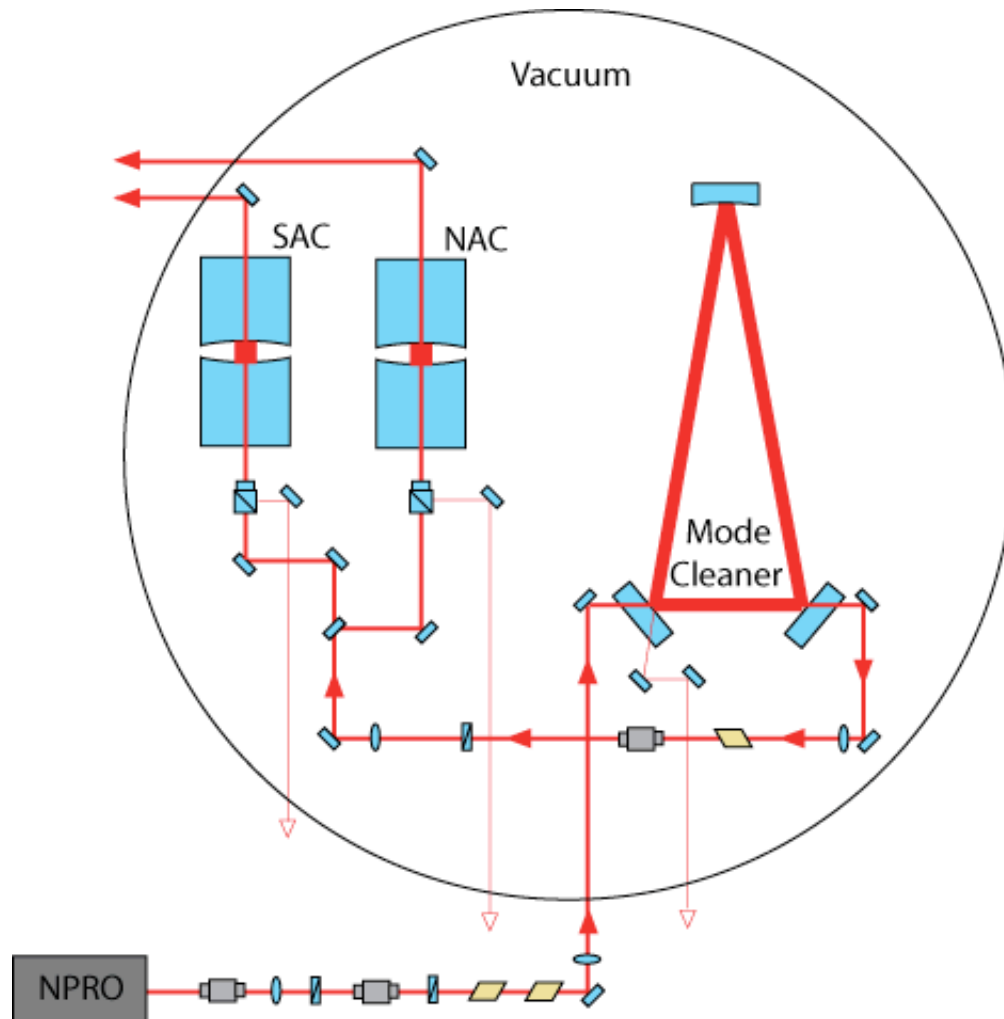
Silica  
 Tantala



$$\tau = 278 \text{ ppm}$$

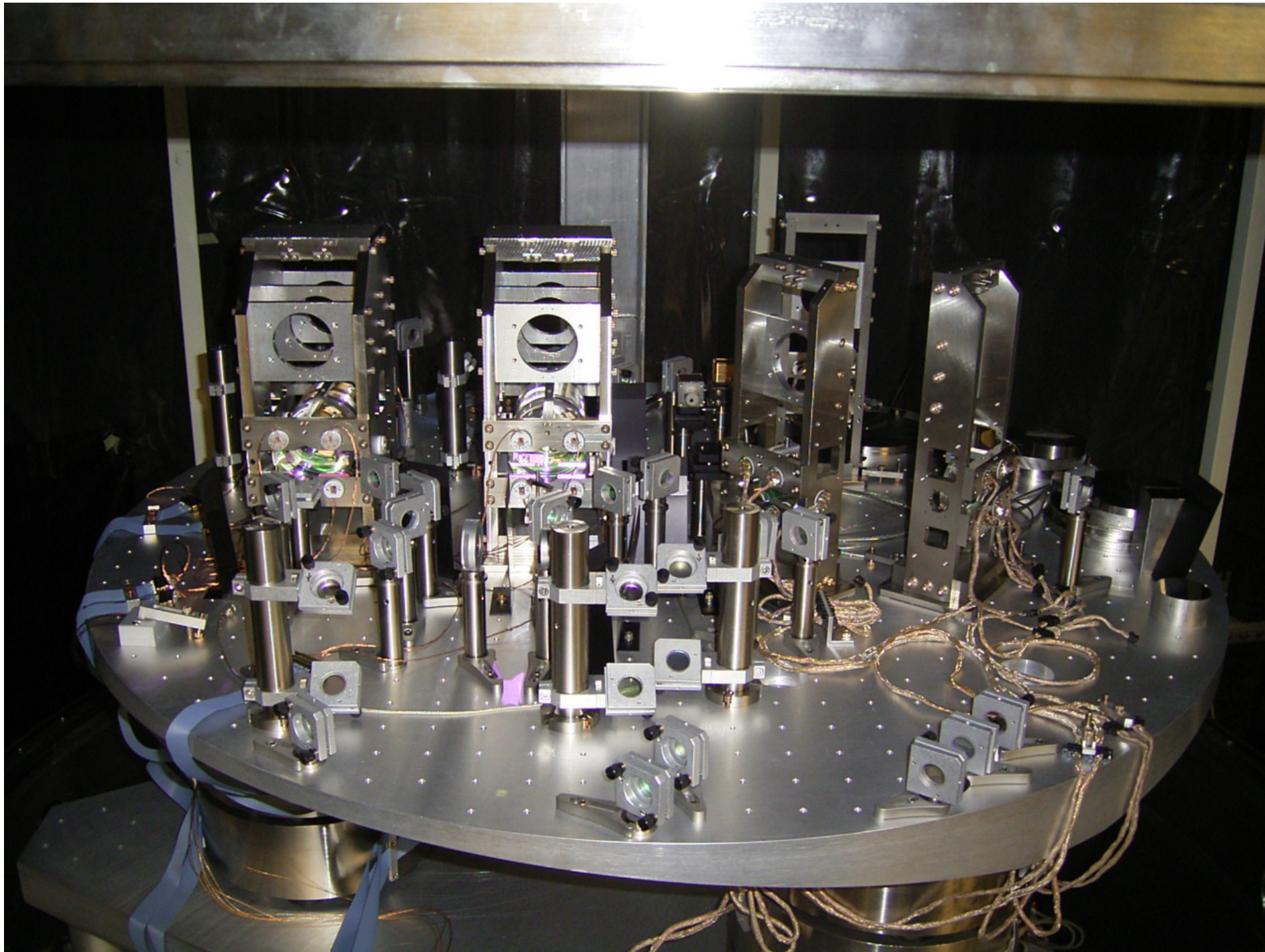
$$r = \frac{\phi_{Opt}}{\phi_{QWL}} = 0.843 \quad (\gamma = 7)$$

## Thermal Noise Interferometer



- Test bed interferometer designed to measure thermal noise in optics
- Short test cavities reduce laser frequency noise
- Small spot size increases thermal noise
- Two test cavities permit CMR
- Sensitivity is better than  $10^{-18}$  m/rHz

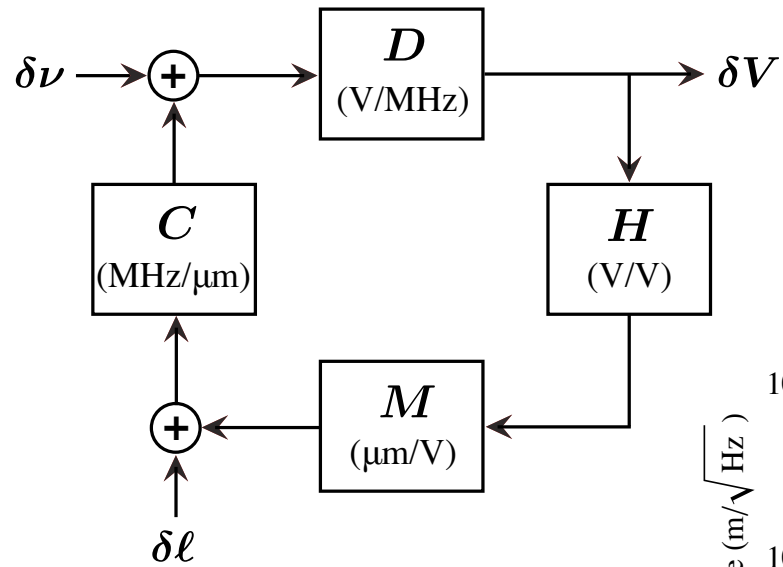




G0900647-v1



# Test Cavity Servo

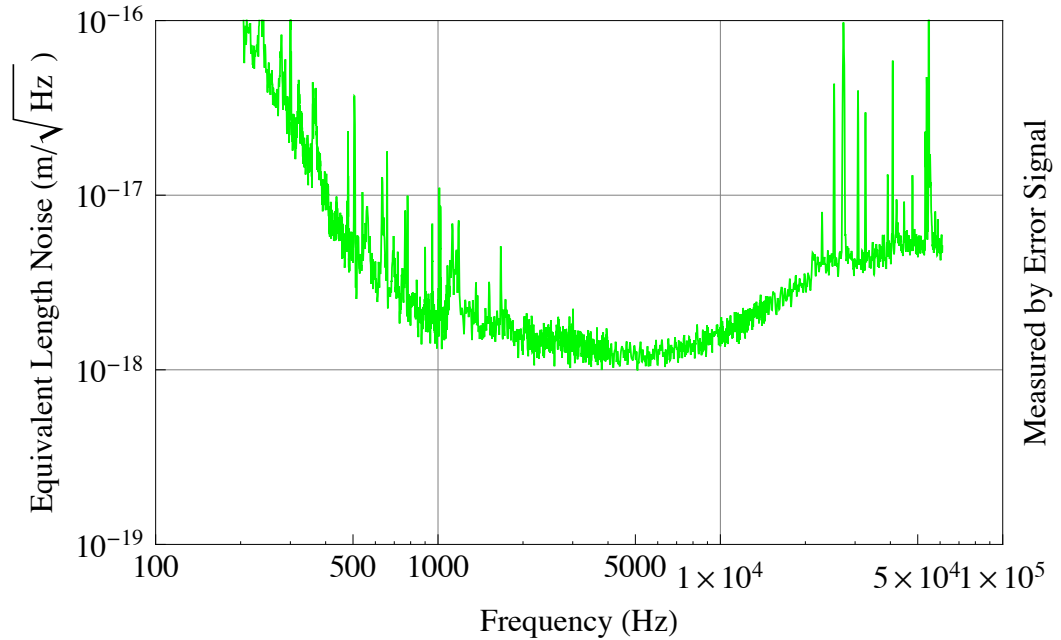


$$\delta V = \frac{DC}{1 - DCMH} \delta \ell$$

$$\delta V = T \delta \ell$$

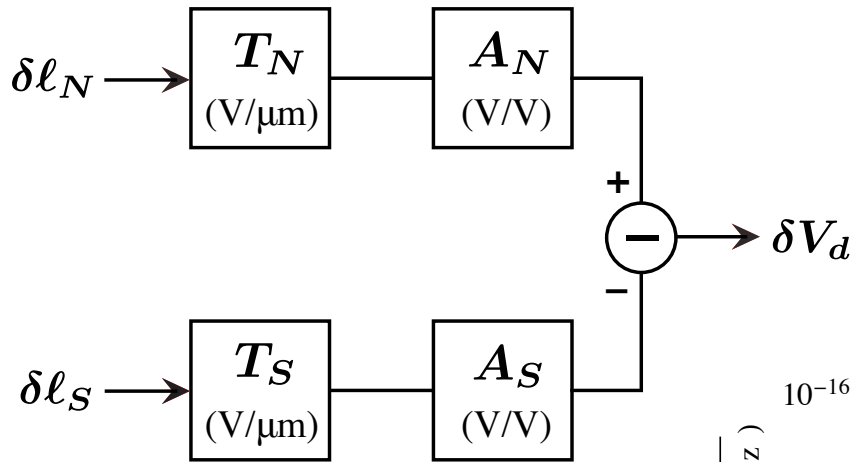
$$\delta \ell = T^{-1} \delta V$$

TNI NAC Cavity Length Noise, 2/10/04





## Common Mode Rejection

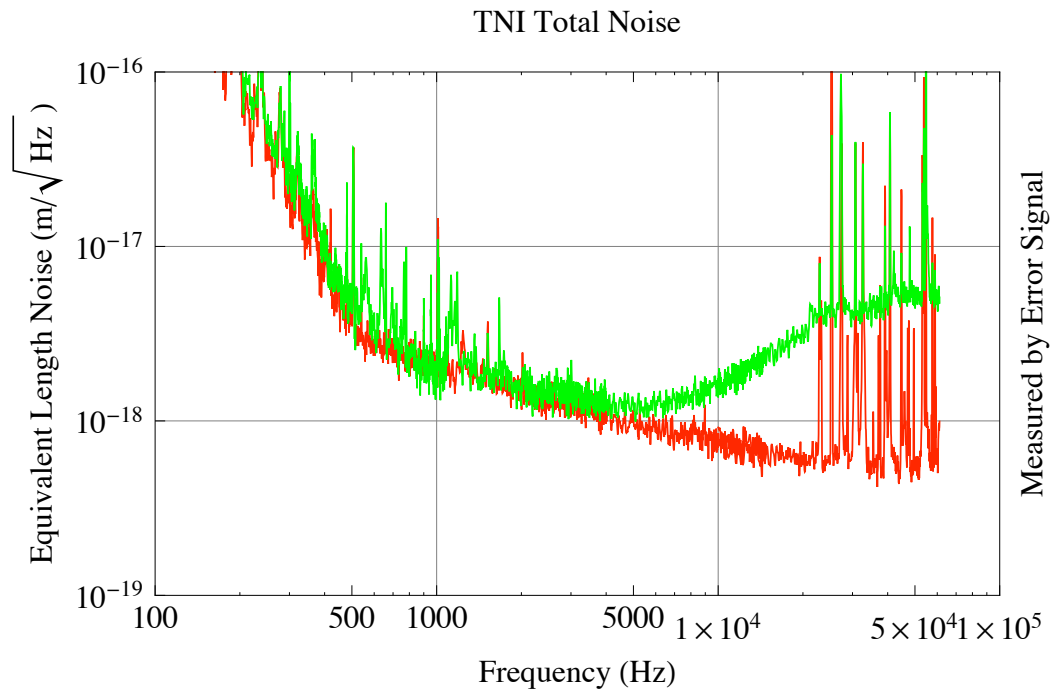


$$\delta l_d \equiv \delta l_N - \delta l_S$$

$$\delta l_d \approx \frac{1}{2} \left( A_N^{-1} T_N^{-1} + A_S^{-1} T_S^{-1} \right) \delta V_d$$

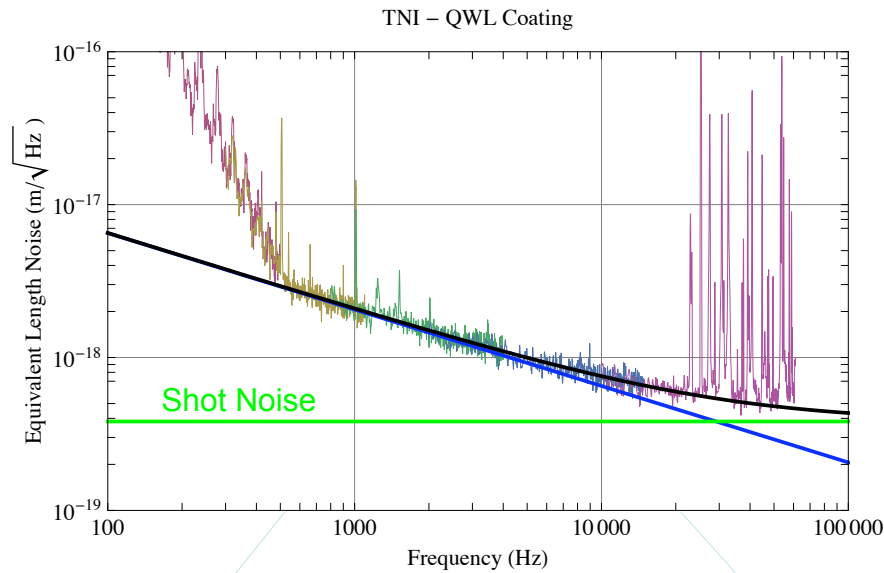
$$\delta l_d \approx \frac{1}{2} \left( A_N^{-1} D_N^{-1} C^{-1} + A_S^{-1} D_S^{-1} C^{-1} \right) \delta V_d$$

- Laser frequency noise is correlated in both cavities thermal noise is not
- CMR allows thermal noise to be visible up to higher frequencies
- Noise floor at high frequencies becomes shot noise dominated



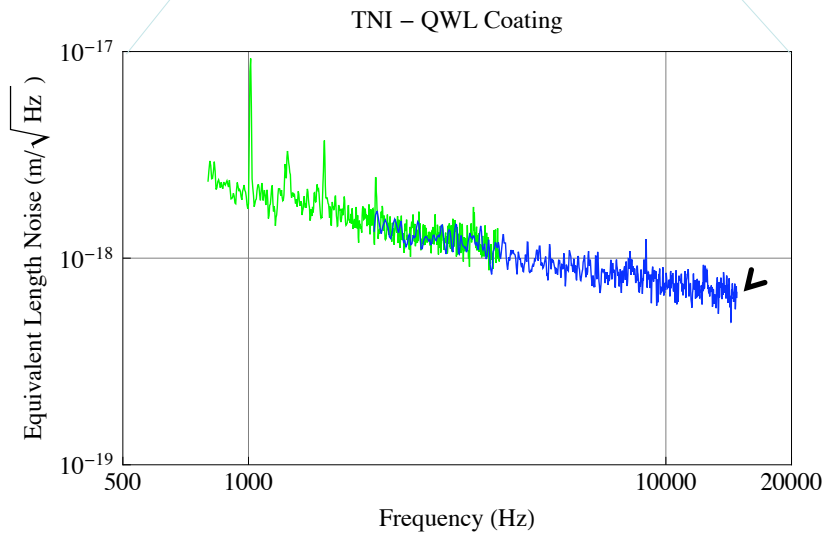


# Extracting the Loss Angle



$$S_B(f) = \frac{2k_B T}{\pi^{3/2} f} \frac{(1 - \sigma^2)}{wY} \phi_{eff}$$

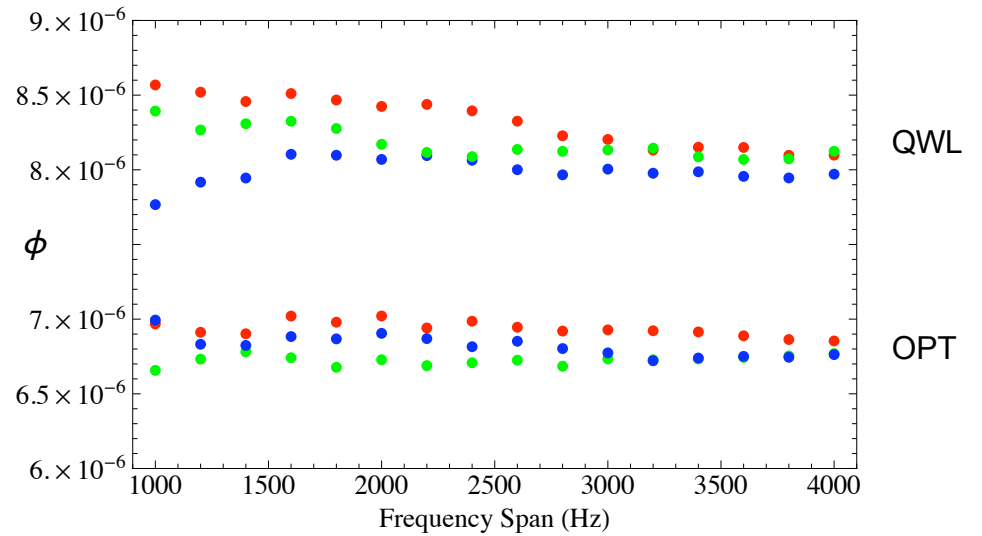
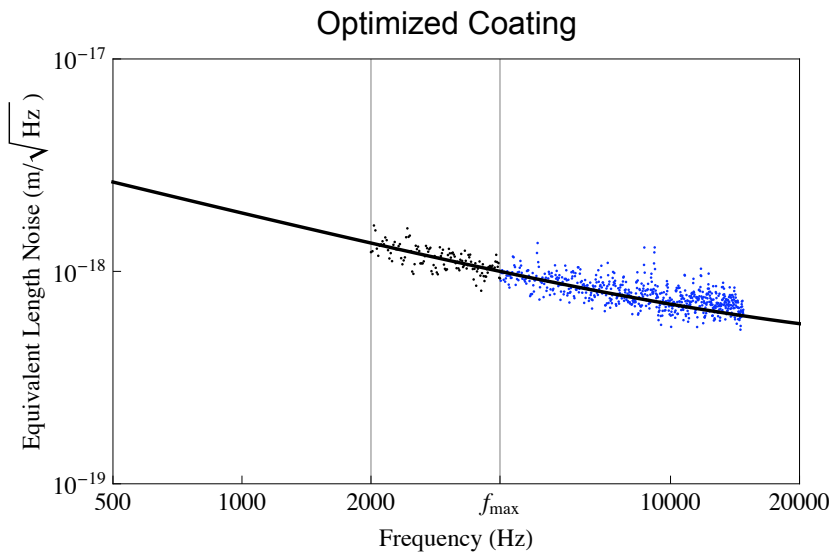
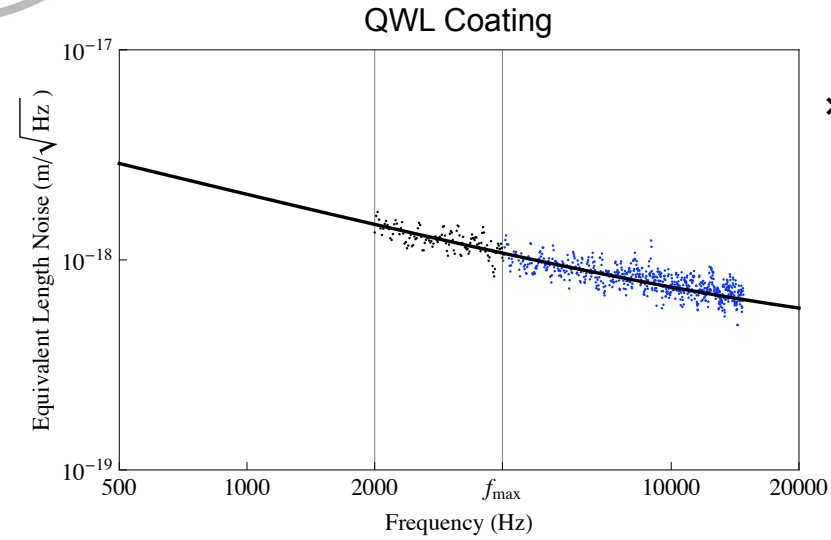
$$\ell(f) = \sqrt{4 S_B(f) + S_s}$$



Fit to data with  $\phi$  as the free parameter

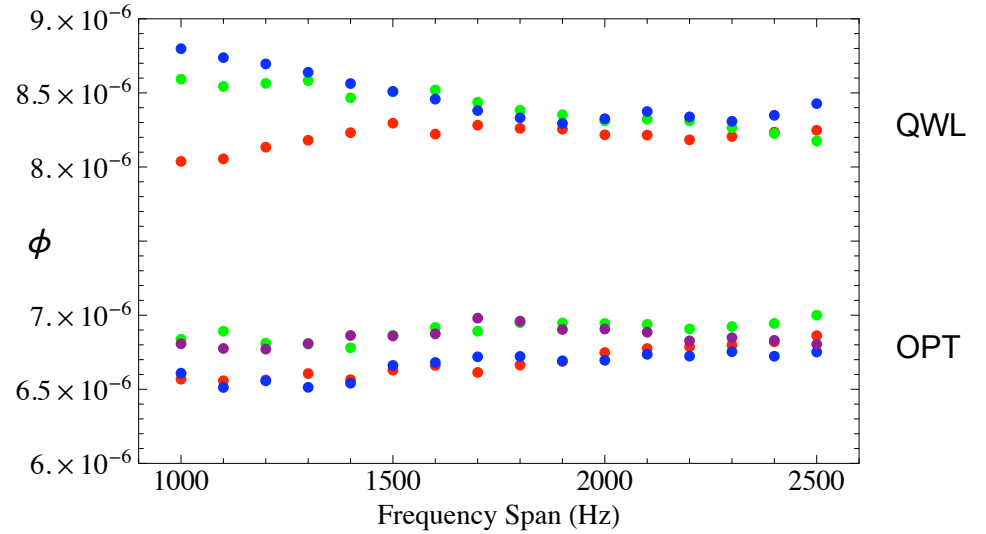
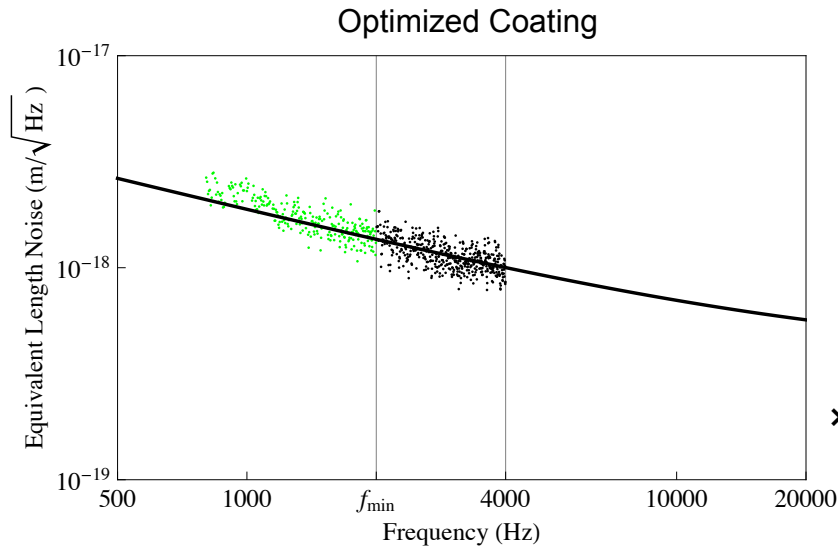
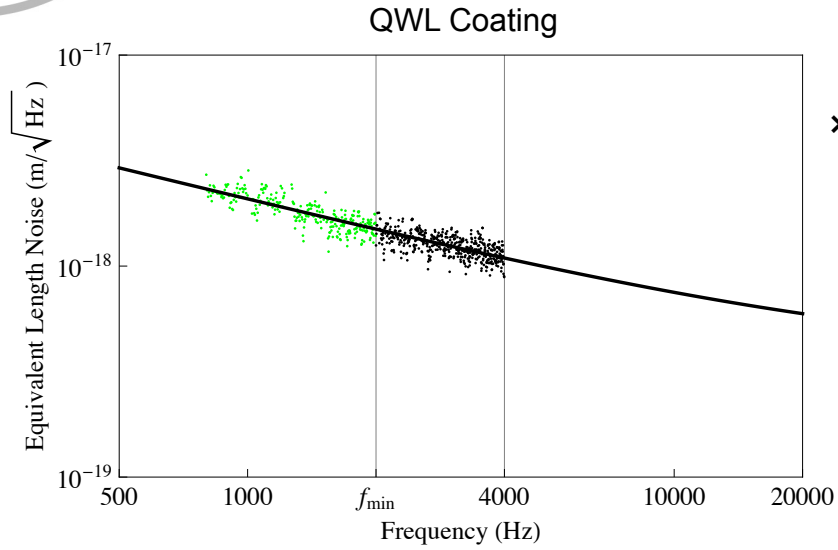


# Consistency of Loss Angle





# Consistency of Loss Angle





## Final Results

	Span (Hz)			
	1500	2000	2500	2500
$\bar{\phi}_{QWL}$	8.4	8.3	8.2	8.3
$\bar{\phi}_{OPT}$	6.8	6.9	6.9	6.9
$r$	0.81	0.83	0.83	0.83

$\times 10^{-6}$

Measured loss angle ratio:

$$r = 0.83 \pm 0.05$$

Compare to expected value of:

$$r = 0.843$$

- 17% reduction in loss angle
- 32% increase in event rate



## The Scatter Is Normal

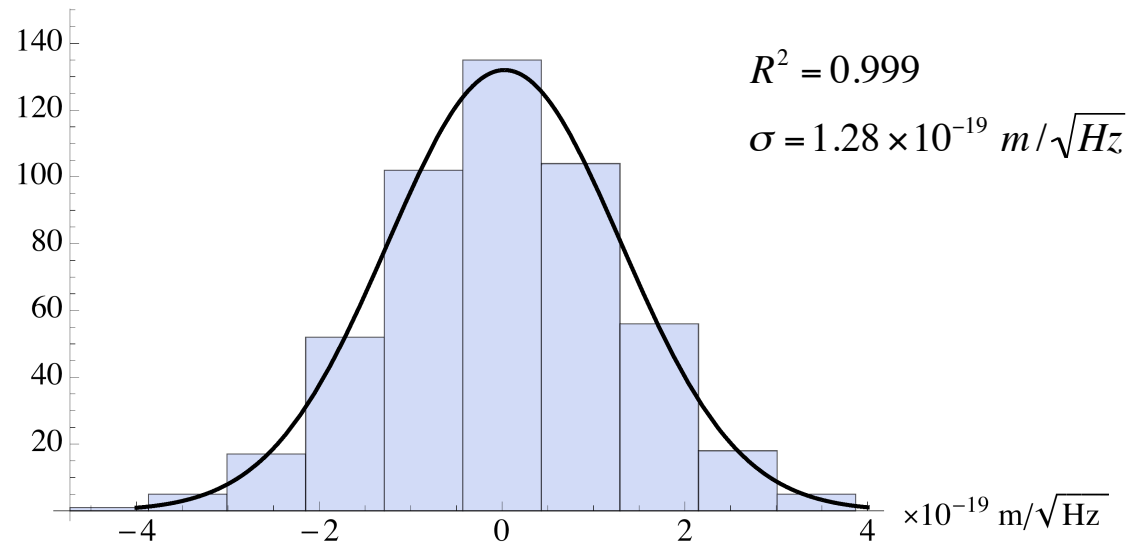
Data:

$$\{f_i, y_i\}$$

Fit Residuals:

$$\delta_i = y_i - \bar{\ell}(f_i)$$

Histogram >



## And Negligible

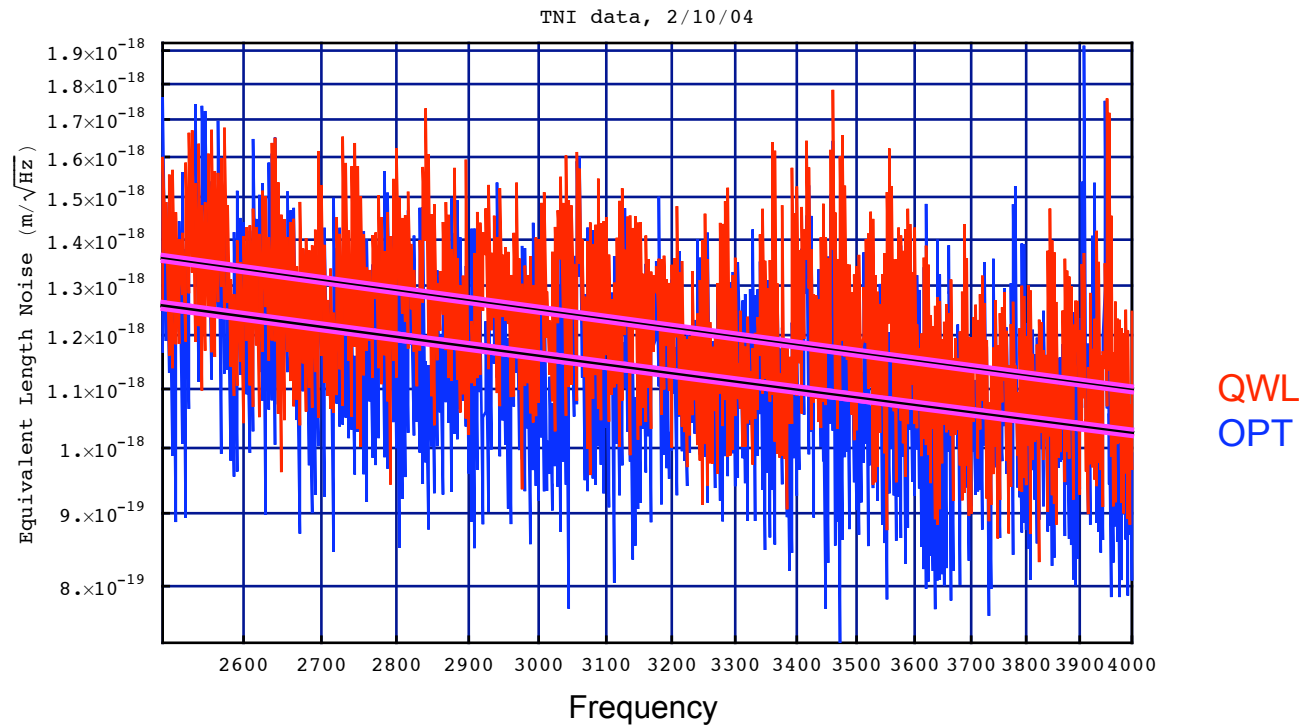
Fit uncertainty is not  $\sigma$

But rather  $\frac{\sigma}{\sqrt{N}}$





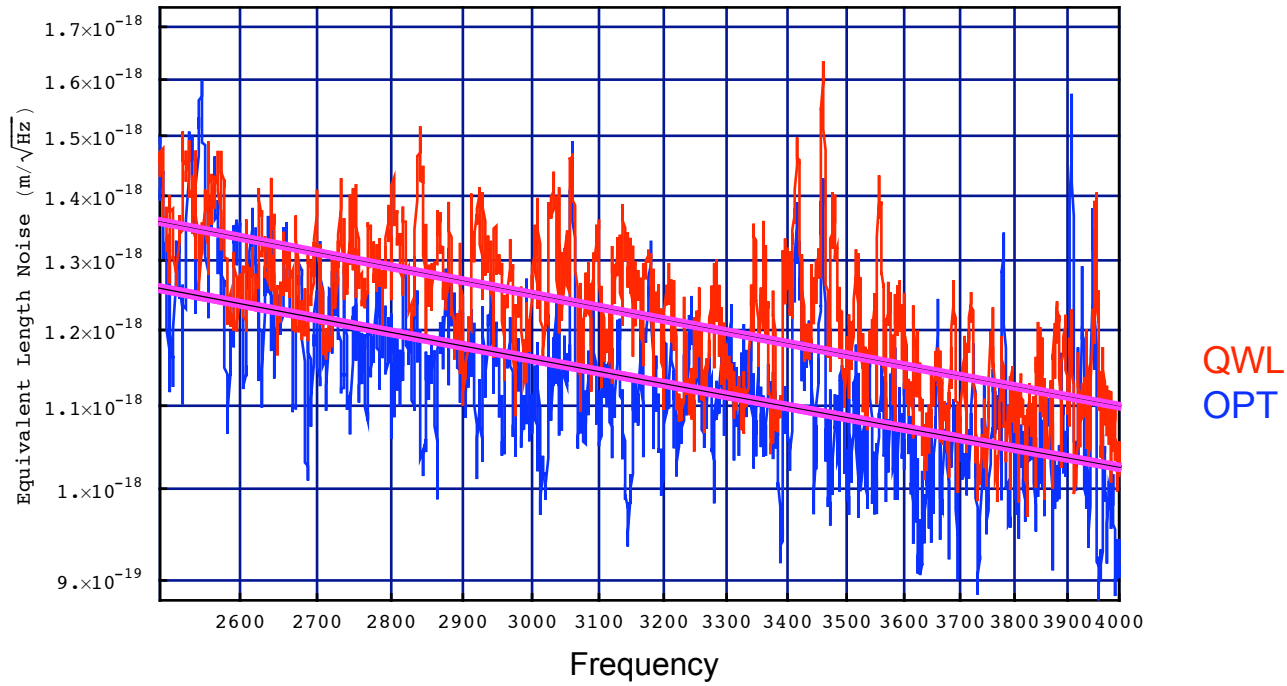
# Smoothed Spectra





# Smoothed Spectra

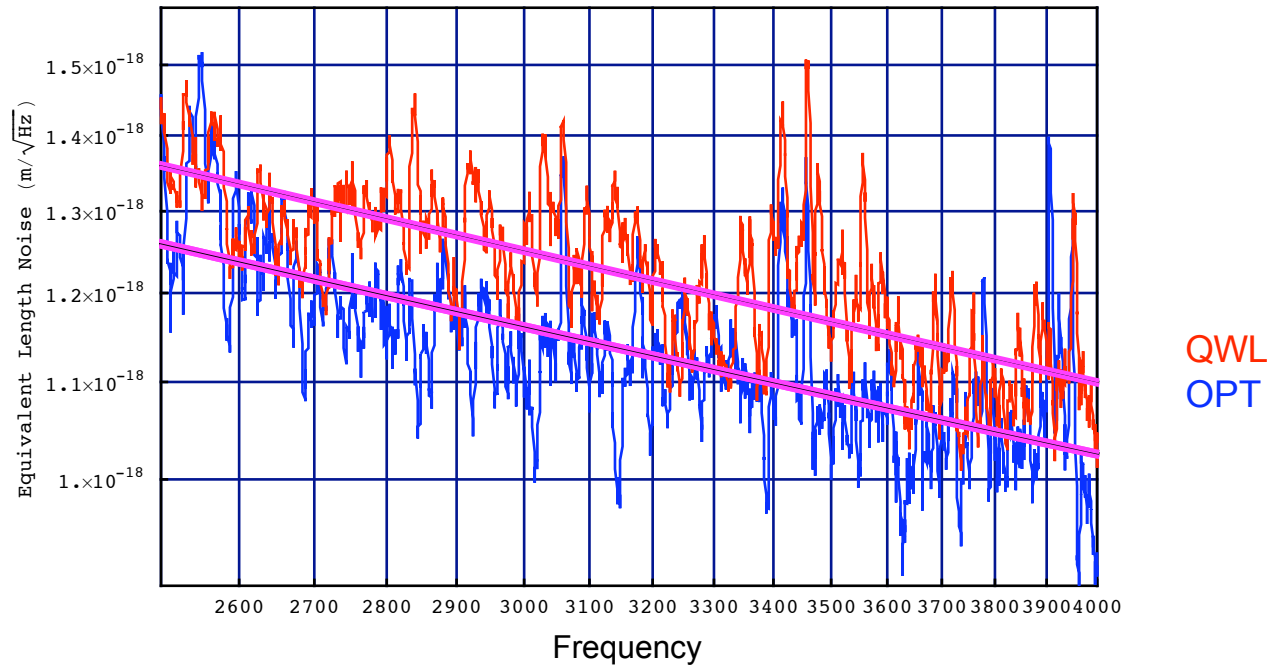
N=2





# Smoothed Spectra

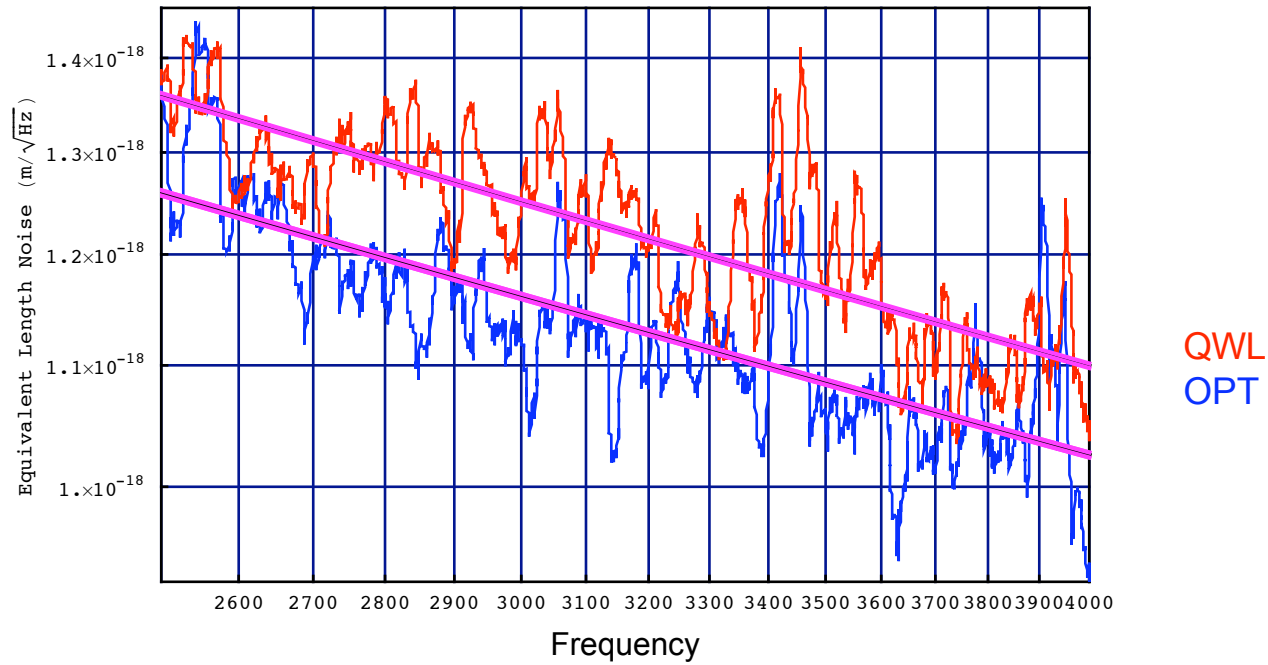
N=5





# Smoothed Spectra

N=10





# Smoothed Spectra

N=50

